AUTOMATED ELECTROMAGNETIC OPTIMIZATION OF RF AND MICROWAVE CIRCUITS

J.W. Bandler

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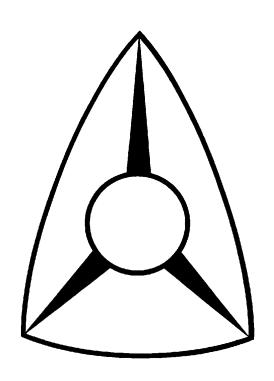
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J.W. Bandler

Optimization Systems Associates Inc. P.O. Box 8083, Dundas, Ontario Canada L9H 5E7

Email osa@osacad.com URL http://www.osacad.com



presented at

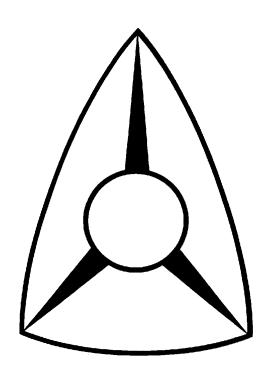
Ansoft Corporation, Pittsburgh, PA, May 8, 1996

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presented at

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Overview of the Presentation

OSA's technology

benchmark EM design problems

double folded stub filter attenuator
HTS filter interdigital filter frequency doubler waveguide transformers waveguide bend

Geometry CaptureTM for user-defined parameterization of arbitrary structures

parallel computing

Space MappingTM

EM optimization of 3D structures



Optimization Systems Associates Inc.

PIONEERS IN

yield and tolerance optimization

circuit performance optimization

parametric design centering

statistical device modeling

robust parameter extraction

harmonic balance simulation

physics based design

EM based design

large-scale optimization

benchmark CAD technology

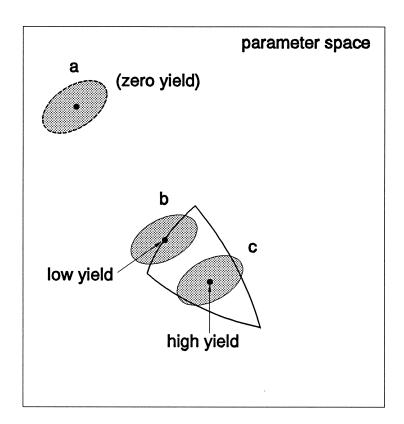
software architecture for IC design



Areas of Expertise

RF/microwave circuit simulation, design and optimization harmonic balance simulation techniques robust and statistical modeling of active and passive devices device modeling, statistical estimation of production yield powerful performance and yield optimization algorithms manufacturing tolerance assignment and cost minimization algorithms for automated production alignment and tuning customized optimizers for large-scale problems software architectures for integrated approach to design electromagnetic optimization





Yield interpretation in the parameter space



OSA90/hopeTM Version 3.1

general nonlinear circuit simulation and optimization analytically unified DC, small-signal and large-signal

harmonic balance analysis statistical analysis and yield optimization comprehensive optimization/nonlinear modeling interconnects external simulators

EmpipeTM merges *em*TM, even for arbitrary geometry! SpicepipeTM merges SPICE

Space MappingTM breakthrough in EM optimization 3D visualization

HarPETM Version 2.0

device characterization, simulation and optimization FET, bipolar, HEMT, HBT, thermal modeling parameter extraction cold measurement processing statistical modeling, Monte Carlo analysis Huber optimization cumulative probability distribution fitting can be invoked from OSA90/hopeTM as a child process



EmpipeTM Version 3.1

powerful and friendly software system for automated EM design optimization

driving Sonnet's emTM field simulator

employing the sophisticated optimizers of OSA90TM

breakthrough Geometry CaptureTM allows you to designate geometrical and material parameters as variables for optimization

any arbitrary structures that can be simulated by *em*TM can be optimized using EmpipeTM

automatic off-grid interpolation integrated with intelligent database management

intuitive and extremely user-friendly

a significant step towards the required <u>integrated approach</u> for interprocessing circuit/field/measurement data



OSA90/hopeTM **Optimization**

state-of-the-art gradient-based optimizers with a proven track record in electrical circuit and system optimization

L1
L2 (least squares)
Huber
minimax
quasi-Newton
conjugate gradient
simplex
random
simulated annealing
yield (design centering)

exact or approximate gradient

specification and goal definition

quadratic modeling of functions and gradients

sensitivity displays help the user to select the most crucial variables for optimization

Space MappingTM for CPU intensive optimization

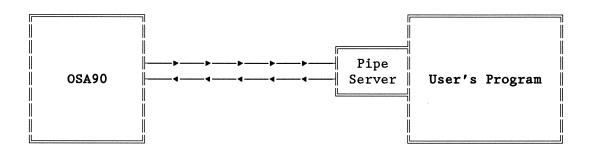
automated Aggressive Space MappingTM



OSA90/hopeTM DatapipeTM

DatapipeTM: predefined protocols for UNIX pipes

ready-to-use to facilitate high-speed data connections to and from the user's software; over networks

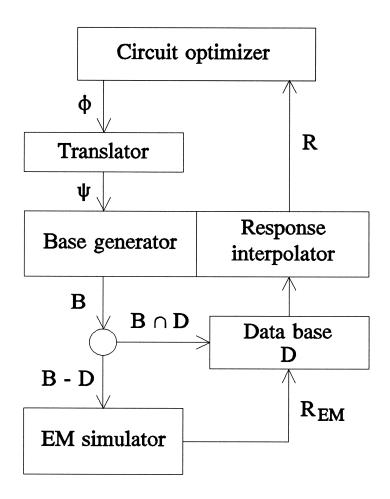


typical READ and WRITE statements are used to receive and send data

a small pipe server establishes the protocols

maintains complete security of user's software: OSA does not need access to the user's source code

Interconnection Between a Circuit Optimizer and a Numerical EM Simulator





Previous Work: Challenges of Automated EM Optimization (Bandler et al., 1993, 1994)

drastically increased analysis time

discrete nature of some EM solvers

continuity of optimization variables

gradient information

interpolation and modeling

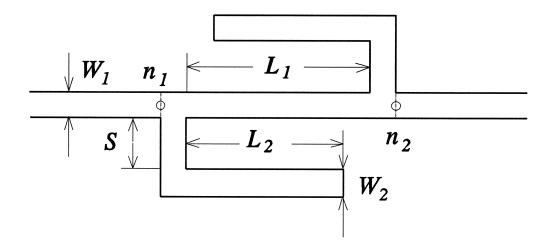
integrated data bases

original Space MappingTM algorithm



Benchmark EM Design Problems A Double Folded Stub Filter

(Jim Rautio, Sonnet Software)



for bandstop filter applications

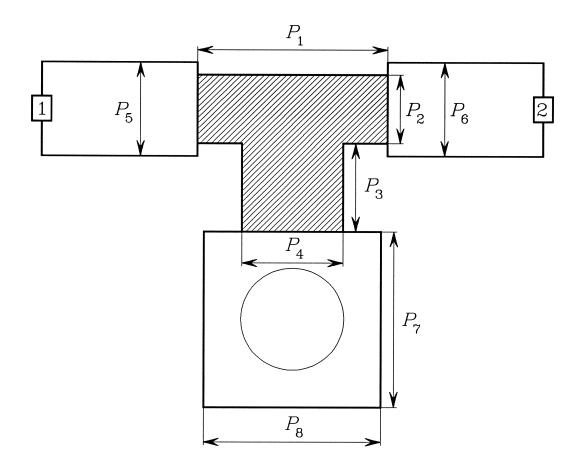
substantially reduced filter area w.r.t. the conventional double stub structure

substrate thickness is 5 mil and the relative dielectric constant is assumed to be 9.9



Benchmark EM Design Problems A 10 dB Distributed Attenuator

(Dan Swanson, Watkins-Johnson)



built on a 15 mil thick substrate with relative dielectric constant of 9.8

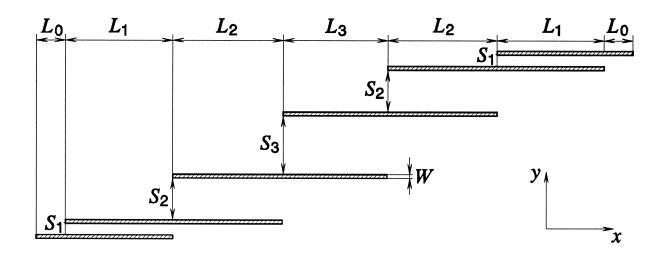
metallization of a high resistivity (50 Ω /sq)

the feed lines and the grounding pad are assumed lossless



Benchmark EM Design Problems An HTS Filter

(Chuck Moskowitz and Salvador Talisa, Westinghouse)



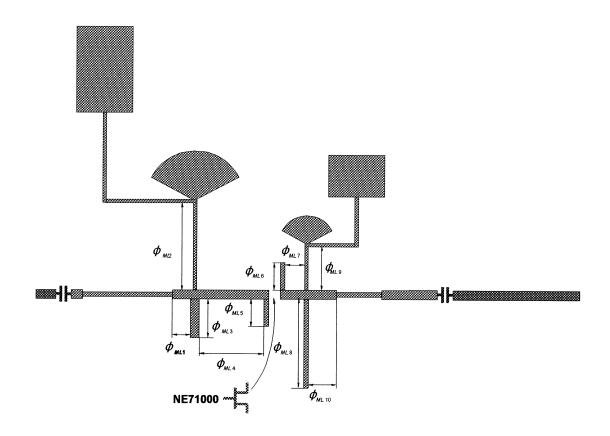
high-temperature superconducting four pole quarter-wave parallel coupled-line microstrip filter

high relative dielectric constant (more than 23) of the substrate material (lanthanum aluminate)

narrow bandwidth (1.25%)



Benchmark EM Design Problems A Nonlinear FET Class B Frequency Doubler (Microwave Engineering Europe, 1994)



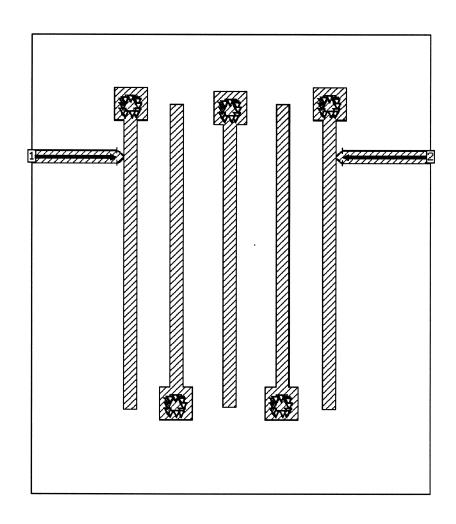
the linear subcircuit is defined as one optimizable structure with 10 variables

requires integration of large-signal harmonic balance of nonlinear circuits with active devices into EM-based optimization



Benchmark EM Design Problems An Interdigital C-Band Filter

(Dan Swanson, Watkins-Johnson)



a five-pole interdigital filter with tapped lines drawn using *xgeom* of Sonnet Software



Geometry CaptureTM

to optimize shapes and dimensions of geometrical objects by automatically adjusting the user-defined parameters subject to implicit geometrical constraints

work includes development of theory and algorithms employing concepts from analytic geometry, supported by graphical interfacing

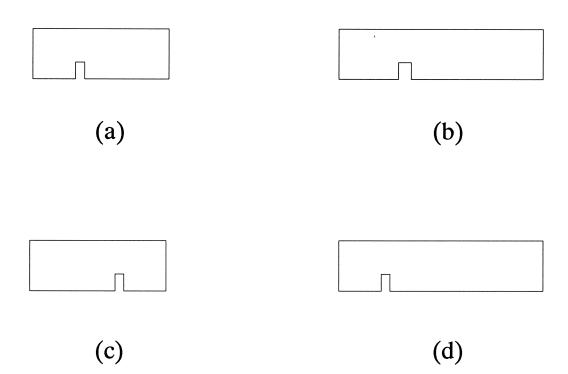
EM simulators deal directly with the layout representation of circuits in terms of absolute coordinates

geometrical coordinates are implicitly related to designable parameters

geometrical parameterization is needed for every new structure



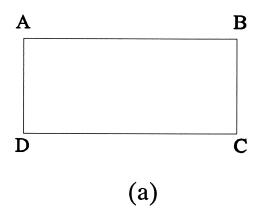
Various Object Evolutions

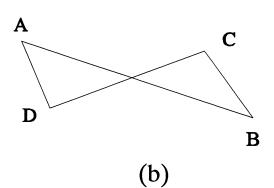


- (a) initial geometry
- (b) proportional expansion of the whole structure along the x axis
- (c) only the location of the slit in the fixed line is allowed to change
- (d) only the segment to the right of the slit is allowed to expand



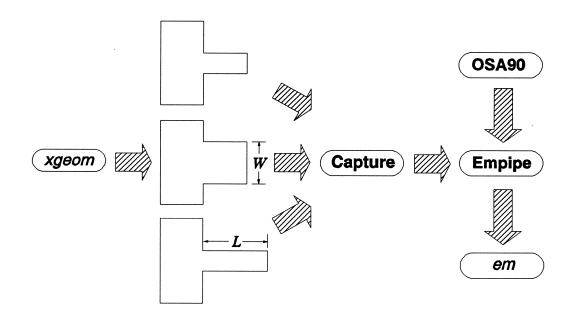
Possible Pitfalls of Arbitrary Movement of Vertices





- (a) initial geometry
- (b) an unwanted result due to an arbitrary and independent movement of vertices

Implementation of Geometry CaptureTM



employs a sophisticated algorithm in a manner completely transparent to the user

processed by $Empipe^{TM}$ to extract the relevant information extremely easy to use



Direct EM Optimization of the Frequency Doubler (Bandler et al., 1995)

involves optimization of an arbitrary planar structure

the complete structure between the two capacitors is considered as a whole and simulated by Sonnet's *em*TM

EmpipeTM links *em*TM simulations to the optimizer

the performance of the overall circuit is directly optimized with 10 optimization variables

design specification:

conversion gain > 3 dB spectral purity > 20 dB

at 7 GHz and 10 dBm input power



Parallel Computing Options

multiprocessor computers and specialized compilers vs. distributing EM analyses over a computer network

the overhead of parallelization is negligible as compared to the CPU-intensive EM analyses

splitting at the component/subcircuit level

suitable when several EM simulation results are needed simultaneously

off-grid interpolation

numerical gradient estimation

multiple outcomes in statistical analysis

suits best the operational flow of interpolation, optimization and statistical analysis



Organization of Parallel Computing

organized by EmpipeTM from one of the networked computers (master host)

using standard UNIX protocols (remote shell and equivalent hosts) an EM analysis is started on each of the available hosts

when the analysis is finished on a host, the next job, if any, is dispatched to that host

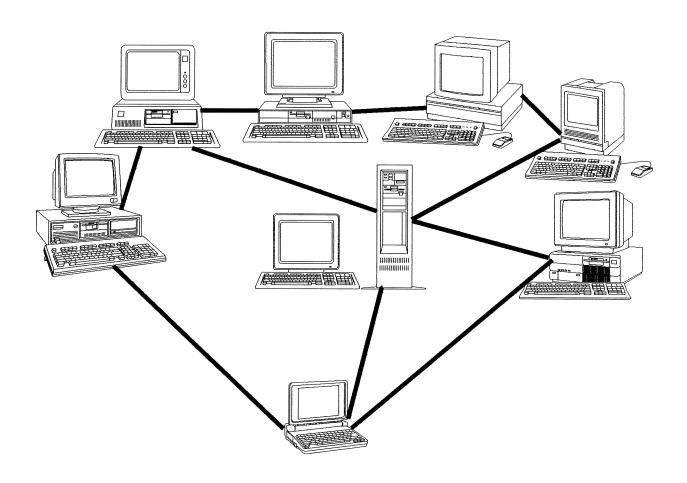
EM simulation results are gathered from all the hosts and stored in a data base created on the master host

no platform specific mechanisms

applicable to both local and wide area networks of heterogeneous workstations



Heterogeneous Network of Computers





Statistical Design of the Attenuator

design specifications (from 2 GHz to 18 GHz)

 $9.5 \text{ dB} \leq \text{insertion loss} \leq 10.5 \text{ dB}$

return loss $\geq 10 dB$

the structure, treated as a whole, is described by 8 geometrical parameters

designable: 4 parameters describing the resistive area

statistical variables: all 8 parameters (with a standard deviation of 0.25 mil)

*em*TM simulation at a single frequency requires about 7 CPU minutes on a Sun SPARCstation 1+



Parallel Computing in Nominal Design of the Attenuator

30 emTM analyses

an average of 3.8 analyses run in parallel

about 168 minutes on the network of Sun SPARCstations 1+ time is reduced by 75%

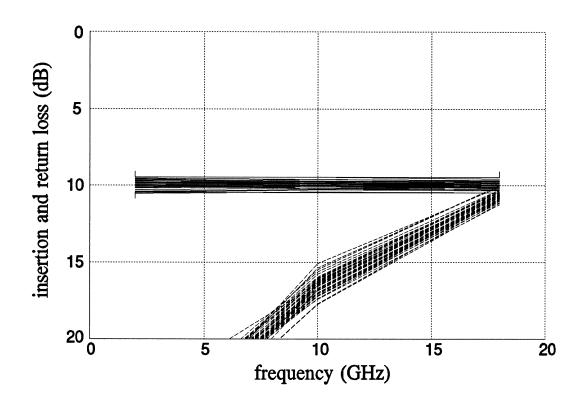
Parallel Computing in Statistical Design of the Attenuator

additional 113 emTM analyses

an average of 2.5 analyses run in parallel

time is reduced by 60%

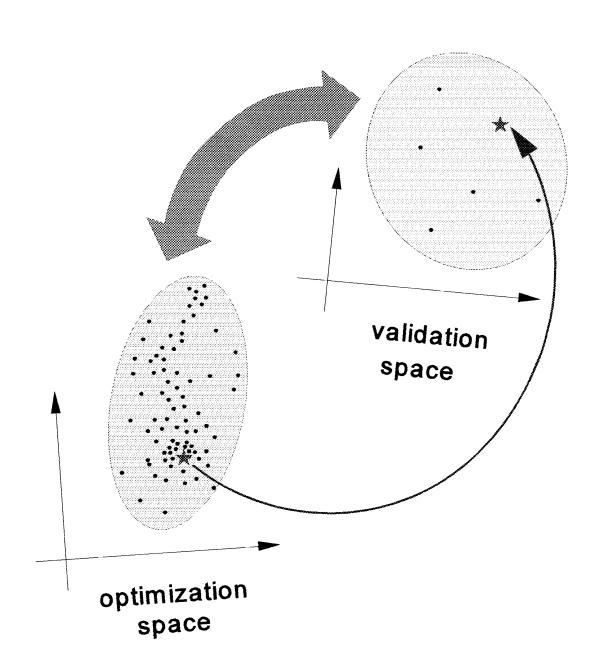
Monte Carlo Sweeps of the Attenuator Responses



yield (estimated from 250 Monte Carlo outcomes) is increased from 82% to 97%



Space MappingTM (Bandler et al., 1994)





Work on Space MappingTM

develop theory and corresponding algorithms for parameter Space MappingTM

to allow CPU intensive models to be automatically replaced during optimization by slower but also less accurate models

consider hierarchical family of models: equivalent circuit, empirical, or even decomposed or coarse grid numerical EM models, particularly for arbitrary geometries

aggressive strategy for Space MappingTM

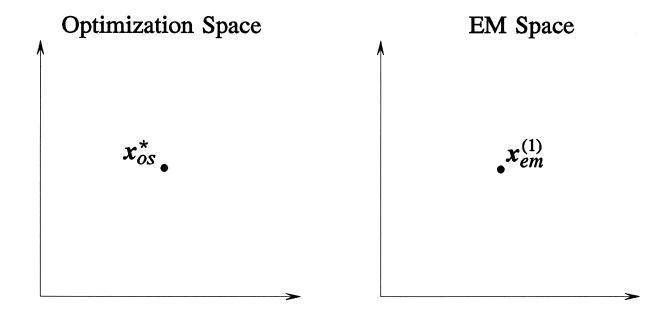
automation issues for Space MappingTM

expected cornerstone for successful EM optimization

Illustration of Aggressive Space MappingTM Optimization

Step 0

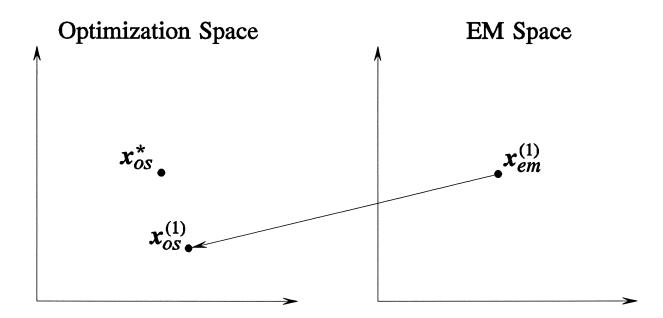
find the optimal design x_{os}^* in Optimization Space Step 1



set $x_{em}^{(1)} = x_{os}^*$ assuming x_{em} and x_{os} represent the same physical parameters

Illustration of Aggressive Space Mapping $^{\text{TM}}$ Optimization

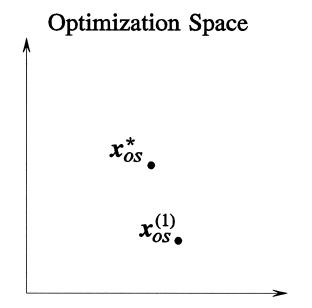
Step 2

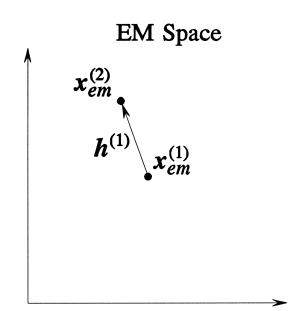


perform X_{os} -space model parameter extraction

Illustration of Aggressive Space MappingTM Optimization

Step 3





initialize Jacobian approximation $B^{(1)} = 1$

obtain $x_{em}^{(2)}$ by solving

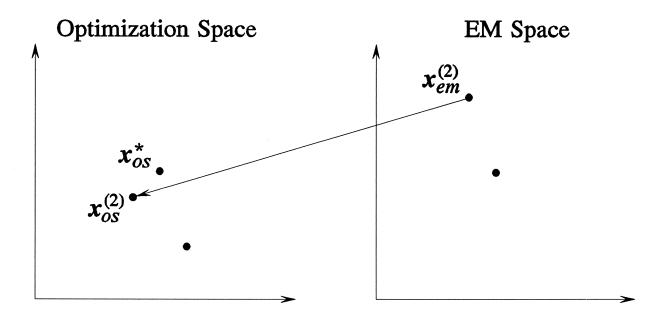
$$B^{(1)}h^{(1)} = -f^{(1)}$$

where

$$f^{(1)} = x_{os}^{(1)} - x_{os}^*$$

Illustration of Aggressive Space MappingTM Optimization

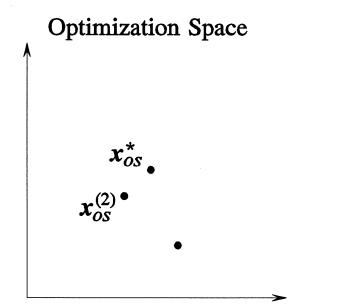
Step 4

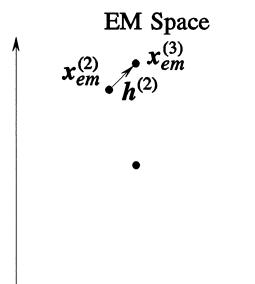


perform X_{os} -space model parameter extraction

Illustration of Aggressive Space MappingTM Optimization

Step 5





update Jacobian approximation from $B^{(1)}$ to $B^{(2)}$

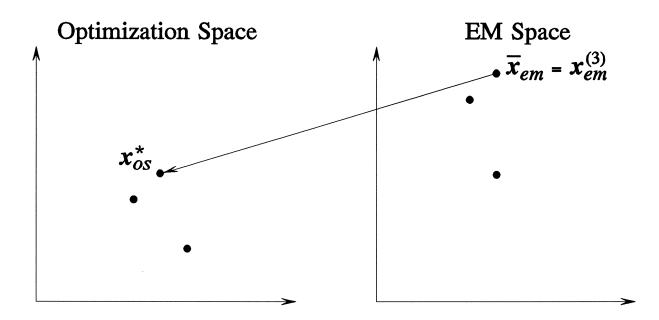
obtain $x_{em}^{(3)}$ by solving

$$B^{(2)}h^{(2)} = -f^{(2)}$$

where

$$f^{(2)} = x_{os}^{(2)} - x_{os}^*$$

Illustration of Aggressive Space Mapping $^{\text{TM}}$ Optimization Step 6



perform X_{os} -space model parameter extraction

if $\|x_{os}^{(3)} - x_{os}^*\| \le \epsilon$ then $\bar{x}_{em} = x_{em}^{(3)}$ is considered as the SM solution



Automated Aggressive Space MappingTM

automating the aggressive SM strategy using a two-level DatapipeTM architecture

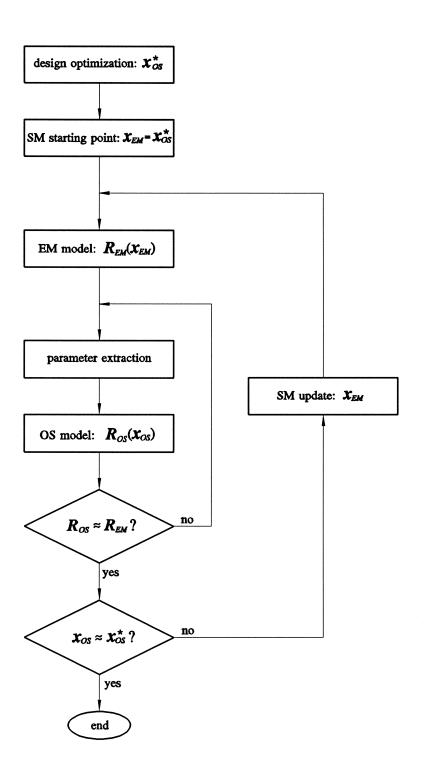
outer level automates a generic aggressive SM loop including a Broyden update

inner level implements parameter extraction for specific models

parameter extraction is crucial to SM optimization

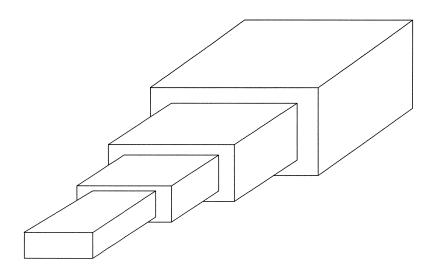
the impact of uniqueness on the convergence of the aggressive SM strategy

Implementation of Aggressive Space $Mapping^{TM}$





Benchmark EM Design Problems Waveguide Transformers



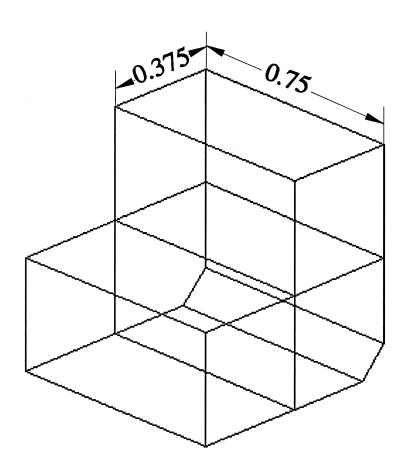
a two-section waveguide transformer

two cases of Space MappingTM used to align

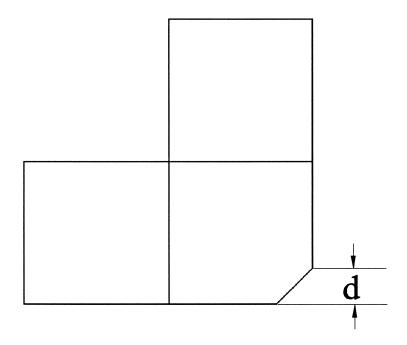
- (a) an ideal empirical model and a non-ideal empirical model
- (b) an empirical model and HFSS simulations



Benchmark EM Design Problems WR-75 Mitered Waveguide Bend



Single Section Mitered Bend



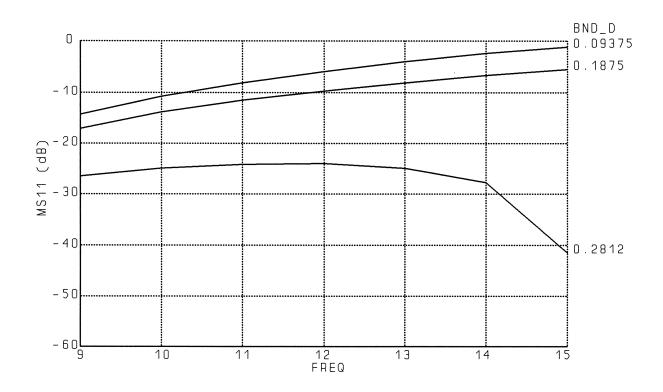
specification in the frequency range from 9.84 to 15 GHz

return loss ≥ 40 dB

one variable only: the position of the miter d, bounded as

 $0 \le d \le 0.375$ inch

Sweep of the Miter Position

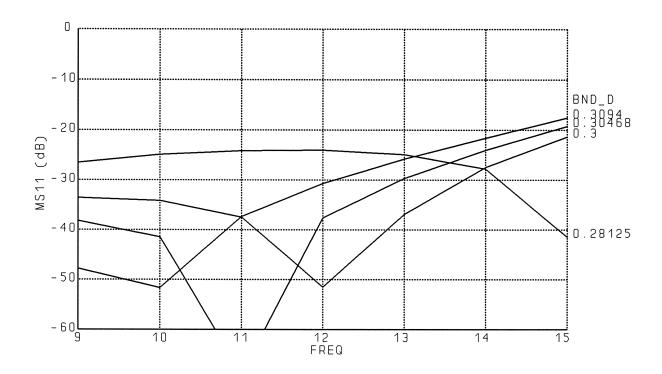


frequencies: from 9 GHz to 15 GHz with a step of 1 GHz

d is swept for 0.09375, 0.1875 and 0.28125 inch

simulation time is approximately 8 CPU hours for each value of d (SPARCstation 10, 9 adaptive meshing iterations)

Fine Sweep of the Parameter "d"



to emulate design by hand, we sweep d with these values: 0.28125, 0.3, 0.304675 and 0.3094 inch

by visual inspection, we can relate the position of the return loss pole to the parameter d as 1 GHz / 0.005 inch



Conclusions

cost-effective yield-driven design technology is indispensable

EM optimization of arbitrary geometries exerts a massive demand on resources, particularly for yield-driven design

integrated EM simulation and optimization capable of handling arbitrary structures is the future

Space MappingTM promises the accuracy of EM simulation and the speed of circuit-level optimization

heterogeneous parallel CAD over a local or wide area network significantly increases design power

Geometry CaptureTM user-defined parameterization allows analysis and optimization of complicated structures as a whole

integration of simulators from various sources into automated design optimization with interpolation, response function modeling and data base techniques will immensely reduce the overall design time



Selected References

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- J.W. Bandler, R.M. Biernacki and S.H. Chen, "Fully automated space mapping optimization of 3D structures," *IEEE MTT-S Int. Microwave Symp*. (San Francisco, CA), June 1996.
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- J.W. Bandler, R.M. Biernacki, Q. Cai, S.H. Chen and P.A. Grobelny, "Integrated harmonic balance and electromagnetic optimization with Geometry Capture," *IEEE MTT-S Int. Microwave Symp Dig.* (Orlando, FL), 1995, pp. 793-796.
- J.W. Bandler, R.M. Biernacki, Q. Cai, S.H. Chen, P.A. Grobelny and D.G. Swanson, Jr., "Heterogeneous parallel yield-driven electromagnetic CAD," *IEEE MTT-S Int. Microwave Symp. Dig.* (Orlando, FL), 1995, pp. 1085-1088.



New Products from OSA

to be unveiled at the IEEE Int. Microwave Symposium and Exhibition, San Francisco, June 1996

$EmpipeExpress^{TM}$

based on EmpipeTM and crafted to the needs of the majority of em^{TM} users

available from OSA for users who seek direct support from the developers

available from Sonnet Software as *empath*TM for users who prefer a single vendor

Empipe3DTM

driving Ansoft's Maxwell® Eminence or HP's HFSS finite element full-wave 3D field simulators

powerful and friendly software system for automated EM design optimization

the **Empipe** family features OSA's breakthrough Geometry CaptureTM front end for optimizing arbitrary structures