APPLICATIONS EXPLOITING COMMERCIAL EM SIMULATORS INCLUDING WAVEGUIDE STRUCTURES, MICROSTRIP FILTERS AND PATCH ANTENNAS

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presented at

WORKSHOP ON NEXT GENERATION OPTIMIZATION METHODOLOGIES FOR WIRELESS AND MICROWAVE CIRCUIT DESIGN

McMaster University, June 28, 1999

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Three-Section Waveguide Transformer

(Bandler et al., 1996)

design specifications

 $vswr \le 1.04$ for 5.7 GHz $\le f \le 7.2$ GHz

the designable parameters are the heights of the waveguide sections b_1 , b_2 and b_3 and the lengths of waveguide sections L_1 , L_2 and L_3

the fine model exploits HP HFSS through HP Empipe3D

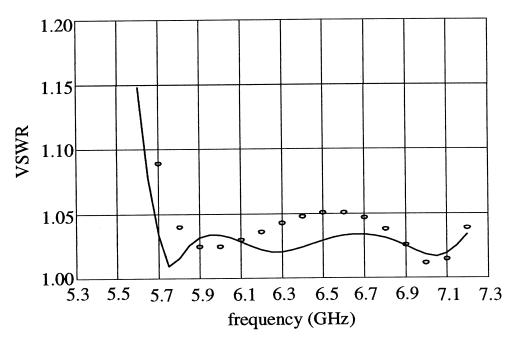
the coarse analytical model does not take into account the junction discontinuity effects

the first phase executed 2 iterations which required 4 fine model simulations

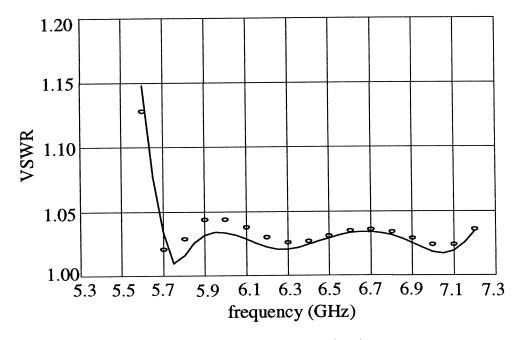
the second phase carried out only 1 iteration which required 2 fine model simulations

minimax optimization is then applied to the original problem starting from the second phase design

Optimization Results for the Three-Section Waveguide Transformer

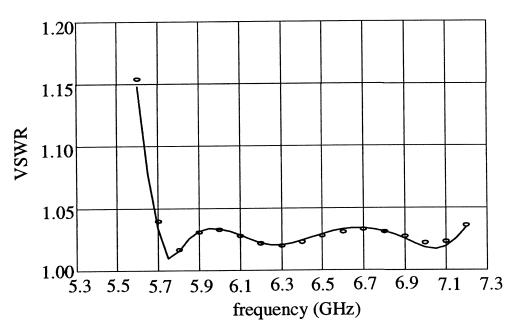


the initial fine model design

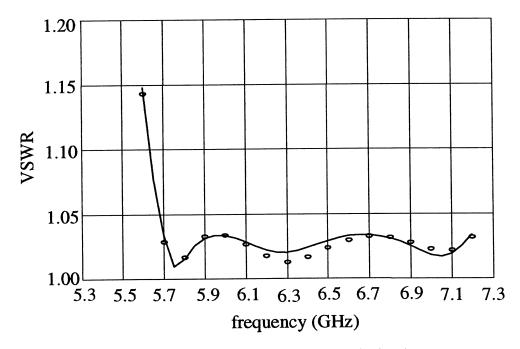


the first phase design

Optimization Results for the Three-Section Waveguide Transformer



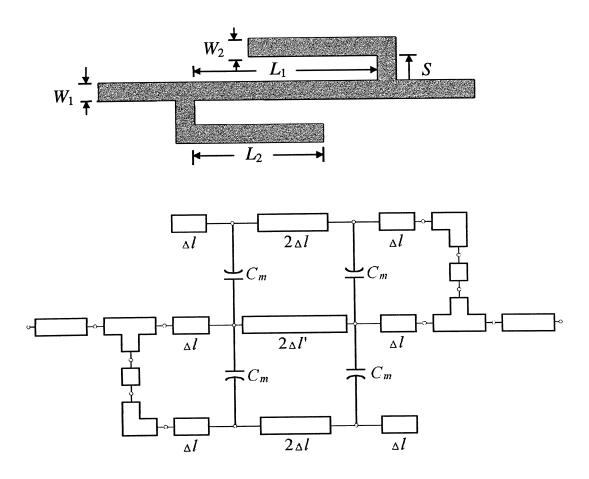
the second phase design



the optimal fine model design

Double-Folded Stub Microstrip Filter

(Bandler et al., 1994)



the fine model is the structure simulated by HP HFSS through HP Empipe3D

the coarse model exploits the microstrip line and microstrip T-junction models available in OSA90/hope

the coupling between the folded stubs and the microstrip line is simulated using equivalent capacitors (Walker, 1990)

Double-Folded Stub Microstrip Filter

the folding effect of the stub is included utilizing the bend model (Jansen et al., 1983)

design specifications are

and

$$|S_{21}| \ge -3$$
 dB for $f \le 9.5$ GHz and 16.5 GHz $\le f$

 $|S_{21}| \le -30 \text{ dB}$ for $12 \text{ GHz} \le f \le 14 \text{ GHz}$

 W_1 and W_2 are fixed at 4.8 mil

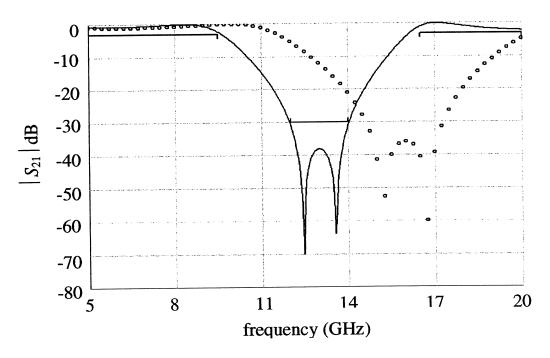
 L_1 , L_2 and S are chosen as optimization variables

the first phase successfully carried out 8 iterations that required 12 fine model simulations

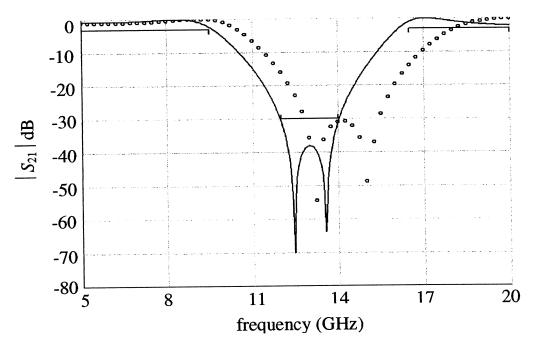
the first phase reached a local minimum for the SM optimization and a switch to the second phase took place

the second phase design is taken as the starting point for the minimax optimizer

Optimization Results for the DFS Filter

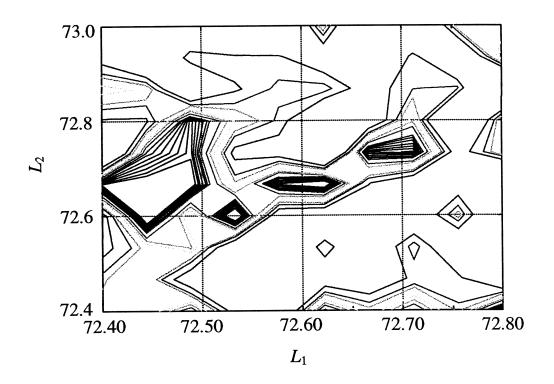


the initial fine model design

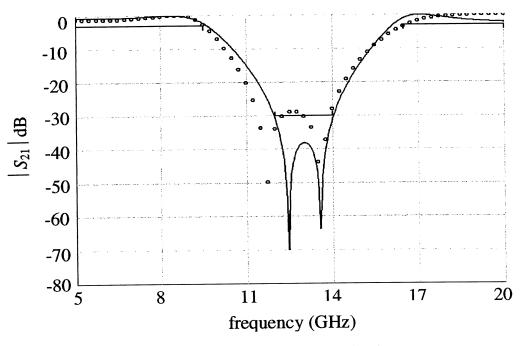


the first phase design

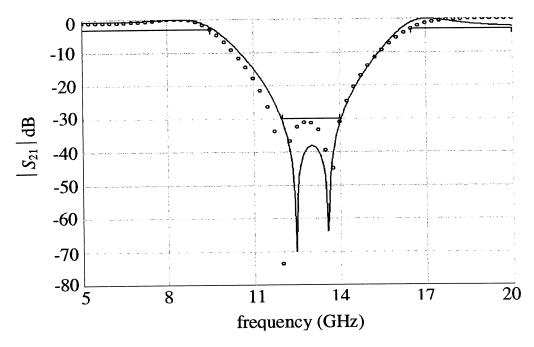
Contours of the Space Mapping Objective Function at the End of the First Phase



Optimization Results for the DFS Filter



the second phase design



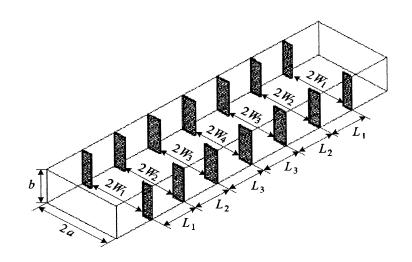
the optimal fine model design

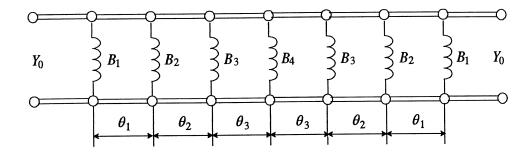


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Six-Section H-Plane Waveguide Filter

(Matthaei et al., 1964)





design specifications are taken as

$$|S_{11}| \le 0.16$$
 for 5.4 GHz $\le f \le 9.0$ GHz

and

$$|S_{11}| \ge 0.85$$
 for $f \le 5.2$ GHz and $|S_{11}| \ge 0.5$ for 9.5 GHz $\le f$

the fine model exploits HP HFSS through HP Empipe3D

a waveguide with a cross-section of 1.372 inches by 0.622 inches (3.485 cm by 1.58 cm) is used

Six-Section H-Plane Waveguide Filter

each septum has a finite thickness of 0.02 inches (0.508 mm)

the coarse model consists of lumped inductances and dispersive transmission line sections

a simplified version of a formula (*Marcuvitz, 1951*) is utilized in evaluating the inductances

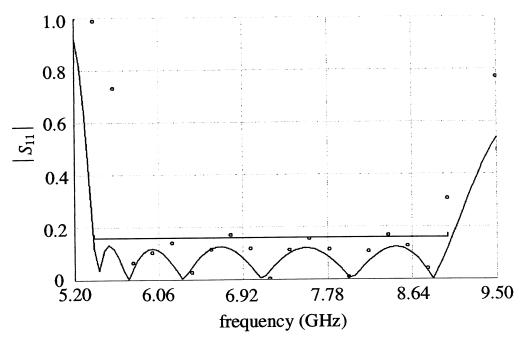
optimizable parameters are the four septa widths W_1 , W_2 , W_3 and W_4 and the three waveguide-section lengths L_1 , L_2 and L_3

the first phase executed 4 iterations requiring a total of 5 fine model simulations

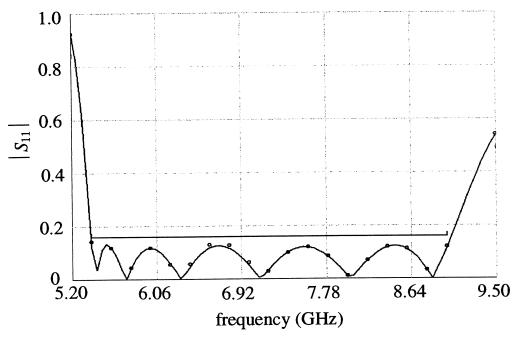
the second phase did not produce successful iterations

the optimal fine model design is obtained using minimax optimization

Optimization Results for the Six-Section H-Plane Filter

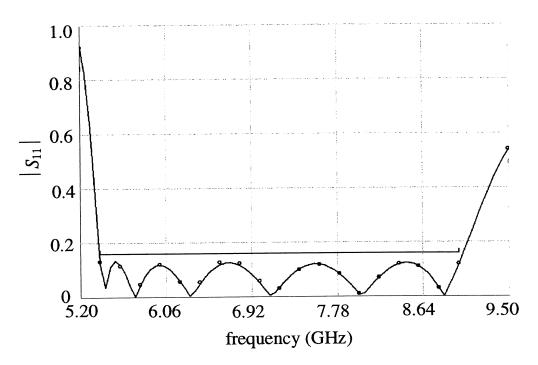


the initial fine model design



the first phase design

Optimization Results for the Six-Section H-Plane Filter

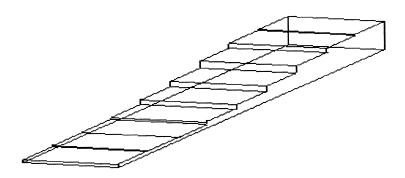


the optimal fine model design



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Seven-Section Waveguide Transformer (*Bandler*, 1969)



the design specifications are taken as

$$vswr \le 1.01$$
 for $1.06 \text{ GHz} \le f \le 1.8 \text{ GHz}$

the fine model is simulated using HP HFSS through HP Empipe3D

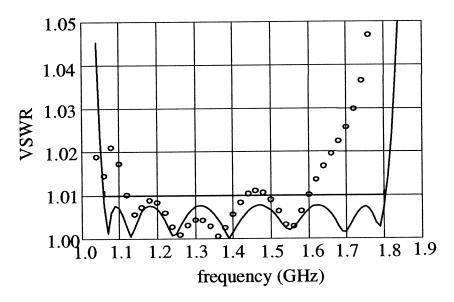
the coarse model is an analytical model which neglects the junction discontinuities

optimizable parameters are the height and length of each waveguide section

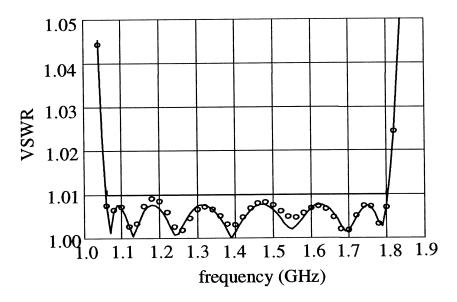
the first phase executed 3 successful iterations that required 6 fine model simulations

the second phase executed 4 iterations

Optimization Results for the Seven-Section Waveguide Transformer

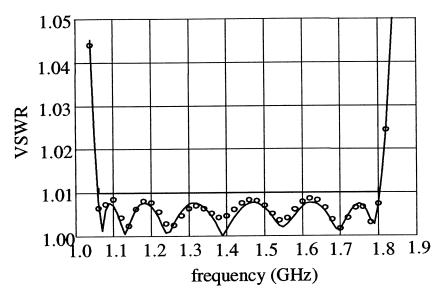


the initial fine model design

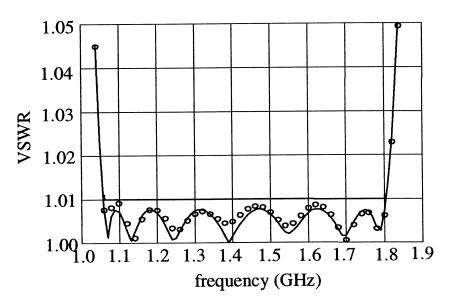


the first phase design

Optimization Results for the Seven-Section Waveguide Transformer



the second phase design



the optimal fine model design

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