

**CCFIL1 - AN INTERACTIVE SOFTWARE SYSTEM  
FOR DESIGN OPTIMIZATION OF IDEAL  
MULTI-COUPLED CAVITY FILTERS**

J.W. Bandler, S.H. Chen, S. Daijavad and M.L. Renault

SOS-84-14-RU

September 1984

© J.W. Bandler, S.H. Chen, S. Daijavad and M.L. Renault 1984

No part of this document may be copied, translated, transcribed or entered in any form into any machine without written permission. Address enquiries in this regard to Dr. J.W. Bandler. Excerpts may be quoted for scholarly purposes with full acknowledgement of source. This document may not be lent or circulated without this title page and its original cover.

**CCFIL1 - AN INTERACTIVE SOFTWARE SYSTEM  
FOR DESIGN OPTIMIZATION  
OF IDEAL MULTI-COUPLED CAVITY FILTERS**

J.W. Bandler, S.H. Chen, S. Daijavad and M.L. Renault

Abstract

CCFIL1 is an interactive software system for design optimization of ideal multi-coupled cavity filters of the narrow-band lossless type with resistive load. User-oriented features for data entry, editing and storage are implemented. The engineering specifications are taken directly as the optimization objectives and the network parameters as the optimization variables. The gain and phase responses may be optimized concurrently and the variable network parameters may be subjected to any required equality or inequality linear constraints. The design solution is found in the minimax sense by the MMLC optimization package running simultaneously with a tracking algorithm which judiciously selects sample frequency points by applying a cubic interpolation routine to the gain response. The package and documentation have been developed on the DEC VAX 11/780 system with the VMS 3.6 operating system and the FORTRAN 3.5 compiler.

---

This work was supported in part by the Natural Sciences and Engineering Research Council of Canada under Grant G1135.

The authors are with the Simulation Optimization Systems Research Laboratory and the Department of Electrical and Computer Engineering, McMaster University, Hamilton, Canada L8S 4L7.

**TABLE OF CONTENTS**

	<b>PAGE</b>
I INTRODUCTION	3
II GENERAL DESCRIPTION	4
III SYSTEM DATA	6
IV OPTIMIZATION DATA	7
Optimization Variables	7
Gain Response Optimization	7
Phase Response Optimization	9
Constraints	10
Optimization Control Data	10
V INTERACTIVE FEATURES	12
VI STRUCTURE OF THE PACKAGE	14
VII LIMITS OF THE PACKAGE	16
APPENDIX A A SAMPLE INTERACTIVE DESIGN OPTIMIZATION SESSION	17
APPENDIX B GAIN RESPONSE CONVERSION TABLE FOR A LOSSLESS FILTER	38
APPENDIX C INCREASING THE LIMITS OF THE PACKAGE	39
REFERENCES	40

## I. INTRODUCTION

This document provides a user-oriented description of the CCFIL1 software system, which effectively implements the algorithm for an interactive computer program for design optimization of ideal multi-coupled cavity filters presented by Bandler and Chen [1]. Efficient approaches to the simulation and sensitivity evaluation of such filters have been developed and discussed in a report [2] wherein various formulas and tables are presented in detail. The CCFIL1 system applies these formulas to the case of a narrow-band lossless type filter with resistive load.

The design optimization is performed by the MMLC package [3,4] which applies a gradient-based minimax method and allows the formulation of linearly constrained design variables. A cubic interpolation technique used to improve computational efficiency has also been incorporated with the optimization procedure.

The CCFIL1 system has been developed in Fortran 77 on the DEC VAX 11/780 system. At McMaster University it is available on the Engineering VAX in the form of binary executable code as a group file under the charge ZE050. The general sequence of VMS commands to use the package can be as follows:

```
$ RUNH GR:CCFIL1
```

## II. GENERAL DESCRIPTION

The network parameters that can be used as optimization variables are the coupling matrix elements, including the diagonal ones which may represent deviations from synchronous tuning, and the input and output transformer ratios. The optimization objectives are formulated directly from the gain and phase responses of the filter. The gain response is specified in terms of the reflection coefficient, or the transducer loss in units of decibels. Since the phase response of interest to the CCFIL1 system is the group delay variation within a certain frequency band, the response is specified in terms of the relative group delay in units of nanoseconds.

The general formulation of the design optimization problem has been provided by Bandler [5] and it essentially consists in minimizing a discrete set of error functions. Each error function is defined at a particular frequency as the product of a weighting factor by the net difference of the network response minus the specified response. The weighting factor is defined as being either smaller or larger than zero which corresponds to a lower or an upper specification, respectively. Hence, the specification is satisfied if the error function is less than or equal to zero, or is violated if the error function is larger than zero. For the relative group delay specification, the network response which defines the error function should be interpreted as the magnitude of the difference between the average group delay and the group delay at the particular frequency.

In conjunction with the minimization of error functions, the variable network parameters may be subjected to any required equality or inequality linear constraints. The MMLC optimization package readily accommodates such constraints and the CCFIL1 system will prompt the user for the necessary data.

The optimal design solution that can be reached by the minimax method is an equal-ripple response which meets the specifications. For the filter problem

considered here, the presence of sharp ripples of the response, especially near the band edges creates a problem in the selection of representative sample frequency points. That is, the optimal solution requires the sample frequency points to present the error peaks to the minimax optimization package. The CCFIL1 system offers assistance with this task during gain response optimization by providing an algorithm to locate the peaks of the error function, that is, the error maxima w.r.t. frequency. The search procedure for a maximum starts from the lower frequency edge of a subinterval and proceeds with a given step-length to evaluate the slope of the error function. When two consecutive points yield a positive succeeded by a negative slope, it follows that at least one maximum lies between the two. If the points are close enough to exclude the existence of multiple maxima, the location of the detected maximum is estimated by a cubic interpolation formula [1]. The initial sample frequency points are then automatically changed in value to reflect the location of the detected error peak.

### III. SYSTEM DATA

For simulation purposes and before optimization can be performed, the following system data is required from the user:

- the order of the coupling matrix (i.e., that of the filter)
- whether the coupling matrix is symmetrical w.r.t. its anti-diagonal (it is always symmetrical w.r.t. its diagonal)
- the value of the coupling matrix elements (only the non-zero ones need be specified)
- the synchronously tuned cavity resonant frequency (the center frequency) in units of MHz
- the bandwidth parameter in units of MHz
- the load resistance multiplied by the output-transformer ratio squared, in units of ohms
- the source resistance and reactance, in units of ohms
- the value of the input-transformer ratio squared.

#### IV. OPTIMIZATION DATA

##### Optimization Variables

The variable coupling matrix elements are identified via their row and column indexes. Symmetrical elements are automatically taken into account. Variable input and output transformer ratios may also be specified. Note that the term transformer ratio should hereafter be interpreted as transformer ratio squared.

The MMLC optimization package printouts will list these parameters under the "VARIABLES" heading. First to be listed, and in the order they were specified, are the values of the coupling matrix elements. Then, if the transformer ratios are variable, the output and then the input ratios are listed. If the transformer ratios are equal by symmetry, only one value will be listed.

##### Gain Response Optimization

The user begins by indicating whether the specifications will be given in terms of the reflection coefficient or the transducer loss. A table which converts between values of these terms and the return loss is contained in Appendix B. The next step consists in dividing the frequency band of interest into a number of subintervals, each characterized by the following data:

- #1: the number of sample frequency points
- #2: the initial value of the sample frequency points
- #3: the step-length of the extrema search
- #4: the specified value of the response
- #5: the corresponding weighting factor

where items #4 and #5 are used to formulate the error functions to be evaluated at frequency points specified by items #1 to #3.

For any subinterval, upper or lower specifications are indicated by positive



or negative weighting factors, respectively. The magnitude of the weighting factor can be used to explicitly emphasize certain specifications, or to adjust for the inherent scaling effect arising when deviations from the specified values that may be insignificant for the stopband are critical for the passband or vice-versa [1].

Two approaches may be used to select the sample frequency points at which the subinterval's error functions are to be evaluated. The first consists in having sample frequency points that remain fixed, and the second in having sample frequency points that vary according to the location of the error peaks [1]. The former option is selected by choosing an extrema search step-length of zero, and the latter by choosing a step-length larger than zero. For both cases, the number of sample frequency points and their fixed/initial values, given in increasing order, have to be specified.

If the extrema tracking algorithm is used, certain rules of thumb can be applied to the selection of the number of sample frequency points and the search step-length value. The number of sample frequency points should equal the number of error peaks that will occur in the subinterval plus two points to delimit the edge of the subinterval plus two or three or more points dispersed throughout the subinterval. The choice of the initial value of the sample frequency points is not very critical and many of them will change value as the optimization proceeds. Upon exit from the MMLC optimization package, the sample frequency points of the last iteration will be listed and the extrema pointed out.

Choosing an extrema search step-length for a subinterval involves a compromise between too fine a step, which would make the search procedure unnecessarily time consuming, and too coarse a step which may not detect an error peak. A rule of thumb is to make the step-length equal to half the distance between either the two nearest error peaks, or an error peak and a subinterval

edge, whichever is the smallest.

It should now be clear that the criteria used to divide the frequency band of interest into a number of subintervals are the specification and weighting factor combination and the extrema search step-length. The last criterion is used to prevent a certain subsection of a frequency range from imposing a search step-length much finer than otherwise necessary on the remainder of the range. It should also be pointed out that, for symmetric responses, only one of the symmetrical halves need be considered throughout the response optimization.

One final word of caution for defining subintervals, is that no subintervals should usually have any points in common. This could give rise to either redundant calculations, or worse, a very ill-conditioned problem. A notable exception occurs when a frequency subinterval is specified twice, once with an upper specification and once with a lower specification.

### Phase Response Optimization

The data required for flat group delay optimization are:

- #1: number of sample frequency points
- #2: frequencies of the fixed sample points
- #3: specification for the relative delay
- #4: the weighting factor

There is effectively only one subinterval of interest, namely the passband, and since its group delay response is a well-behaved function, only fixed sample frequency points are required. The number of points and their locations can easily be determined by performing a group delay simulation and noting where the undesirable peaks occur. It should also be mentioned that the group delay sample frequency points do not interfere with those specified for the gain response optimization even if they happen to cover the same frequency range.

The relative delay specification is given in units of nanoseconds. A specification of zero implies that a perfectly flat response is desired w.r.t. the sample points, whereas a value larger than zero would tolerate a finite ripple in the response at the solution. The weighting factor should always be a positive value since the error function formula interprets as an upper specification the relative group delay specification.

### Constraints

The variable network parameters may be subjected to any required linear equality or inequality constraints. The generic forms of the linear constraints are:

$$C_1 * X_1 + \dots + C_i * X_i + \dots + C_n * X_n + B = 0$$

$$C_1 * X_1 + \dots + C_i * X_i + \dots + C_n * X_n + B \geq 0$$

where B is a constant,  $X_i$  are the variable network parameters and  $C_i$  their coefficients in the equation.

The CCFIL1 system will prompt the user for all the necessary data.

### Optimization Control Data

The CCFIL1 system utilizes the MMLC optimization package [3,4] to reach a design solution. The following control data is required:

- #1: maximum number of function evaluations
- #2: initial step-length
- #3: accuracy requirement

Data items #1 and #3 are used to stop the optimization algorithm if a solution has not yet been found. Item #1 limits the number of calls to the FDF subroutine (see Section VI of this report), and item #3 is used to measure if a sufficiently small change in the optimization variables is occurring. Data item #2 specifies the initial step-length of the iterative optimization algorithm. It must

be positive and normally an appropriate value is ten percent of the average variable network parameter.

The step-length is adjusted by the MMLC package during the optimization and upon return from the last function evaluation its value is saved by the CCFIL1 system. If the optimization process is initiated more than once, the user will be notified of the step-length value used during the last iteration. Using it for data item #2 will cause the optimization to proceed from the last function evaluation, otherwise the optimization will start anew from the specified step-length.

Apart from the optimization control data, the user will be prompted for certain printout options. One printout option is used to list the values of the optimization variables and the error functions at various stages of the optimization. The user chooses to have these values listed only at the last function evaluation, or regularly after a specified number of function evaluations. Another printout option involves the plotting of error functions as the optimization proceeds. These error functions are the ones evaluated at the search and sample frequency points and so this option does not create a computational burden for the package. This feature is offered as a matter of interest as it allows the user to observe the effects of the minimax optimization method on the error function values. The user is well forewarned that the plotting itself is time consuming and therefore slows down the optimization. It is best to test this feature when only a small number of function evaluations have been specified.

## V. INTERACTIVE FEATURES

The interactive system CCFIL1 offers many practical user-oriented features so as to allow efficient and productive design sessions. See, for example, the sample session of Appendix A. Most features are described below, while others which deal with the entry of invalid data or editing changes that have secondary implications, although present in the package, are not detailed here.

A typical interactive session begins by having the program prompt the user for all of the required system and optimization data. Entered data is regularly reiterated and the user queried about its correctness. Data entry may be made by the user from the keyboard or read from a file, which has been previously saved by the CCFIL1 system. Once the system is defined, the package enters a menu-driven mode having the following options:

- 1) NEW COUPLING MATRIX
- 2) NEW VARIABLE COUPLINGS
- 3) NEW CENTER FREQUENCY, BANDWIDTH, TERMINATIONS
- 4) NEW SUBINTERVAL DATA
- 5) NEW CONSTRAINTS
- 6) OPTIMIZATION
- 7) SIMULATION
- 8) VIEW A LOCAL FILE
- 9) SAVE THE DESIGN DATA
- 10) QUIT.

Menu items 1 to 5 allow editing of all the system data. Menu item 6 will allow the optimization to start anew or to proceed from the last function evaluation stage. Menu item 7 proceeds to simulate the existing system and offers to append the plot to a local file. This allows the user to create a file, which could later be referred to for comparison purposes by specifying menu item

8. Menu item 9 will save the entire design data, including the optimization step-length at the last function evaluation, in a format compatible with subsequent initial data entry to the program. The user may then select menu item 10 with the assurance of being able to proceed with the design session at some future time.

## VI. STRUCTURE OF THE PACKAGE

The CCFIL1 filter optimization system comprises the following files:

- CCFIL1 deals with the interactive features of the package
- FILOSUB implements the algorithm which solves the filter network
- LOWRPLT a low resolution plotting package
- LMMLC8D the MMLC optimization library

A block diagram of the structure is shown in Figure 1.

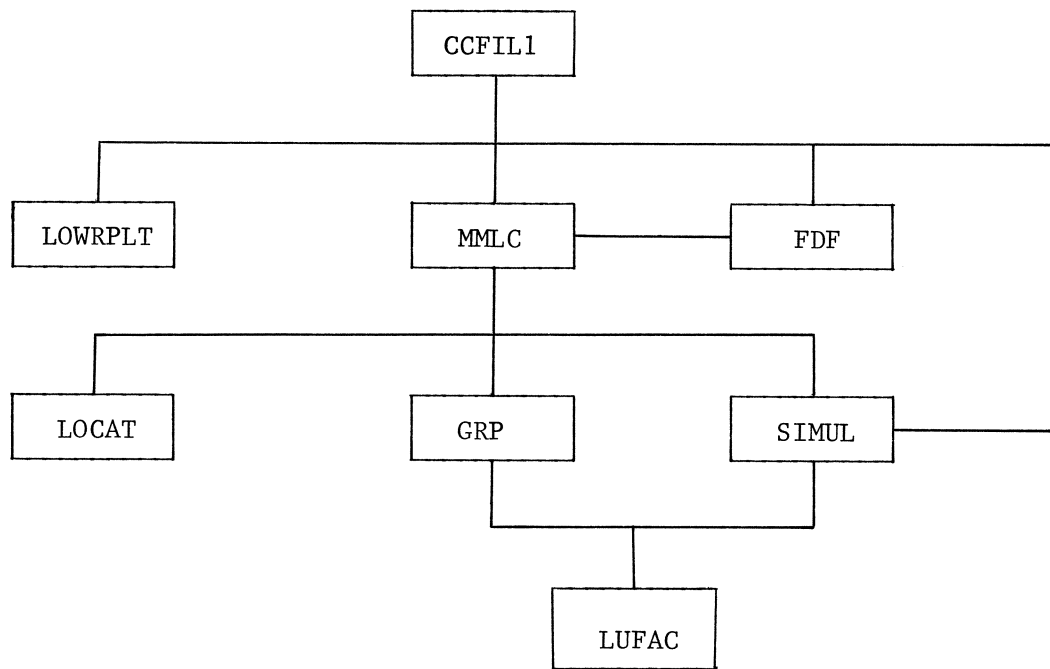


Figure 1. Structure of the CCFIL1 system.

The FILOSUB subroutines are further detailed:

- FDF interacts with the MMLC optimization package. Variable network parameters are updated and objective functions and gradients are

constructed in correspondence with the subinterval specifications. Optimal selection of sample frequency points is also performed in FDF.

- LOCAT estimates the frequency point at which a maximum occurs in the error function by applying a cubic interpolation algorithm to the error function.
- SIMUL computes the gain response and its sensitivities w.r.t. the optimization variables and the frequency at a given frequency point.
- LUFAC solves the loaded filter network at a given frequency. One real LU factorization of an  $N \times N$  matrix is performed. The complex original solution with or without three adjoint solutions is computed.
- GRP calculates the exact group delay and its sensitivities at a given frequency. The group delay is given in units of nanoseconds.



## VII. LIMITS OF THE PACKAGE

The size of a problem that can be accommodated by the CCFIL1 system is determined by the dimension of various arrays in the CCFIL1.FOR and FILOSUB.FOR routines. The present limits are:

- 12 = the order of the filter
- 30 = the number of optimization variables in the coupling matrix
- 40 = the number of linear constraints
- 10 = the number of frequency subintervals
- 50 = the total number of sample frequency points

If a larger problem is to be solved, adjustments will be required in the CCFIL1.FOR and FILOSUB.FOR routines. These files will then need to be recompiled and all files re-linked. A typical sequence of VMS commands that could be used is listed in Appendix C.

## APPENDIX A

## A SAMPLE INTERACTIVE DESIGN OPTIMIZATION SESSION

THIS IS A COMPUTER PROGRAM IMPLEMENTING AN ALGORITHM  
 FOR THE DESIGN OPTIMIZATION OF  
 NARROW-BAND MULTI-CAVITY MICROWAVE FILTERS

IS THE INPUT DATA TO BE READ FROM A LOCAL FILE ? Y/N  
 INPUT : N

-----  
 PLEASE ENTER:

# 1: ORDER OF THE COUPLING MATRIX  
 INPUT : 6  
 # 2: IS THE COUPLING MATRIX SYMMETRICAL  
 W.R.T. THE ANTIDIAGONAL ? Y/N  
 INPUT : Y  
 # 3: NUMBER OF NONZERO ELEMENTS OF THE COUPLING MATRIX  
 (NOT COUNTING SYMMETRICAL OR ANTISYMMETRICAL ONES)  
 INPUT : 5

RE:

# 1: ORDER OF THE COUPLING MATRIX  
 = 6  
 # 2: ANTISYMMETRICAL ?  
 = Y  
 # 3: NUMBER OF NONZERO ELEMENTS OF THE COUPLING MATRIX  
 = 5

DATA CORRECT ? ANSWER N IF NOT  
 INPUT :

-----  
 SET UP THE COUPLING MATRIX

FOR ELEMENT NUMBER " 1"  
 ENTER: ROW INDEX, COLUMN INDEX, COUPLING VALUE  
 INPUT : 1,2,.8101

FOR ELEMENT NUMBER " 2"  
 ENTER: ROW INDEX, COLUMN INDEX, COUPLING VALUE  
 INPUT : 2,3,.4894

FOR ELEMENT NUMBER " 3"  
 ENTER: ROW INDEX, COLUMN INDEX, COUPLING VALUE  
 INPUT : 3,4,.8450

FOR ELEMENT NUMBER " 4"  
 ENTER: ROW INDEX, COLUMN INDEX, COUPLING VALUE  
 INPUT : 1,6,.1197

FOR ELEMENT NUMBER " 5"  
 ENTER: ROW INDEX, COLUMN INDEX, COUPLING VALUE  
 INPUT : 2,5,-.4910

## CHECK YOUR COUPLING MATRIX

```

0.00000 0.81010 0.00000 0.00000 0.00000 0.11970
0.81010 0.00000 0.48940 0.00000 -0.40100 0.00000
0.00000 0.48940 0.00000 0.84500 0.00000 0.00000
0.00000 0.00000 0.84500 0.00000 0.48940 0.00000
0.00000 -0.40100 0.00000 0.48940 0.00000 0.81010
0.11970 0.00000 0.00000 0.00000 0.81010 0.00000

```

DATA CORRECT ? ANSWER N IF NOT

INPUT :

-----

VARIABLE COUPLINGS

ENTER THE NUMBER OF OPTIMIZATION VARIABLES  
IN THE COUPLING MATRIX

INPUT : 5

IDENTIFY VARIABLE NUMBER "1"  
ROW INDEX, COLUMN INDEX

INPUT : 1,2

IDENTIFY VARIABLE NUMBER "2"  
ROW INDEX, COLUMN INDEX

INPUT : 2,3

IDENTIFY VARIABLE NUMBER "3"  
ROW INDEX, COLUMN INDEX

INPUT : 3,4

IDENTIFY VARIABLE NUMBER "4"  
ROW INDEX, COLUMN INDEX

INPUT : 1,6

IDENTIFY VARIABLE NUMBER "5"  
ROW INDEX, COLUMN INDEX

INPUT : 2,4

RE:

THE VARIABLE ELEMENTS OF THE COUPLING MATRIX ARE :

```

( 1 , 2)
( 2 , 3)
( 3 , 4)
( 1 , 6)
( 2 , 4)

```

DATA CORRECT ? ANSWER N IF NOT

INPUT : N

PLEASE CHOOSE:

```

2 --- RE-KEY THIS DATA
3 --- CONTINUE

```

INPUT : 2

-----

## VARIABLE COUPLINGS

ENTER THE NUMBER OF OPTIMIZATION VARIABLES  
IN THE COUPLING MATRIX

INPUT : 5  
IDENTIFY VARIABLE NUMBER "1"  
ROW INDEX, COLUMN INDEX

INPUT : 1,2  
IDENTIFY VARIABLE NUMBER "2"  
ROW INDEX, COLUMN INDEX

INPUT : 2,3  
IDENTIFY VARIABLE NUMBER "3"  
ROW INDEX, COLUMN INDEX

INPUT : 3,4  
IDENTIFY VARIABLE NUMBER "4"  
ROW INDEX, COLUMN INDEX

INPUT : 1,6  
IDENTIFY VARIABLE NUMBER "5"  
ROW INDEX, COLUMN INDEX

INPUT : 2,5

RE:

THE VARIABLE ELEMENTS OF THE COUPLING MATRIX ARE :

( 1 , 2)  
( 2 , 3)  
( 3 , 4)  
( 1 , 6)  
( 2 , 5)

DATA CORRECT ? ANSWER N IF NOT

INPUT :

PLEASE ENTER:

# 1: CENTER FREQUENCY  
# 2: BANDWIDTH PARAMETER  
# 3: RESISTANCE \* OUTPUT TRANSFORMER RATIO SQUARED  
# 4: SOURCE RESISTANCE  
# 5: SOURCE REACTANCE  
# 6: VALUE OF THE INPUT-TRANSFORMER RATIO SQUARED

INPUT : 4000 40 .96 1 0 .96

# 7: TRANSFORMER RATIOS VARIABLE ? Y/N

INPUT : Y

RE:

```

# 1:      = CENTER FREQUENCY
           = 4000.00
# 2:      = BANDWIDTH PARAMETER
           = 40.00
# 3:      = RESISTANCE * OUTPUT TRANSFORMER RATIO SQUARED
           = 0.960000
# 4:      = SOURCE RESISTANCE
           = 1.000000
# 5:      = SOURCE REACTANCE
           = 0.000000
# 6:      = VALUE OF THE INPUT-TRANSFORMER RATIO SQUARED
           = 0.960000
# 7:      = TRANSFORMER RATIOS VARIABLE ? Y/N
           = Y
    
```

DATA CORRECT ? ANSWER N IF NOT

INPUT :

-----

SIMULATION ? ANSWER N IF NOT

INPUT :

-----

S I M U L A T I O N

LOWER & UPPER EDGES OF THE BAND TO BE SIMULATED

NUMBER OF FREQUENCY POINTS AND

RESPONSE INDICATOR : 1 --- REFLECTION COEF.  
 2 --- TRANSDUCER LOSS  
 3 --- GROUP DELAY

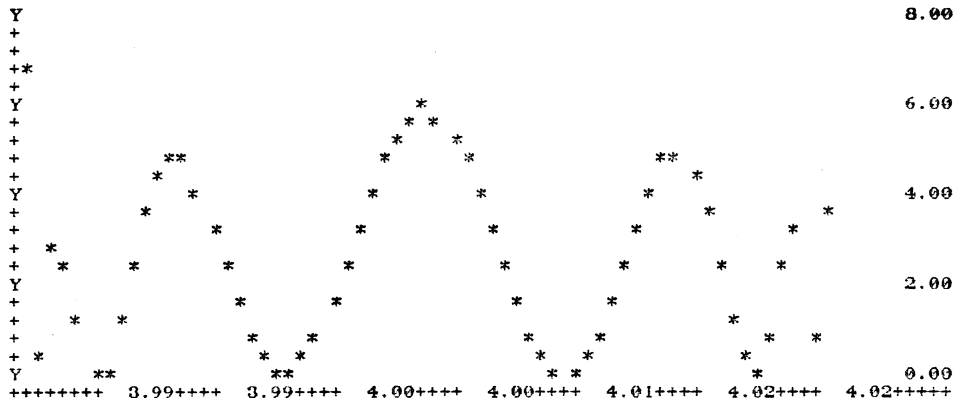
INPUT : 3980,4020,61,2

DATA CORRECT ?	ANSWER	N	IF NOT
INPUT :			
	3980.000		0.068989
	3980.667		0.005189
	3981.333		0.029428
	3982.000		0.025982
	3982.667		0.010701
	3983.333		0.000917
	3984.000		0.001737
	3984.667		0.010834
	3985.333		0.023501
	3986.000		0.035456
	3986.667		0.043886
	3987.333		0.047534
	3988.000		0.046391
	3988.667		0.041288
	3989.333		0.033518
	3990.000		0.024527
	3990.667		0.015697
	3991.333		0.008191
	3992.000		0.002867
	3992.667		0.000243
	3993.333		0.000497
	3994.000		0.003501
	3994.667		0.008274
	3995.333		0.016044
	3996.000		0.024319
	3996.667		0.032953
	3997.333		0.041209
	3998.000		0.048412
	3998.667		0.053992
	3999.333		0.057518
	4000.000		0.058723
	4000.667		0.057518
	4001.333		0.053995
	4002.000		0.048422
	4002.667		0.041230
	4003.333		0.032989
	4004.000		0.024370
	4004.667		0.016108
	4005.333		0.008942
	4006.000		0.003559
	4006.667		0.000525
	4007.333		0.000220
	4008.000		0.002771
	4008.667		0.008003
	4009.333		0.015426
	4010.000		0.024186
	4010.667		0.033150
	4011.333		0.040965
	4012.000		0.046267
	4012.667		0.047596
	4013.333		0.044283
	4014.000		0.036217
	4014.667		0.024536
	4015.333		0.011873
	4016.000		0.002318
	4016.667		0.000509
	4017.333		0.009139
	4018.000		0.024302
	4018.667		0.030499
	4019.333		0.009259
	4020.000		0.036167

DO YOU ALSO WANT THIS PLOT FILED (Y/N) ?  
INPUT : N

DATA CORRECT ? ANSWER N IF NOT  
INPUT :

X AXIS: FREQUENCY (MHZ)  
 Y AXIS: TRANSDUCER LOSS (DB)



PAUSING: TYPE ANYTHING TO CONTINUE OR TYPE STOP  
 INPUT :

-----  
 SIMULATION ? ANSWER N IF NOT

INPUT :  
 -----

## S I M U L A T I O N

LOWER &amp; UPPER EDGES OF THE BAND TO BE SIMULATED

NUMBER OF FREQUENCY POINTS AND

RESPONSE INDICATOR : 1 --- REFLECTION COEF.  
 2 --- TRANSDUCER LOSS  
 3 --- GROUP DELAY

INPUT : 3960,3980,31,2

DATA CORRECT ? ANSWER N IF NOT

INPUT :

3960.000	30.991592
3960.667	31.041719
3961.333	31.122062
3962.000	31.230210
3962.667	31.397144
3963.333	31.607702
3964.000	31.881296
3964.667	32.232935
3965.333	32.682910
3966.000	33.259515
3966.667	34.003819
3967.333	34.978661
3968.000	36.287360
3968.667	38.118485
3969.333	40.877867
3970.000	45.756820
3970.667	62.616600
3971.333	47.534349
3972.000	40.348165
3972.667	36.295534
3973.333	33.562348
3974.000	31.730949
3974.667	30.825116
3975.333	31.387553
3976.000	36.225100
3976.667	35.865191
3977.333	20.944713
3978.000	11.985676
3978.667	5.041695
3979.333	1.074342
3980.000	0.068988

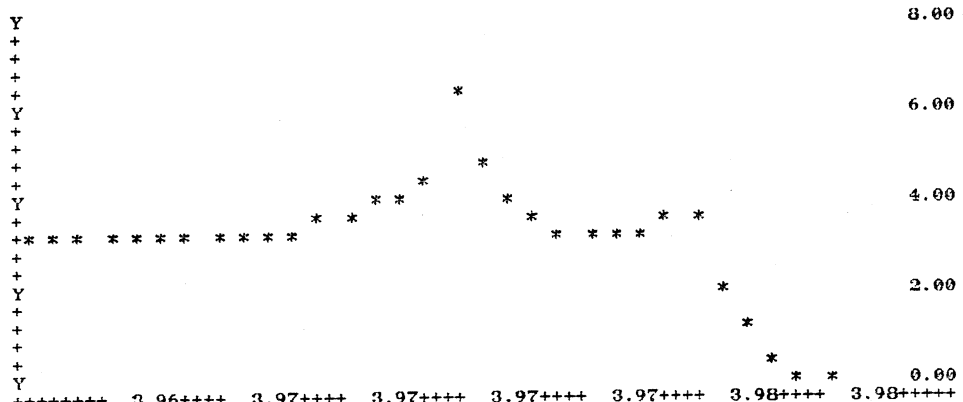
DO YOU ALSO WANT THIS PLOT FILED (Y/N) ?  
 INPUT : N

DATA CORRECT ? ANSWER N IF NOT

INPUT :



X AXIS: FREQUENCY (MHZ)  
 Y AXIS: TRANSDUCER LOSS (DB)



PAUSING: TYPE ANYTHING TO CONTINUE OR TYPE STOP  
 INPUT :

-----  
 SIMULATION ? ANSWER N IF NOT

INPUT :  
 -----

## S I M U L A T I O N

LOWER &amp; UPPER EDGES OF THE BAND TO BE SIMULATED

NUMBER OF FREQUENCY POINTS AND

RESPONSE INDICATOR : 1 --- REFLECTION COEF.  
 2 --- TRANSDUCER LOSS  
 3 --- GROUP DELAY

INPUT : 3985,4015,41,3

DATA CORRECT ? ANSWER N IF NOT

INPUT :

3985.000	37.576716
3985.750	34.662640
3986.500	32.321967
3987.250	30.449227
3988.000	28.948464
3988.750	27.735773
3989.500	26.740880
3990.250	25.907283
3991.000	25.191482
3991.750	24.561617
3992.500	23.995939
3993.250	23.481076
3994.000	23.010293
3994.750	22.581798
3995.500	22.197190
3996.250	21.860109
3997.000	21.575128
3997.750	21.346904
3998.500	21.179560
3999.250	21.076268
4000.000	21.038994
4000.750	21.068354
4001.500	21.163582
4002.250	21.322575
4003.000	21.542032
4003.750	21.817722
4004.500	22.144900
4005.250	22.518914
4006.000	22.936048
4006.750	23.394596
4007.500	23.896173
4008.250	24.447216
4009.000	25.060607
4009.750	25.757335
4010.500	26.568115
4011.250	27.504871
4012.000	28.711949
4012.750	30.166849
4013.500	31.980059
4014.250	34.243540
4015.000	37.058213

DO YOU ALSO WANT THIS PLOT FILED (Y/N) ?

INPUT : N

DATA CORRECT ? ANSWER N IF NOT

INPUT :



PLEASE ENTER:

```

SUBINTERVAL NUMBER 1
# 1: NUMBER OF SAMPLE POINTS
# 2: INITIAL POSITIONS OF THE SAMPLE POINTS
# 3: STEP-LENGTH OF EXTREMA SEARCH
      ( ENTER 0.0 FOR FIXED POINTS )
# 4: THE SPECIFIED VALUE OF THE RESPONSE
# 5: THE CORRESPONDING WEIGHTING FACTOR
      < 0 FOR LOWER SPECIFICATION

```

INPUT : 4,3950,3960,3965,3970,2,.9993,-1

RE:

```

SUBINTERVAL NUMBER 1
# 1: NUMBER OF SAMPLE POINTS
      = 4
# 2: INITIAL POSITIONS OF THE SAMPLE POINTS
      = 3950.00 3960.00 3965.00 3970.00
# 3: STEP-LENGTH OF EXTREMA SEARCH
      ( ENTER 0.0 FOR FIXED POINTS )
      = 2.0000
# 4: THE SPECIFIED VALUE OF THE RESPONSE
      = 0.999300
# 5: THE CORRESPONDING WEIGHTING FACTOR
      < 0 FOR LOWER SPECIFICATION
      = -1.000000

```

PLEASE CHOOSE:

```

2 --- EDIT THIS DATA
3 --- CONTINUE

```

INPUT : 3

PLEASE ENTER:

```

SUBINTERVAL NUMBER 2
# 1: NUMBER OF SAMPLE POINTS
# 2: INITIAL POSITIONS OF THE SAMPLE POINTS
# 3: STEP-LENGTH OF EXTREMA SEARCH
      ( ENTER 0.0 FOR FIXED POINTS )
# 4: THE SPECIFIED VALUE OF THE RESPONSE
# 5: THE CORRESPONDING WEIGHTING FACTOR
      < 0 FOR LOWER SPECIFICATION

```

INPUT : 4,3970,3972,3974,3976,1,.9993,-1

RE:

## SUBINTERVAL NUMBER 2

```

# 1:      NUMBER OF SAMPLE POINTS
      = 4
# 2:      INITIAL POSITIONS OF THE SAMPLE POINTS
      = 3970.00 3972.00 3974.00 3976.00
# 3:      STEP-LENGTH OF EXTREMA SEARCH
      ( ENTER 0.0 FOR FIXED POINTS )
      = 1.0000
# 4:      THE SPECIFIED VALUE OF THE RESPONSE
      = 0.999300
# 5:      THE CORRESPONDING WEIGHTING FACTOR
      < 0 FOR LOWER SPECIFICATION
      = -1.000000

```

PLEASE CHOOSE:

```

2 --- EDIT THIS DATA
3 --- CONTINUE

```

INPUT : 3

PLEASE ENTER:

## SUBINTERVAL NUMBER 3

```

# 1:      NUMBER OF SAMPLE POINTS
# 2:      INITIAL POSITIONS OF THE SAMPLE POINTS
# 3:      STEP-LENGTH OF EXTREMA SEARCH
      ( ENTER 0.0 FOR FIXED POINTS )
# 4:      THE SPECIFIED VALUE OF THE RESPONSE
# 5:      THE CORRESPONDING WEIGHTING FACTOR
      < 0 FOR LOWER SPECIFICATION

```

INPUT : 8,3980,3982,3984,3989,3993,3995,3998,4001,.5,.1,1

RE:

## SUBINTERVAL NUMBER 3

```

# 1:      NUMBER OF SAMPLE POINTS
      = 8
# 2:      INITIAL POSITIONS OF THE SAMPLE POINTS
      = 3980.00 3982.00 3984.00 3989.00 3993.00
      = 3995.00 3998.00 4001.00
# 3:      STEP-LENGTH OF EXTREMA SEARCH
      ( ENTER 0.0 FOR FIXED POINTS )
      = 0.5000
# 4:      THE SPECIFIED VALUE OF THE RESPONSE
      = 0.100000
# 5:      THE CORRESPONDING WEIGHTING FACTOR
      < 0 FOR LOWER SPECIFICATION
      = 1.000000

```

PLEASE CHOOSE:

```

2 --- EDIT THIS DATA
3 --- CONTINUE

```

INPUT : 3

PLEASE ENTER:

G R O U P      D E L A Y

# 1:            NUMBER OF POINTS ( ENTER 0 IF NONE )  
 INPUT : 0

DATA CORRECT ?    ANSWER N IF NOT  
 INPUT :

-----  
 C O N S T R A I N T S

NUMBER OF LINEAR CONSTRAINTS ( ENTER 0 IF NONE)

INPUT : 0

DATA CORRECT ?    ANSWER N IF NOT  
 INPUT :

-----  
 OPTIONS : ENTER    1 ---- NEW COUPLING MATRIX  
                       2 ---- NEW VARIABLE COUPLINGS  
                       3 ---- NEW CENTER FREQUENCY, BANDWITH, TERMINATIONS  
                       4 ---- NEW SUBINTERVAL DATA  
                       5 ---- NEW CONSTRAINTS  
                       6 ---- OPTIMIZATION  
                       7 ---- SIMULATION  
                       8 ---- VIEW A LOCAL FILE  
                       9 ---- SAVE THE DESIGN DATA  
                      10 ---- QUIT

INPUT : 9

-----  
 PLEASE ENTER THE FILE NAME  
 IN WHICH THE SYSTEM STATE IS TO BE SAVED:

INPUT : INIT.PNT

SYSTEM STATE IS NOW STORED IN FILE : INIT.PNT

TYPE ANYTHING TO CONTINUE...

INPUT :

-----

```

OPTIONS : ENTER  1 ---- NEW COUPLING MATRIX
                2 ---- NEW VARIABLE COUPLINGS
                3 ---- NEW CENTER FREQUENCY, BANDWIDTH, TERMINATIONS
                4 ---- NEW SUBINTERVAL DATA
                5 ---- NEW CONSTRAINTS
                6 ---- OPTIMIZATION
                7 ---- SIMULATION
                8 ---- VIEW A LOCAL FILE
                9 ---- SAVE THE DESIGN DATA
               10 ---- QUIT
INPUT : 6

```

-----

OPTIMIZATION CONTROL DATA

PLEASE ENTER:

# 1: MAXIMUM NO. OF ITERATIONS  
INPUT : 50

# 2: INITIAL STEP-LENGTH  
INPUT : .005

# 3: ACCURACY REQUIREMENT  
INPUT : 1.E-6

PRINTOUT CONTROL: FUNCTION VALUES AT SOLUTION ONLY? Y/N  
INPUT : N

AFTER HOW MANY FUNCTION EVALUATIONS ?  
INPUT : 10

DO YOU WISH TO SEE THE ERROR FUNCTIONS PLOTTED  
AS THE OPTIMIZATION PROCEEDS ? Y/N  
(WARNING: THIS PLOTTING IS TIME CONSUMING  
AND THEREFORE SLOWS DOWN THE OPTIMIZATION PROCESS)

INPUT : N

DATA CORRECT ? ANSWER N IF NOT  
INPUT :

-----

ATE : 18-OCT-1984                    TIME : 09:06:13  
LINEARLY CONSTRAINED MINIMAX OPTIMIZATION (MMLC PACKAGE) (REAL\*8)    (V:84.02)

INPUT DATA

```

-----
NUMBER OF VARIABLES (N) . . . . . 6
NUMBER OF FUNCTIONS (M) . . . . . 16
TOTAL NUMBER OF LINEAR CONSTRAINTS (L) . . . . . 0
NUMBER OF EQUALITY CONSTRAINTS (LEQ) . . . . . 0
STEP LENGTH (DX) . . . . . 5.000E-03
ACCURACY (EPS) . . . . . 1.000E-06
MAX NUMBER OF FUNCTION EVALUATIONS (MAXF) . . . . . 50
NUMBER OF SUCCESSIVE ITERATIONS (KEQS) . . . . . 3
WORKING SPACE (IW) . . . . . 8946
PRINTOUT CONTROL (IPIO) . . . . . 10000

```

STARTING POINT :

VARIABLES		FUNCTION VALUES	
1	8.101000000000E-01	1	-3.846836349045E-04
2	4.894000000000E-01	2	-2.993775218064E-04
3	8.450000000000E-01	3	-4.151457951448E-04
4	1.197000000000E-01	4	-6.867171602540E-04
5	-4.010000000000E-01	5	-6.867171602540E-04
6	9.600000000000E-01	6	-6.538508702268E-04
		7	-2.827413352129E-04
		8	-5.897424459313E-04
		9	2.553714130263E-02
		10	-1.553915347907E-02
		11	-8.000363508608E-02
		12	4.488379337303E-03
		13	-9.835686245257E-02
		14	-4.687239660174E-02
		15	1.588995855072E-02
		16	1.322247410953E-02

FUNCTION EVALUATION : 10 / 1

VARIABLES		FUNCTION VALUES	
1	8.201534041768E-01	1	-5.247889890181E-04
2	5.111040113376E-01	2	-5.027003561060E-04
3	8.267479102785E-01	3	-6.090597910786E-04
4	9.458781006473E-02	4	-6.937678285622E-04
5	-3.593457494794E-01	5	-6.937678285622E-04
6	9.670264259351E-01	6	-6.006983401075E-04
		7	-5.021960100974E-04
		8	-4.936119849662E-04
		9	-9.709394165884E-03
		10	-5.119351990363E-04
		11	-9.658129848684E-02
		12	-2.627209002094E-03
		13	-8.953627711734E-02
		14	-6.170063961931E-02
		15	-5.042177712500E-04
		16	-3.136655985882E-03

FUNCTION EVALUATION : 20 / 2

VARIABLES		FUNCTION VALUES	
1	8.183566974919E-01	1	-5.295407077706E-04
2	5.115146745080E-01	2	-5.082152699415E-04
3	8.242838684941E-01	3	-6.118164159783E-04
4	9.354212214981E-02	4	-6.939408656646E-04
5	-3.574834245519E-01	5	-6.939408656646E-04
6	9.856507688489E-01	6	-6.037946153604E-04
		7	-5.082125462975E-04
		8	-5.082176442507E-04
		9	-5.093942975951E-04
		10	-5.064299445283E-04
		11	-9.598340189497E-02
		12	-5.077782331604E-04
		13	-8.629493043951E-02
		14	-6.490221442620E-02
		15	-3.496121542879E-03
		16	-6.140303209929E-03

SOLUTION  
-----

VARIABLES		FUNCTION VALUES	
1	8.177562326145E-01	1	-5.312818327661E-04
2	5.110354748401E-01	2	-5.100499090424E-04
3	8.242954956108E-01	3	-6.124155349890E-04
4	9.330020381562E-02	4	-6.940881272135E-04
5	-3.571042539381E-01	5	-6.940881272135E-04
6	9.823662047636E-01	6	-6.049617180980E-04
		7	-5.100499083371E-04
		8	-5.100499090424E-04
		9	-5.100499090426E-04
		10	-5.100499090055E-04
		11	-9.649038243903E-02
		12	-5.100499090417E-04
		13	-8.802774342185E-02
		14	-6.256975104911E-02
		15	-5.100499090425E-04
		16	-3.180383321256E-03



TYPE OF SOLUTION (IFALL) . . . . . 0  
 NUMBER OF FUNCTION EVALUATIONS . . . . . 26  
 NUMBER OF SHIFTS TO STAGE-2 . . . . . 4  
 EXECUTION TIME (IN SECONDS) . . . . . 11.73

-----  
 THE CORRESPONDING FREQUENCY POINTS ARE :

3950.0000  
 3956.2750 ---- EXTREMUM POINT  
 3965.0000  
 3970.0000  
 3970.0000  
 3972.0000  
 3973.7262 ---- EXTREMUM POINT  
 3976.0000  
 3980.0000  
 3981.6456 ---- EXTREMUM POINT  
 3984.0000  
 3987.9864 ---- EXTREMUM POINT  
 3993.0000  
 3995.0000  
 4000.0000 ---- EXTREMUM POINT  
 4001.0000

-----  
 OPTIONS : ENTER 1 ---- NEW COUPLING MATRIX  
 2 ---- NEW VARIABLE COUPLINGS  
 3 ---- NEW CENTER FREQUENCY, BANDWIDTH, TERMINATIONS  
 4 ---- NEW SUBINTERVAL DATA  
 5 ---- NEW CONSTRAINTS  
 6 ---- OPTIMIZATION  
 7 ---- SIMULATION  
 8 ---- VIEW A LOCAL FILE  
 9 ---- SAVE THE DESIGN DATA  
 10 ---- QUIT  
 INPUT : 7

-----  
 S I M U L A T I O N

LOWER & UPPER EDGES OF THE BAND TO BE SIMULATED  
 NUMBER OF FREQUENCY POINTS AND  
 RESPONSE INDICATOR : 1 --- REFLECTION COEF.  
 2 --- TRANSDUCER LOSS  
 3 --- GROUP DELAY

INPUT : 3980.4020.61.2

DATA CORRECT ?	ANSWER	N	IF NOT
INPUT :			
	3980.000		0.043202
	3980.667		0.009239
	3981.333		0.039630
	3982.000		0.034593
	3982.667		0.022308
	3983.333		0.006389
	3984.000		0.000053
	3984.667		0.003486
	3985.333		0.013100
	3986.000		0.024630
	3986.667		0.034658
	3987.333		0.041110
	3988.000		0.043201
	3988.667		0.041140
	3989.333		0.035795
	3990.000		0.023376
	3990.667		0.020185
	3991.333		0.012425
	3992.000		0.006079
	3992.667		0.001832
	3993.333		0.000050
	3994.000		0.000790
	3994.667		0.003833
	3995.333		0.003744
	3996.000		0.014936
	3996.667		0.021737
	3997.333		0.028458
	3998.000		0.034453
	3998.667		0.039165
	3999.333		0.042170
	4000.000		0.043202
	4000.667		0.042170
	4001.333		0.039168
	4002.000		0.034461
	4002.667		0.028476
	4003.333		0.021765
	4004.000		0.014975
	4004.667		0.008790
	4005.333		0.003876
	4006.000		0.000816
	4006.667		0.000042
	4007.333		0.001771
	4008.000		0.005950
	4008.667		0.012224
	4009.333		0.019919
	4010.000		0.023076
	4010.667		0.035512
	4011.333		0.040950
	4012.000		0.043190
	4012.667		0.041361
	4013.333		0.035212
	4014.000		0.025449
	4014.667		0.014009
	4015.333		0.004147
	4016.000		0.000000
	4016.667		0.005225
	4017.333		0.020208
	4018.000		0.037970
	4018.667		0.041378
	4019.333		0.043203
	4020.000		0.020777

DO YOU ALSO WANT THIS PLOT FILED (Y/N) ?

INPUT : N

DATA CORRECT ? ANSWER N IF NOT

INPUT :



DATA CORRECT ? ANSWER N IF NOT

INPUT :

3960.000	34.553816
3960.667	34.720288
3961.333	34.933625
3962.000	35.203393
3962.667	35.541930
3963.333	35.965551
3964.000	36.496412
3964.667	37.165645
3965.333	38.018927
3966.000	39.127235
3966.667	40.609936
3967.333	42.692819
3968.000	45.892538
3968.667	51.949997
3969.333	70.031076
3970.000	49.272462
3970.667	43.347224
3971.333	39.733311
3972.000	37.210921
3972.667	35.444373
<b>3973.333</b>	<b>34.400250</b>
3974.000	34.321634
3974.667	36.150687
3975.333	46.448764
3976.000	34.203717
3976.667	23.176257
3977.333	15.438644
3978.000	8.851656
3978.667	3.566890
3979.333	0.741361
3980.000	0.043202

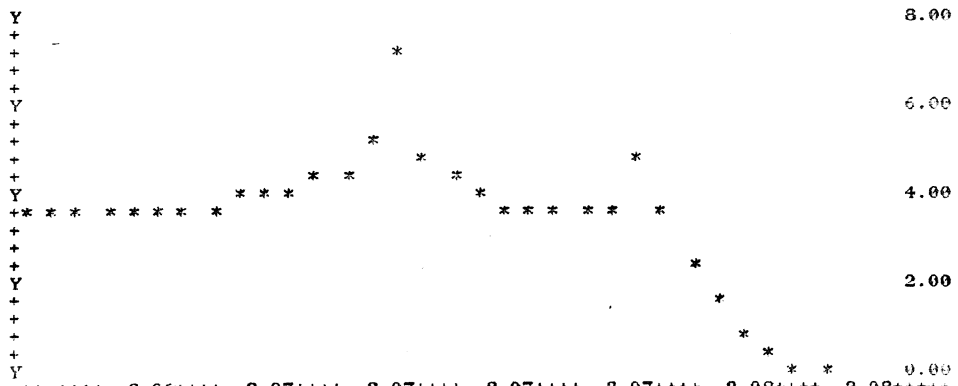
DO YOU ALSO WANT THIS PLOT FILED (Y/N) ?

INPUT : N

DATA CORRECT ? ANSWER N IF NOT

INPUT :

X AXIS: FREQUENCY (MHZ)  
Y AXIS: TRANSDUCER LOSS (DB)



PAUSING: TYPE ANYTHING TO CONTINUE OR TYPE STOP  
INPUT :

-----

OPTIONS : ENTER 1 ---- NEW COUPLING MATRIX  
 2 ---- NEW VARIABLE COUPLINGS  
 3 ---- NEW CENTER FREQUENCY, BANDWIDTH, TERMINATIONS  
 4 ---- NEW SUBINTERVAL DATA  
 5 ---- NEW CONSTRAINTS  
 6 ---- OPTIMIZATION  
 7 ---- SIMULATION  
 8 ---- VIEW A LOCAL FILE  
 9 ---- SAVE THE DESIGN DATA  
 10 ---- QUIT

INPUT : 7

-----

S I M U L A T I O N

LOWER & UPPER EDGES OF THE BAND TO BE SIMULATED  
 NUMBER OF FREQUENCY POINTS AND

RESPONSE INDICATOR : 1 --- REFLECTION COEF.  
 2 --- TRANSDUCER LOSS  
 3 --- GROUP DELAY

INPUT : 3985.4015,41,3

DATA CORRECT ? ANSWER N IF NOT

INPUT :

3985.000	33.521876
3985.750	35.731513
3986.500	33.429010
3987.250	31.553710
3988.000	30.033468
3988.750	28.796796
3989.500	27.786961
3990.250	26.944418
3991.000	26.227768
3991.750	25.603720
3992.500	25.043391
3993.250	24.546209
3994.000	24.068555
3994.750	23.672170
3995.500	23.297853
3996.250	22.968657
3997.000	22.689774
3997.750	22.465520
3998.500	22.300584
3999.250	22.190488
4000.000	22.161442
4000.750	22.190155
4001.500	22.283767
4002.250	22.439939
4003.000	22.655022
4003.750	22.924420
4004.500	23.243152
4005.250	23.606533
4006.000	24.011215
4006.750	24.456342
4007.500	24.944911
4008.250	25.465225
4009.000	26.023223
4009.750	26.709281
4010.500	27.608252
4011.250	28.591096
4012.000	29.769461
4012.750	31.263543
4013.500	33.000374
4014.250	35.009307
4015.000	38.018209

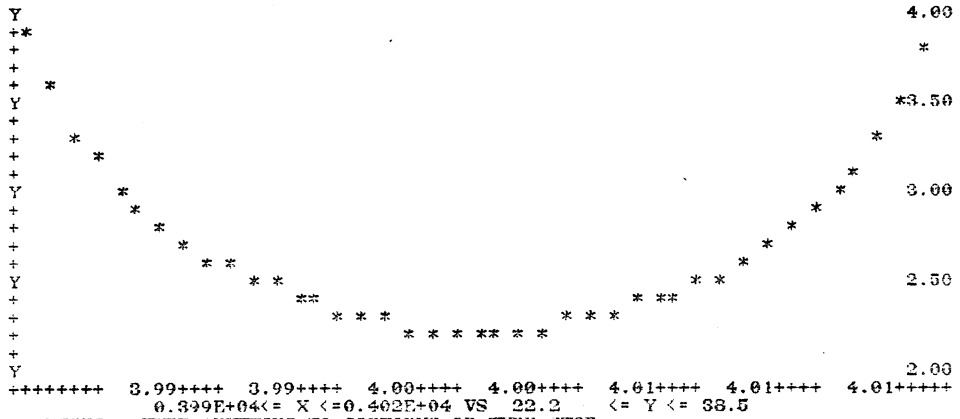
DO YOU ALSO WANT THIS PLOT FILED (Y/N) ?

INPUT : N

DATA CORRECT ? ANSWER N IF NOT

INPUT :

X AXIS: FREQUENCY (MEZ)  
 Y AXIS: GROUP DELAY (NSECS)



PAUSING: TYPE ANYTHING TO CONTINUE OR TYPE STOP  
 INPUT :

- 
- OPTIONS : ENTER
- 1 ---- NEW COUPLING MATRIX
  - 2 ---- NEW VARIABLE COUPLINGS
  - 3 ---- NEW CENTER FREQUENCY, BANDWIDTH, TERMINATIONS
  - 4 ---- NEW SUBINTERVAL DATA
  - 5 ---- NEW CONSTRAINTS
  - 6 ---- OPTIMIZATION
  - 7 ---- SIMULATION
  - 8 ---- VIEW A LOCAL FILE
  - 9 ---- SAVE THE DESIGN DATA
  - 10 ---- QUIT
- INPUT : 10

**APPENDIX B**  
**GAIN RESPONSE CONVERSION TABLE FOR A LOSSLESS FILTER**

---

REFLECTION COEFFICIENT	RETURN LOSS (DB)	TRANSDUCER LOSS (DB)
0.031623	30	0.004345
0.042170	27.5	0.007730
0.056234	25	0.013755
0.074989	22.5	0.024491
0.089125	21	0.034635
0.1	20	0.043648
0.112202	19	0.055022
0.125893	18	0.069383
0.141254	17	0.087530
0.158489	16	0.110483
0.177828	15	0.139554
0.984062		15
0.989973		17
0.993685		19
0.994987		20
0.997184		22.5
0.998418		25
0.999002		27
0.999110		27.5
0.999500		30
0.999719		32.5
0.999482		35
0.999900		37
0.999911		37.5
0.999950		40
0.999972		42.5
0.999984		45
0.999990		47
0.999995		50

---

## APPENDIX C

### INCREASING THE LIMITS OF THE SYSTEM

Increasing the limits of the CCFIL1 system requires re-dimensioning of particular arrays in the CCFIL1.FOR and FILOSUB.FOR routines. These arrays are automatically dimensioned according to the MAXNT and MAXEL parameters. Hence, the only editing needed involves redefining 'ia' and 'ib' in all occurrences of

```
PARAMETER ( MAXNT=ia, MAXEL=ib )
```

where 'ia' is an integer value equal to the maximum order of the coupling matrix and 'ib' is an integer value equal to the maximum number of optimization variables in the coupling matrix (not counting as more than one those set equal by matrix symmetry).

The user will have to be given permission, via the master account ZE050, to read the following files:

- CCFIL1.FOR
- FILOSUB.FOR
- LOWRPLT.OBJ
- LMMLC8D.OLB.

The following sequence of VMS commands could then be used:

\$COPY GR:*. * *	to obtain the above files
\$EDIT CCFIL1.FOR	to edit the MAXNT,
...	MAXEL parameters
\$EDIT FILOSUB.FOR	to edit the MAXNT,
...	MAXEL parameters
\$FOR CCFIL1	to compile the edited file
\$FOR FILOSUB	to compile the edited file
\$LINK CCFIL1,FILOSUB,LOWRPLT,LMMLC8D/LIB	to re-link all files

The executable file CCFIL1.EXE is thence available and can be used:

```
$RUNH CCFIL1
```



## REFERENCES

- [1] J.W. Bandler and S.H. Chen, "Interactive optimization of multi-coupled cavity microwave filters", Department of Electrical and Computer Engineering, McMaster University, Hamilton, Canada, Report SOS-84-13-R, 1984.
- [2] J.W. Bandler, S.H. Chen and S. Daijavad, "Efficient approaches to the simulation of narrow-band multi-cavity filters", Department of Electrical and Computer Engineering, McMaster University, Hamilton, Canada, Report SOS-84-9-R, 1984.
- [3] J. Hald and K. Madsen, "Combined LP and quasi-Newton methods for minimax optimization", Mathematical Programming, vol. 20, 1981, pp. 49-62.
- [4] J.W. Bandler and W.M. Zuberek, "MMLC - a Fortran package for linearly constrained minimax optimization", Department of Electrical and Computer Engineering, McMaster University, Hamilton, Canada, Report SOS-82-5-U2, 1983.
- [5] J.W. Bandler, "Computer-aided circuit optimization", in Modern Filter Theory and Design, G.C. Temes and S.K. Mitra, Eds. New York: Wiley-Interscience, 1973.