A Comparison of Sigma-Point Kalman Filters on an Aerospace Actuator

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ABSTRACT

This paper contains a comparison of several sigma-point Kalman filters, including the unscented Kalman filter (UKF), the cubature Kalman filter (CKF), and the central difference Kalman filter (CDKF). The comparison is based on a simulated electro-hydrostatic actuator, which is commonly used for flight surface actuation in aerospace systems. This brief study compares the response, root mean square error, and the stability of these sigma-point Kalman filters.

Keywords: Sigma point, Kalman filter, unscented, cubature, central-difference, EHA.

1. BRIEF INTRODUCTION

Estimation is the process of extracting useful information from a noisy signal. One of the most well-studied categories within estimation theory is model-based filters, which use models that mimic the system and sensor. Pioneering work in this area is nearly 60 years old, and is the well-known Kalman filter (KF). The KF is a predictor-corrector model-based filter that was developed to minimize estimation error, and is applicable on linear systems and measurements. In this case, the KF yields the optimal estimation assuming the system and measurement models are known and the respective noises are white [1-6].

When the model of the system and/or sensor are/is not linear, the traditional KF cannot be implemented. Several works were developed to modify the KF and to make it applicable to nonlinear systems. These works include the extended KF (EKF), the iterated EKF (IEKF), and higher-order EKF; where these techniques use linearization approaches such as first order Taylor series expansions and Jacobian matrices [7-10]. On the other hand, other types of KFs were developed that use statistical linearization, which is accomplished by weighted linear regression methods. These include the sigma point KF (SPKF), such as the unscented KF (UKF), the cubature KF (CKF; which is a special case of the UKF) and the central difference KF (CDKF) [11-17].

The rest of this brief paper is organized as follows. Three SPKFs are introduced in Section 2. Section 3 describes the electro-hydrostatic actuator, which is the benchmark problem of this work as it is used in aerospace applications. The results are discussed in Section 4 and are concluded Section 5.

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2. THE UNSCENTED, CUBATURE AND CENTER-DIFFERENCE KALMAN FILTERS

The SPKFs linearize the models statistically using sigma points that are drawn from known distributions, and are fused together using certain weights. The UKF, CKF and CDKF are illustrated in Tables 1, 2 and 3, respectively.

$k = 0 \rightarrow Initialize \hat{\mathbf{x}}_{olo}$ and \mathbf{P}_{olo}
$k = 0 \text{Minimize } \mathbf{x}_{0 0} \text{ und } 1_{0 0}$
for $i = 0.1$ 2n
$\int \frac{\partial f(t)}{\partial t} = 0, i = 0$
$\widehat{\mathbf{X}}_{i_{k-1} k-1} = \widehat{\mathbf{x}}_{k-1 k-1} + \begin{cases} 0 & i = 0 \\ \left(\sqrt{nP_{k-1} k-1}\right)_{i}^{T} & 1 \le i \le n \\ \left(\sqrt{nP_{k-1} k-1}\right)_{i}^{T} & 1 \le i \le n \end{cases}, \widehat{\mathbf{X}}_{i_{k} k-1} = \widehat{\mathbf{f}}\left(\widehat{\mathbf{X}}_{i_{k-1} k-1}, u_{k-1}\right)$
$\left(-\left(\sqrt{nP_{k-1 k-1}}\right)_{i} n+1 \le i \le 2n\right)$
end
$\hat{\mathbf{x}}_{k k-1} = \sum_{i=0}^{2n} \frac{1}{2n} \hat{\mathbf{X}}_{i_{k k-1}}, \mathbf{P}_{k k-1} = \sum_{i=0}^{2n} \frac{1}{2n} \left(\hat{\mathbf{X}}_{i_{k k-1}} - \hat{\mathbf{x}}_{k k-1} \right) \left(\hat{\mathbf{X}}_{i_{k k-1}} - \hat{\mathbf{x}}_{k k-1} \right)^T + \mathbf{Q}_{k-1}$
<u>for</u> $i = 0, 1,, 2n$
$ \begin{pmatrix} 0 & i = 0 \\ \hline & & T \end{pmatrix} $
$ \hat{\mathbf{X}}_{i_{k k-1}} = \hat{\mathbf{x}}_{k k-1} + \begin{cases} \left(\sqrt{nP_{k k-1}}\right)_{i} & 1 \le i \le n \\ i \le n \end{cases}, \hat{\mathbf{Z}}_{i_{k k-1}} = \hat{\mathbf{g}}\left(\hat{\mathbf{X}}_{i_{k k-1}}\right) $
$\left(-\left(\sqrt{nP_{k k-1}}\right)_{i}^{T} n+1 \le i \le 2n\right)$
end
$\hat{\mathbf{z}}_{k k-1} = \sum_{i=0}^{2n} \frac{1}{2n} \hat{\mathbf{Z}}_{i_{k k-1}}, \mathbf{P}_{zz} = \sum_{i=0}^{2n} \frac{1}{2n} (\hat{\mathbf{Z}}_{i_{k k-1}} - \hat{\mathbf{z}}_{k k-1}) (\hat{\mathbf{Z}}_{i_{k k-1}} - \hat{\mathbf{z}}_{k k-1})^T + \mathbf{R}_k$
$\mathbf{P}_{xz} = \sum_{i=0}^{2n} \frac{1}{2n} \Big(\hat{\mathbf{X}}_{i_{k k-1}} - \hat{\mathbf{x}}_{k k-1} \Big) \Big(\hat{\mathbf{Z}}_{i_{k k-1}} - \hat{\mathbf{z}}_{k k-1} \Big)^{T}$
$\mathbf{K}_{k} = \mathbf{P}_{xz} \mathbf{P}_{zz}^{-1}, \hat{\mathbf{x}}_{k k} = \hat{\mathbf{x}}_{k k-1} + \mathbf{K}_{k} (\mathbf{z}_{k} - \hat{\mathbf{z}}_{k k-1}), \mathbf{P}_{k k} = (\mathbf{P}_{k k-1} - \mathbf{K}_{k} \mathbf{P}_{zz} \mathbf{K}_{k}^{T})$
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Table 1. The pseudocode for the UKF code, as per [7].

Table 2. The pseudocode for the CKF code, as per [7].

$$\begin{split} k &= 0 \rightarrow Initialize \ \hat{\mathbf{x}}_{0|0} \ and \ \mathbf{P}_{0|0} \\ \text{Start } k &= k+1 \\ for \ i &= 0, 1, \dots, 2n \\ \hline \\ \widehat{\mathbf{X}}_{i_{k-1|k-1}} &= \widehat{\mathbf{x}}_{k-1|k-1} + \begin{cases} 0 & i = 0 \\ \left(\sqrt{nP_{k-1|k-1}}\right)_{i}^{T} & 1 \leq i \leq n \\ -\left(\sqrt{nP_{k-1|k-1}}\right)_{i}^{T} & n+1 \leq i \leq 2n \end{cases}, \quad \widehat{\mathbf{X}}_{i_{k|k-1}} &= \widehat{\mathbf{f}}\left(\widehat{\mathbf{X}}_{i_{k-1|k-1}}, u_{k-1}\right) \\ end \\ \widehat{\mathbf{x}}_{k|k-1} &= \sum_{i=0}^{2n} \frac{1}{2n} \widehat{\mathbf{X}}_{i_{k|k-1}}, \quad \mathbf{P}_{k|k-1} &= \frac{1}{2n} \sum_{i=1}^{2n} \left(\widehat{\mathbf{X}}_{i_{k|k-1}} \widehat{\mathbf{X}}_{i_{k|k-1}}^{T} - \widehat{\mathbf{x}}_{k|k-1} \widehat{\mathbf{x}}_{k|k-1}^{T}\right) + \mathbf{Q}_{k-1} \end{split}$$

$$\frac{for \ i = 0, 1, ..., 2n}{\hat{\mathbf{X}}_{i_{k|k-1}} = \hat{\mathbf{x}}_{k|k-1} + \begin{cases} 0 & i = 0\\ \left(\sqrt{nP_{k|k-1}}\right)_{i}^{T} & 1 \le i \le n\\ -\left(\sqrt{nP_{k|k-1}}\right)_{i}^{T} & n+1 \le i \le 2n \end{cases}}, \quad \hat{\mathbf{Z}}_{i_{k|k-1}} = \hat{\mathbf{g}}\left(\hat{\mathbf{X}}_{i_{k|k-1}}\right)$$
end
$$\hat{\mathbf{z}}_{k|k-1} = \sum_{i=0}^{2n} \frac{1}{2n} \hat{\mathbf{Z}}_{i_{k|k-1}}, \quad \mathbf{P}_{zz} = \frac{1}{2n} \sum_{i=0}^{2n} \left(\hat{\mathbf{Z}}_{i_{k|k-1}} \hat{\mathbf{Z}}_{i_{k|k-1}}^{T} - \hat{\mathbf{z}}_{k|k-1} \hat{\mathbf{z}}_{k|k-1}^{T}\right) + \mathbf{R}_{k}$$

$$\mathbf{P}_{xz} = \frac{1}{2n} \sum_{i=0}^{2n} \left(\hat{\mathbf{X}}_{i_{k|k-1}} \hat{\mathbf{Z}}_{i_{k|k-1}}^{T} - \hat{\mathbf{x}}_{k|k-1} \hat{\mathbf{z}}_{k|k-1}^{T}\right)$$

$$\mathbf{K}_{k} = \mathbf{P}_{xz} \mathbf{P}_{zz}^{-1}, \quad \hat{\mathbf{x}}_{k|k} = \hat{\mathbf{x}}_{k|k-1} + \mathbf{K}_{k} \left(\mathbf{z}_{k} - \hat{\mathbf{z}}_{k|k-1}\right), \quad \mathbf{P}_{k|k} = \left(\mathbf{P}_{k|k-1} - \mathbf{K}_{k} \mathbf{P}_{zz} \mathbf{K}_{k}^{T}\right)$$
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 Table 3. Pseudocode of the CDKF from [7]

$$\begin{split} & k = 0 \rightarrow Initialize \ \hat{\mathbf{x}}_{0|0} \ and \ \mathbf{P}_{0|0} \\ & \text{Start } k = k + 1 \\ & for \ i = 0, 1, ..., 2n \\ & \mathbf{x}_{k|k-1} = \hat{\mathbf{x}}_{k-1|k-1} + \left\{ \begin{array}{l} \left(\sqrt{3\mathbf{P}_{k-1|k-1}} \right)_{i}^{T} & 1 \leq i \leq n \\ \left(\sqrt{3\mathbf{P}_{k-1|k-1}} \right)_{i}^{T} & 1 \leq i \leq n \\ -\left(\sqrt{3\mathbf{P}_{k-1|k-1}} \right)_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \ \hat{\mathbf{x}}_{i_{k|k-1}} = \mathbf{f} \left(\hat{\mathbf{x}}_{i_{k-1}|k-1}, u_{k-1} \right) \\ & end \\ & \hat{\mathbf{x}}_{k|k-1} = \sum_{i=0}^{2n} \left[\hat{\mathbf{x}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{i} & i = 0 \\ \frac{1}{6} & i \neq 0 \end{array} \right], E_{i} = \hat{\mathbf{x}}_{i_{k|k-1}} - \hat{\mathbf{x}}_{i+n_{k|k-1}}, D_{i} = \hat{\mathbf{x}}_{i_{k|k-1}} + \hat{\mathbf{x}}_{i+n_{k|k-1}} - 2\hat{\mathbf{x}}_{0_{k|k-1}} \\ & \mathbf{P}_{k|k-1} = \sum_{i=1}^{n} \frac{1}{12} E_{i} E_{i}^{T} + \sum_{i=1}^{n} \frac{1}{18} (D_{i} D_{i}^{T}) + \mathbf{Q}_{k-1} \\ & \frac{for \ i = 0, 1, ..., 2n}{\hat{\mathbf{x}}_{i_{k|k-1}} = \hat{\mathbf{x}}_{k|k-1}} + \left\{ \begin{array}{l} \left(\sqrt{3\mathbf{P}_{k|k-1}} \right)_{i}^{T} & 1 \leq i \leq n \\ -\left(\sqrt{3\mathbf{P}_{k|k-1}} \right)_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & \hat{\mathbf{z}}_{k|k-1} = \sum_{i=0}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{\sqrt{3\mathbf{P}_{k|k-1}}} \right]_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & end \\ & \hat{\mathbf{z}}_{k|k-1} = \sum_{i=0}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{\sqrt{3\mathbf{P}_{k|k-1}}} \right]_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & \mathbf{z}_{k|k-1} = \sum_{i=0}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{\sqrt{3\mathbf{P}_{k|k-1}}} \right\}_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & \mathbf{z}_{k|k-1} = \sum_{i=0}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{\sqrt{3\mathbf{P}_{k|k-1}}} \right\}_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & \mathbf{z}_{k|k-1} = \sum_{i=0}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{\sqrt{3\mathbf{P}_{k|k-1}}} \right\}_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & \mathbf{z}_{k|k-1} = \sum_{i=1}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} \times \left\{ \frac{3-n}{\sqrt{3\mathbf{P}_{k|k-1}}} \right\}_{i}^{T} & n+1 \leq i \leq 2n \end{array}, \\ & \mathbf{z}_{k|k-1} = \sum_{i=1}^{2n} \left[\hat{\mathbf{z}}_{i_{k|k-1}} + \hat{\mathbf{z}}_{i-1} \frac{1}{18} (D_{i} D_{i}^{T}) + \mathbf{R}_{k}, \quad \mathbf{P}_{xz} = \frac{1}{2} \sqrt{\frac{\mathbf{P}_{k|k-1}}{3}} \left(\left[\hat{\mathbf{z}}_{i_{k|k-1}}^{T} + \hat{\mathbf{z}}_{i+n_{k|k-1}} - 2\hat{\mathbf{z}}_{0_{k|k-1}} \right] \right) \\ & \mathbf{K}_{k} = \mathbf{P}_{xz} \mathbf{P}_{xz}^{-1}, \quad \mathbf{x}_{k|k} = \hat{\mathbf{x}_{k|k-1}} + \mathbf{K}_{k} (\mathbf{z}_{k} - \hat{\mathbf{z}_{k|k-1}}), \quad \mathbf{P}_{k|k} = \left(\mathbf{P}_{k|k-1} - \mathbf{K}_{k} \mathbf{P}_{xz} \mathbf{K}_{x}^{T} \right) \end{aligned}$$

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3. MATHEMATICAL MODELS FOR THE EHA STUDY

In this section, the aforementioned algorithms are applied to the electro-hydrostatic actuator (EHA) shown in Fig. 1. This type of device is used in several applications including aerospace for flight surface actuation. It is used to control components of a wing including the spoiler, aileron, flaps, elevator, and rudder [18]. The EHA model equations are defined as follows [18][19]:

$$\mathbf{x}_{k+1} = \begin{bmatrix} x_1 + T_s x_2 \\ x_2 + T_s x_3 \\ x_2 + T_s x_3 \\ x_3 - T_s \begin{bmatrix} \frac{a_2 V_0 + M \beta_e L}{M V_0} x_3 + \frac{(A_E^2 + a_2 L) \beta_e}{M V_0} x_2 \\ + \frac{2a_1 V_0 x_2 x_3 + \beta_e L (a_1 x_2^2 + a_3)}{M V_0} sgn(x_2) \end{bmatrix} + T_s \frac{A_E \beta_e}{M V_0} u_k \\ \frac{1}{A_E} (a_2 x_2 + (a_1 x_2^2 + a_3) sgn(x_2)) \end{bmatrix}_{\mathbf{k}}$$
(1)

Where we have the following

T _s	0.001 sec	М	7.3760	<i>a</i> ₁	83108
A_E	1.52×10^{-3}	β_e	2.07×10^{8}	<i>a</i> ₂	2100
V ₀	1.08×10^{-3}	L	4.8×10^{-12}	<i>a</i> ₃	512

In this case, the first and fourth states (position and differential pressure) are measured.



Figure 1. The EHA experimental setup at McMaster University [18][19].

4. SIMULATION RESULTS

The setup from Section 3 was used. The sampling time was 0.1 seconds. Four scenarios are considered:

- 1. Case 1: No modeling uncertainties and low noise level.
- 2. Case 2: No modeling uncertainties and high noise level.
- 3. Case 3: With modeling uncertainties (assuming β_e is 5000 times its value) and low noise level.
- 4. Case 4: With modeling uncertainties (assuming β_e is 5000 times its value) and high noise level.

The results of these cases are presented in Tables 4 to 7, and Figures 2 to 5. The results reveal that the UKF has similar results as the CKF. These two filters have superior performance compared to CDKF and EKF. Moreover, CDKF has better performance than the EKF which reinforces the fact that sigma point approximations are more accurate than linearization. Increasing the noise level makes the performance worse, particularly for the non-measured states (2 and 3). In this case, the root mean square error (RMSE) increased between 10 to 100 times. When modelling uncertainties are injected, the RMSE increased from 10 to 10^7 times which could be catastrophic for aerospace systems. This is further magnified when the noise level is increased.

	RMSE				
rnter	Position × 10 ¹¹	Velocity × 10 ⁹	Acceleration × 10 ⁴	Pressure × 10 ⁴	
EKF	2.63	67.2	56.9	1.92	
UKF	2.47	1.63	1.46	1.92	
CKF	2.47	1.63	1.46	1.92	
CDKF	2.48	1.50	1.58	1.92	

Table 3. RMSE results for Case 1.

Table 4. RMSE results for Case 2.

Eller	RMSE				
Filter	Position × 10 ⁹	Velocity × 10 ⁷	Acceleration $\times 10^3$	Pressure× 10 ²	
EKF	7.23	12.0	4.73	1.92	
UKF	7.23	3.48	1.31	1.92	
CKF	7.23	3.48	1.31	1.92	
CDKF	7.22	3.48	1.32	1.92	

	RMSE				
Filter	Position × 10 ¹⁰	osition × 10 ¹⁰ Velocity × 10 ⁵		Pressure × 10 ⁴	
EKF	4.32	8.22	3.84	1.92	
UKF	4.34	8.47	3.07	1.92	
CKF	4.34	8.47	3.07	1.92	
CDKF	4.34	8.47	3.07	1.92	

Table 3. RMSE results for Case 3.

Table 4. RMSE results for Case 4.

	RMSE				
Filter	Position × 10 ⁹	Position × 109Velocity × 104		Pressure × 10 ²	
EKF	2.27	1.30	3.88	1.92	
UKF	2.27	1.35	3.09	1.92	
CKF	2.27	1.35	3.09	1.92	
CDKF	2.27	1.35	3.09	1.92	



Figure 2. State estimation for Case 1.



Figure 3. State estimation for Case 2.



Figure 4. State estimation for Case 3.



Figure 5. State estimation for Case 4.

5. CONCLUSIONS

In this work, a comparison between UKF, CKF, CDKF and EKF estimation strategies was conducted. A simulation based on a real experiment setup of the EHA was used as a benchmark problem. The results of the simulation demonstrate that all four filters were able to successfully estimate the states given a known input. The UKF and CKF yielded similar performances and they provided the best estimates among the other filters. This was followed by CDKF and then finally EKF. When modeling uncertainties were injected, the error significantly increased. Future work will look at studying these filters as applied on an experimental setup.

6. APPENDIX

The following table summarizes the main nomenclature used in this paper.

Table 5. List of nomenclature [18][19].

- -1 *T* Inverse, and transpose, respectively.
- $(\mathbf{a})_i$ The *i* row of **a**.
- $\mathbf{e}_{\mathbf{m}}$ The estimation error vectors in \mathbf{m} .
- **f**(.) The system's model function.
- **g**(.) The sensor's model function.

- **P**_{zz} The output's error covariance matrix.
- **P** The error covariance matrix.
- *q* The number of the sigma points.
- **Q** The process noise covariance matrix.
- **R** The measurements noise covariance matrix.

i,j	Subscripts used to identify elements.	Σ	The summation operator.
$\mathbf{I}_{n \times n}$	The identity matrix with dimensions of $n \times n$.	T_s	Sampling time, and is equal to 0.001 sec.
k	Time step value.	v , w	The measurement and system noise, respectively.
k k-1	The a priori value at time k.	W_i	The assigned weight.
k k	The a posteriori value at time k.	х	The state vector.
\mathbf{K}_X	The correction gain of the filter X .	z	The output vector.
m,n	Number of measurements and states, respectively.	X _i and Z _i :	The estimate and its measurement for the i^{th} sigma point, respectively.
\mathbf{P}_{xx}	The state's error covariance matrix.		
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