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The Aim of Space Mapping

(Bandler et al., 1994-)





The Derivative Space Mapping

assume that \boldsymbol{x}_c corresponds to \boldsymbol{x}_f through a parameter extraction process

the Jacobian J_f of the fine model response at x_f and the Jacobian J_c of the coarse model response at x_c are related by

$$\boldsymbol{J}_f = \boldsymbol{J}_c \boldsymbol{B}$$

where **B** is a valid mapping at \boldsymbol{x}_c and \boldsymbol{x}_f

consequently

$$\boldsymbol{B} = \left(\boldsymbol{J}_c^T \boldsymbol{J}_c \right)^{-1} \boldsymbol{J}_c^T \boldsymbol{J}_f$$

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The Algorithm

suppose we need a fast and accurate approximation to the fine model response near a particular point x_{em}^*

we denote by J_{em}^* the Jacobian of the fine model responses at x_{em}^* w.r.t. x_{em}

the point \overline{x}_{os} corresponding to x_{em}^* is obtained through the parameter extraction step

$$\overline{\mathbf{x}}_{os} = \arg \left\{ \min_{\mathbf{x}_{os}} \left\| \mathbf{R}_{em}(\mathbf{x}_{em}^{*}) - \mathbf{R}_{os}(\mathbf{x}_{os}) \right\| \right\}$$

the Jacobian \overline{J}_{os} of the coarse model responses at \overline{x}_{os} may be estimated by perturbation

the matrix **B** is then estimated by

$$\boldsymbol{B} = \left(\boldsymbol{\overline{J}}_{os}^{T}\boldsymbol{\overline{J}}_{os}\right)^{-1}\boldsymbol{\overline{J}}_{os}^{T}\boldsymbol{J}_{em}^{*}$$

the Space Derivative Mapping (SDM) model is simply given by

$$\boldsymbol{R}_{em}(\boldsymbol{x}_{em}) \approx \boldsymbol{R}_{os}(\boldsymbol{x}_{os} + \boldsymbol{B}(\boldsymbol{x}_{em} - \boldsymbol{x}_{em}^*))$$

the SDM model should enjoy a wide region of validity as the two models are assumed to share the same physical structure

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Two-Section WaveguideTransformer

(*Bandler*, 1969)

the coarse model is an "ideal" analytical model which neglects the junction discontinuity effects

the fine model is a more accurate "nonideal" analytical model which includes the junction discontinuity effects

optimizable parameters are the height and the length of each waveguide section.

the fine model is optimized using the OSA90/hope minimax optimizer

an estimate for the Jacobian of the fine model response is then obtained

parameter extraction is applied to get \overline{x}_{os} and the Jacobian of the coarse model \overline{J}_{os} is obtained using perturbation

the matrix **B** is estimated using SDM

the established mapping can be utilized in SDM statistical analysis



Two-Section WaveguideTransformer

(*Bandler*, 1969)



fine model response (0) and coarse model response (—) at the corresponding points



Statistical Analysis Using the SDM Model

1.0% tolerance



using fine model simulations



Statistical Analysis Using the SDM Model

4.0% tolerance



using Space Derivative Mapping





Six-Section H-Plane Filter

(Matthaei et al., 1964, Bakr et al., 1999)



the coarse model

optimizable parameters are the septa widths W_1 , W_2 , W_3 and W_4 and lengths L_1 , L_2 and L_3

the fine model exploits HP HFSS through HP Empipe3D



Six-Section H-Plane Filter

the H-plane speta have a finite thickness of 0.02 inches (0.508 mm)

the coarse model consists of lumped inductances and dispersive transmission line sections simulated by OSA90/hope

the equivalent inductances of the H-plane septa are calculated using formulas by *Marcuvitz* (1951)

the fine point of interest is the optimal fine model design

parameter extraction is then applied to obtain \overline{x}_{os}

linear interpolation formulas (*Bandler et al.*, 1997) are utilized to estimate J_{em}^* using the database generated during optimization

 \overline{J}_{os} is estimated by perturbation

the estimated matrix \boldsymbol{B} is utilized in statistical analysis



Six-Section H-Plane Filter



fine model response (o) and coarse model response (—) at the corresponding points



Statistical Analysis of the H-Plane Filter

1.0% tolerance







Statistical Analysis of the H-Plane Filter

4.0% tolerance









Three-section Rounded Edge Waveguide Transformer (*HP Empipe3D Manual*, 1998)



the fine model of this circuit exploits HP HFSS through HP Empipe3D

the coarse model exploits an ideal empirical model that does not take into account the rounding of the corners

designable parameters for this problem are the height and length of each waveguide section

the fine point of interest is the optimal fine model design

linear interpolation formulas (*Bandler et al.*, 1997) are utilized to estimate J_{em}^* using the database generated during optimization

 \overline{J}_{os} is estimated by perturbation



Three-section Rounded Edge Waveguide Transformer



fine model response (o) and coarse model response (—) at the corresponding points



Three-section Rounded Edge Waveguide Transformer

2.0% tolerance



using Space Derivative Mapping



using fine model simulations



Three-section Rounded Edge Waveguide Transformer

4.0% tolerance



using Space Derivative Mapping



using fine model simulations



Conclusions

we present a novel technique for the fast and accurate modeling of microwave circuits

the technique exploits a Space Derivative Mapping (SDM) approach in the construction of a space-mapping based model

a novel lemma establishes the mapping between the input parameters to an EM model and the parameters of a corresponding empirical model with no additional overhead of EM simulations

SDM Modeling (SDMM) alleviates the extraction uniqueness problem involved in prior SM algorithms and the necessity of applying SM optimization in the ASM algorithm

statistical analysis of microwave circuits exemplifies our technique