

ESTIMATING COMPONENT FAILURE RATES AND YIELDS

ESTIMATION METHODS FOR DETERMINING FAILURE RATES
OF COMPONENT FAMILIES FROM OBSERVED FAILURE RATES OF UNITS
AND
YIELDS OF COMPONENT FAMILIES FROM OBSERVED YIELDS OF UNITS

By

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of Units

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ABSTRACT

In the field of communications electronic plug-in units operating together form a system. In the event of failure a plug-in unit can easily be replaced by another. Each unit consists of electronic components soldered onto a board in a particular pattern. A component may be either a single electronic part such as a transistor or a combination of single parts such as an integrated circuit. Electronic components with similar properties have been grouped into families. This reduces the number of parameters to be estimated from the observations available.

The method of maximum likelihood is used to estimate the failure rates of component families. The number of unit failures and the number of units in use observed during measured periods of time and the component family makeup of the observed units are used to make the estimates.

The probability of an electronic component from a given component from a given family being acceptable after the production process will be referred to as the component yield for that family. Similarly, the probability of a given type of unit being acceptable after the production process will be referred to as the yield for that type of unit. By taking the logarithms of the yields, the estimation problem can be reduced to the linear problem of estimating logarithms of component family yields. Using unit yields, the total

number of each type of unit produced, and the component family makeup of those units produced, component family yields are estimated. The method of maximum likelihood is applied directly to the data and the method of weighted least squares is applied to the linearized problem.

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CHAPTER 1

INTRODUCTION

One of the tasks of a reliability engineer in the communications industry is prediction. If the yield of electronic units from the production line can be predicted, producers can better predict production costs and hence determine a selling price for their products. If the reliability of a newly designed electronic unit can be predicted, purchasers of the units can be given estimates of their maintenance costs. Knowledge of the component family yields and component family reliabilities would make these predictions possible.

Components within an electronic unit may either be in series or in parallel. In the case of components in series, a component failure will cause a break in the circuit thereby resulting in a unit failure. When a component which is parallel with another fails the circuit is not broken and hence the unit continues to function. Parallel components are sometimes installed in order to lengthen the lifetime of an electronic circuit. Designers of electronic plug-in units tend to avoid parallel components because a plug-in unit can be easily replaced, parallel components add to the cost of production, and the lifetime of a unit is not greatly prolonged by the addition of extra components. It is therefore reasonable to assume that components within units are in series.

CHAPTER 2

FAILURE RATES OF COMPONENT FAMILIES FROM UNIT FAILURE RATES

2.1 Introduction

The reliability of an electronic unit can be estimated if the unit has been in service for a length of time, but no adequate method has been developed for predicting the reliability of a newly designed unit. If estimates of component family reliabilities were available this would be possible. When units from the field are serviced, a list of those components replaced can be obtained. Unfortunately no differentiation is made between those components which have been removed because of failure and those removed as trouble shooting aids. As a result, no direct method of estimating component reliabilities is available. Testing of the reliability of electronic components under actual operating conditions is costly in terms of both time and money. Accelerated testing, where components are tested at their highest ratings of temperature and humidity have been done. However, in the tests, chemical reactions which occur within components at different temperatures and humidities make the results difficult to apply. Tests of the reliability of electronic components have been done in the aircraft industry but cannot be applied because of the effect of vibration as well as different temperature and humidity conditions. For purposes of prediction, a method of estimating component family

reliabilities is needed by reliability engineers.

Units within a system can be assumed to operate independently. The failure of one unit does not damage another unit or cause another unit to fail. The same assumption can be made for individual components since those components which have failed or have been damaged as a result of the original component failure are replaced along with the original component which failed. Unfortunately damage to components cannot always be detected. Component failures are assumed to follow a Poisson process with a constant failure rate. With a constant failure rate, components can be replaced without affecting the model.

2.2 Method of Maximum Likelihood

Consider N distinct types of electronic units produced using components from M distinct component families. Since components are Poisson:

$$P[z \text{ components of type } j \text{ failing in time } t] = \frac{e^{-\alpha_j t} (\alpha_j t)^z}{z!} \quad (j=1, \dots, M),$$

where α_j is the constant failure rate of a component of type j .

Since component failures are independent and components are in series:

$$\lambda_i = \sum_{j=1}^M \alpha_j q_{ij} \quad (i=1, \dots, N),$$

where λ_i is the constant failure rate of a unit of type i and q_{ij} is the number of components of type j in a unit of type i .

The total number of units of a particular type in actual use and the total number in the field may vary from one time period to

another. As a result, the expected number of failures may differ from one period to another. Let Y_{ik} be the random variable denoting the number of failures of a unit of type i during the k^{th} time period. Then Y_{ik} is Poisson with parameter ϕ_{ik} where:

$$\phi_{ik} = \gamma_{ik} n_{ik} t_k \lambda_i \quad (i=1, \dots, N; k=1, \dots, K);$$

and γ_{ik} is the proportion of the units of type i in the field actually used during the k^{th} time period, n_{ik} is the total number of units of type i in the field during the k^{th} time period, and t_k is the length of the k^{th} time period.

The likelihood function L can now be set up:

$$L(\alpha_1, \dots, \alpha_M | y_{11}, \dots, y_{NK}) = \prod_{i=1}^N \prod_{k=1}^K \frac{e^{-\phi_{ik}} \phi_{ik}^{y_{ik}}}{y_{ik}!}.$$

Maximizing the likelihood is equivalent to maximizing the logarithm of the likelihood:

$$\log L(\alpha_1, \dots, \alpha_M | y_{11}, \dots, y_{NK}) = \sum_{i=1}^N \sum_{k=1}^K \{y_{ik} \log \phi_{ik} - \phi_{ik} - \log(y_{ik}!)\}.$$

To maximize $\log L$, its derivatives are taken with respect to the parameters α_s ($s=1, \dots, M$) and set equal to zero. Since:

$$\phi_{ik} = \gamma_{ik} n_{ik} t_k \sum_{j=1}^M \alpha_j q_{ij} \quad (i=1, \dots, N; k=1, \dots, K),$$

it follows that:

$$\frac{\partial \phi_{ik}}{\partial \alpha_s} = \gamma_{ik} n_{ik} t_k q_{is} \quad (i=1, \dots, N; k=1, \dots, K; s=1, \dots, M).$$

Hence:

$$\begin{aligned} \frac{\partial \log L}{\partial \alpha_s} &= \sum_{i=1}^N \sum_{k=1}^K \left\{ \frac{y_{ik}}{\phi_{ik}} \frac{\partial \phi_{ik}}{\partial \alpha_s} - \frac{\partial \phi_{ik}}{\partial \alpha_s} \right\} \\ &= \sum_{i=1}^N \sum_{k=1}^K \left\{ \gamma_{ik} n_{ik} t_k q_{is} \left\{ \frac{y_{ik}}{\phi_{ik}} - 1 \right\} \right\} \quad (s=1, \dots, M). \end{aligned}$$

Set derivatives equal to zero and solve for $\hat{\alpha}_s$ ($s=1, \dots, M$) where $\hat{\alpha}_s$ is the maximum likelihood estimate of the failure rate of a component of the s^{th} component family:

$$\sum_{i=1}^N \sum_{k=1}^K \gamma_{ik} n_{ik} t_k q_{is} \left\{ \frac{y_{ik}}{\sum_{j=1}^M \hat{\alpha}_j q_{ij}} - 1 \right\} = 0 \quad (s=1, \dots, M).$$

The method of scoring (Appendix 1) is used to solve this set of non-linear equations. The information matrix is required for scoring:

$$\begin{aligned} \frac{\partial^2 \log L}{\partial \alpha_t \partial \alpha_s} &= \sum_{i=1}^N \sum_{k=1}^K q_{is} y_{ik} \frac{\partial}{\partial \alpha_t} \left(\frac{1}{\sum_{j=1}^M \alpha_j q_{ij}} \right) \\ &= - \sum_{i=1}^N \sum_{k=1}^K \frac{y_{ik} q_{is} q_{it}}{\left(\sum_{j=1}^M \alpha_j q_{ij} \right)^2} \quad (s=1, \dots, M; t=1, \dots, M), \end{aligned}$$

$$E \left[\frac{-\partial^2 \log L}{\partial \alpha_t \partial \alpha_s} \right] = \sum_{i=1}^N \sum_{k=1}^K \frac{\gamma_{ik} n_{ik} t_k q_{is} q_{it}}{\sum_{j=1}^M \alpha_j q_{ij}} = \mathcal{G}(s, t) \quad (s=1, \dots, M; t=1, \dots, M),$$

$$\hat{\mathcal{G}}(s,t) = \sum_{i=1}^N \sum_{k=1}^K \frac{\gamma_{ik} n_{ik} t_k q_{is} q_{it}}{\sum_{j=1}^M \hat{\alpha}_j q_{ij}} \quad (s=1,\dots,M; t=1,\dots,M).$$

Using the inverse of the estimated information matrix an approximate $100(1-\varepsilon)\%$ confidence interval for the s^{th} component family failure rate is

$$\hat{\alpha}_s \pm z_{\varepsilon/2} \sqrt{\hat{\mathcal{G}}^{-1}(s,s)} \quad (s=1,\dots,M),$$

where $z_{\varepsilon/2}$ is the $100 \varepsilon/2\%$ critical value for the normal distribution and $\hat{\mathcal{G}}^{-1}(s,s)$ is the (s,s) entry of the inverse of the estimated information matrix.

Unit failure rates can now be predicted using our estimated component family failure rates:

$$\hat{\lambda}_0 = \sum_{j=1}^M \hat{\alpha}_j q_{0j},$$

where $\hat{\lambda}_0$ is the predicted failure rate of any unit made of components from the M component families for which we estimated failure rates and q_{0j} is the number of components of type j in that unit.

$$\begin{aligned} \text{Var}(\hat{\lambda}_0) &= \text{Var}\left(\sum_{j=1}^M \hat{\alpha}_j q_{0j}\right) \\ &= \sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \text{Cov}(\hat{\alpha}_j, \hat{\alpha}_k) \\ &\approx \sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \mathcal{G}^{-1}(j,k) \\ &\approx \sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \hat{\mathcal{G}}^{-1}(j,k) \end{aligned}$$

Then approximate 100(1-ε)% confidence intervals for the unit failure rates based on the predicted failure rates are:

$$\hat{\lambda}_0 \pm z_{\varepsilon/2} \sqrt{\sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \hat{\mathcal{D}}^{-1}(j,k)}$$

Using the normal approximation to the Poisson distribution, approximate 100(1-ε)% confidence intervals for the unit failure rates based on the observed failure rates are:

$$\sum_{k=1}^K \frac{y_{ik}}{\gamma_{ik} n_{ik} t_k} \pm z_{\varepsilon/2} \sqrt{\sum_{k=1}^K \frac{y_{ik}}{\gamma_{ik} n_{ik} t_k}} \quad (i=1, \dots, N).$$

For those units used to estimate the component family failure rates, the approximate confidence intervals for unit failure rates based on predicted failure rates can be compared with those based on observed failure rates.

An approximate test of fit can be done using the normal approximation to the Poisson distribution. The statistic

$$\sum_{i=1}^N \sum_{k=1}^K \frac{(y_{ik} - \hat{\phi}_{ik})^2}{\hat{\phi}_{ik}} \text{ is asymptotically Chi squared on } N \cdot K - M$$

degrees of freedom.

2.3 Discussion and Recommendations

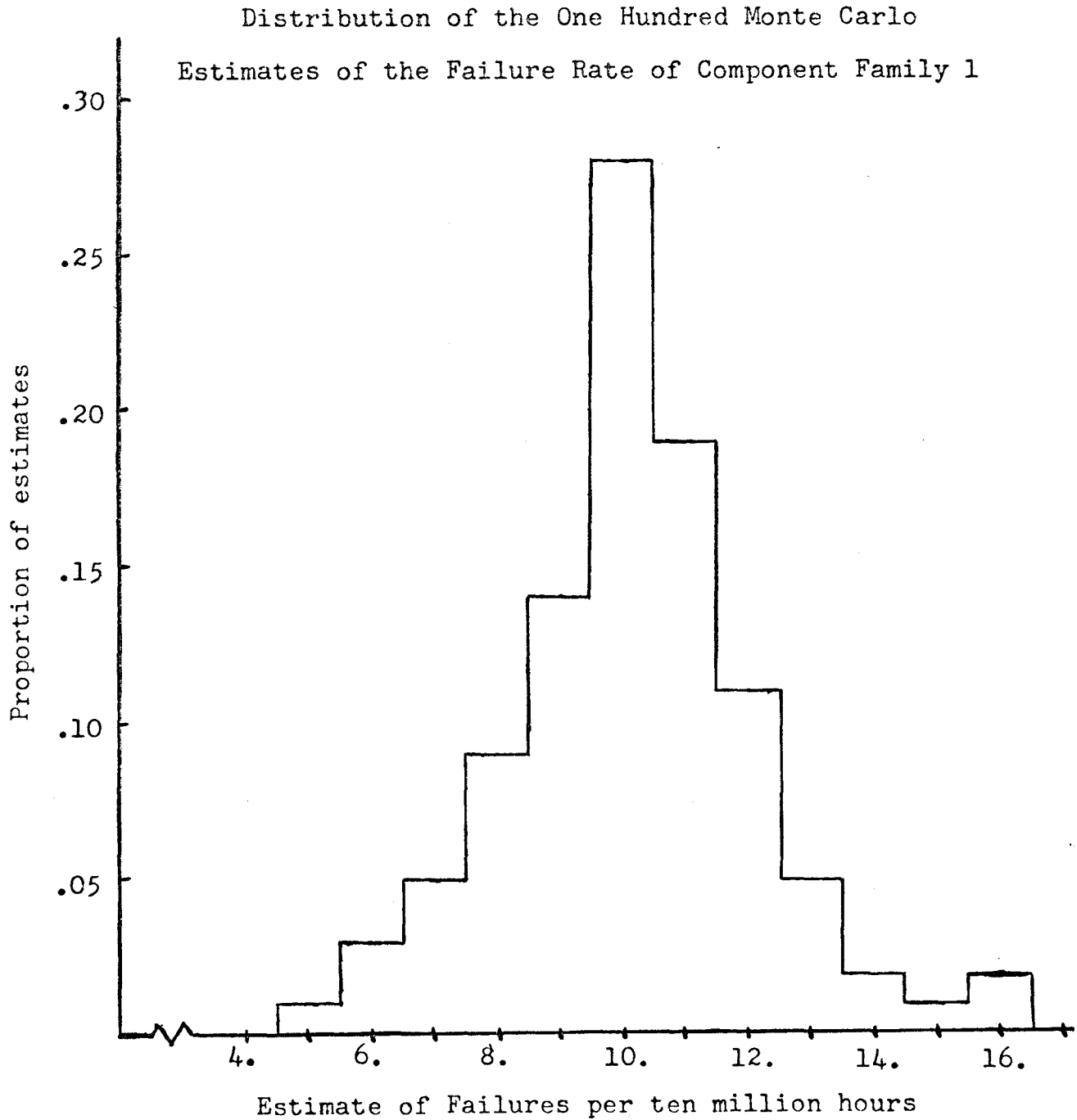
2.3.1 Monte Carlo Study:

Ten distinct artificial units, each made of components from three distinct families with known failure rates, were simulated. Setting the ratio of units in use to the number of units in the field to one, the number of each type of unit in use for a period of five

thousand hours was chosen to represent possible actual conditions. One hundred samples of the number of failures of each of the ten units were randomly generated using the normal approximation to the Poisson distribution. If Y_i is Poisson with mean ϕ_i and variance ϕ_i , then Y_i is approximately normal with mean ϕ_i and variance ϕ_i . Estimates of the component family failure rates and predicted unit failure rates were then made for the one hundred samples using the method of maximum likelihood.

Approximate ninety-five percent confidence intervals for each of the component family failure rate estimates for the one hundred samples were calculated under the assumption that the component family failure rates are approximately normal. The estimates made from the generated unit failure rate data appear to be approximately normal (Figures 1, 2 and 3). Under actual conditions, it can be expected that the same will occur. A likelihood ratio test was used to test equality of the estimated variance-covariance matrix of the one hundred sets of component family failure rates and the inverse of the true information matrix (T.W. Anderson, 1958, Section 10.8). The calculated statistic was 5.16. The five percent Chi-squared critical value on six degrees of freedom is 12.6, meaning that the hypothesis of equality of the two matrices is accepted at the five percent level. Then the use of the inverse of the estimated information matrix in calculating confidence intervals should not affect the level of confidence.

Figure 1

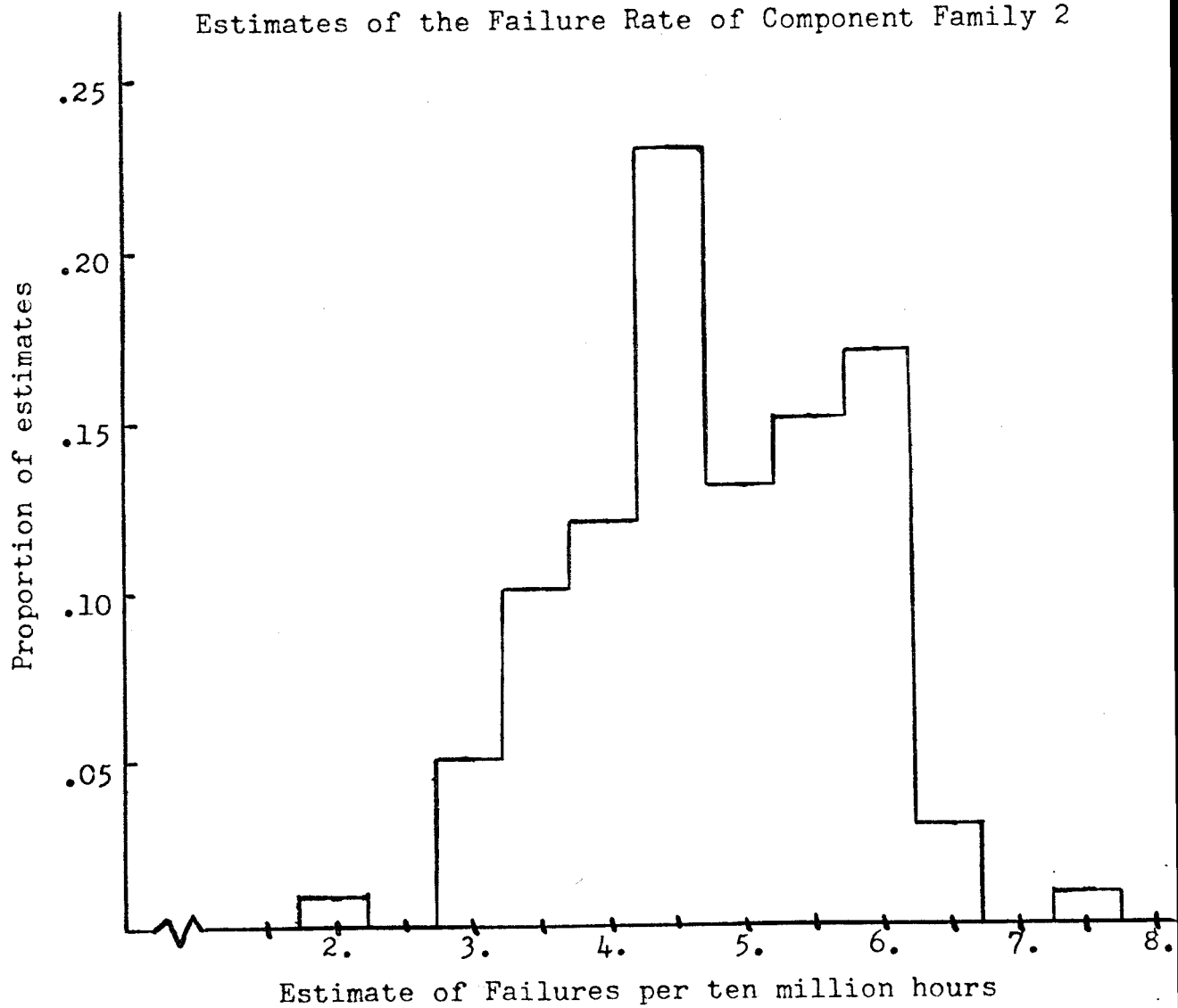


True Value: 10.0 failures/10 million hours

Average of Estimates: 10.166 failures/10 million hours

Figure 2

Distribution of the One Hundred Monte Carlo
Estimates of the Failure Rate of Component Family 2

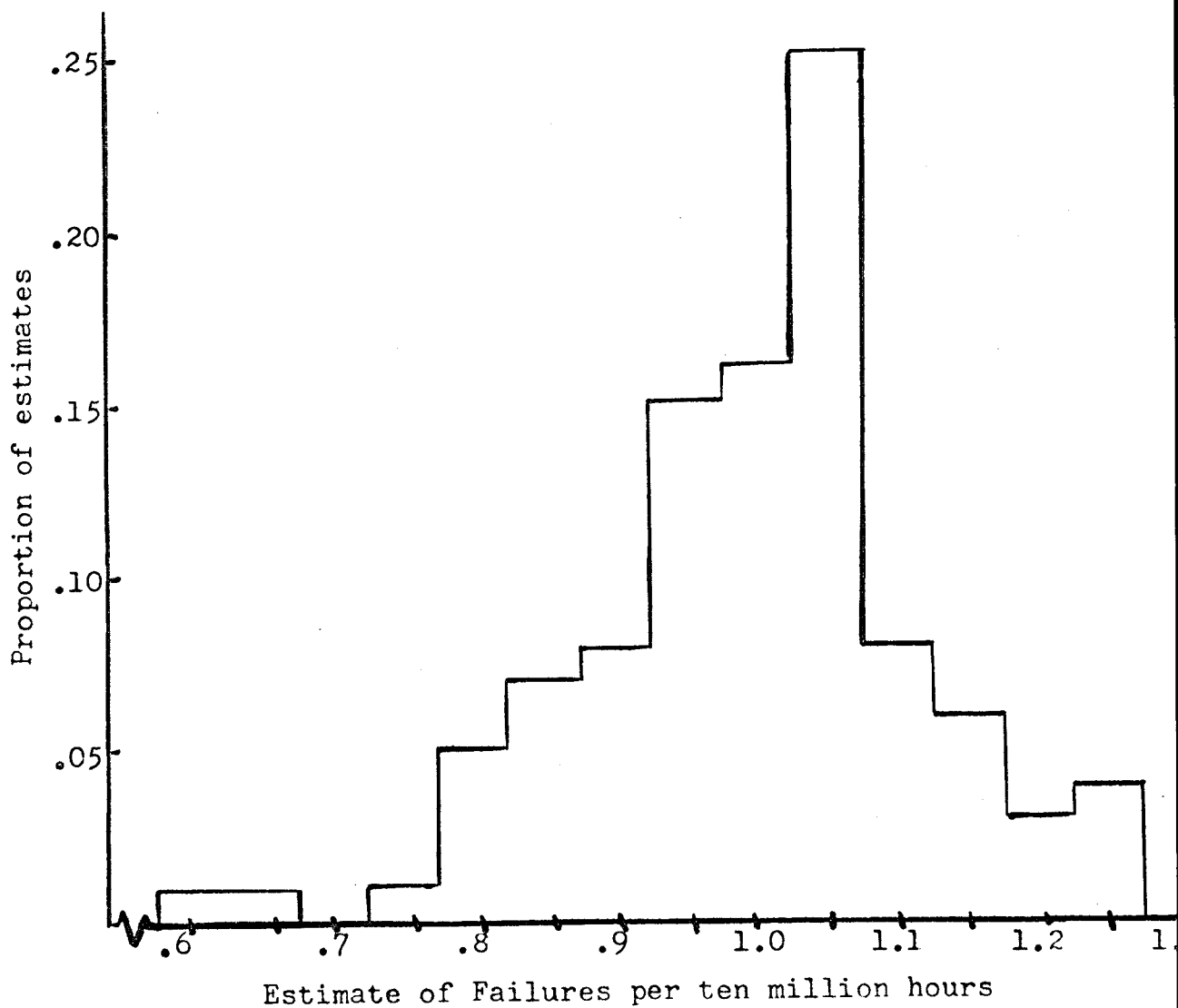


True Value: 5.0 failures/10 million hours

Average of Estimates: 4.830 failures/10 million hours

Figure 3

Distribution of the One Hundred Monte Carlo
Estimates of the Failure Rate of Component Family 3



True Value: 1.0 failures/10 million hours

Average of Estimates: .997 failures/10 million hours

The number of confidence intervals for each family containing the true parameter value indicates that the true level of confidence may be less than ninety-five percent (Table 1). Further Monte Carlo studies with larger samples would allow us to make stronger inferences regarding confidence levels, as the differences between the observed levels of confidence and ninety-five percent may be the result of sampling error.

Since the predicted unit failure rates are linear combinations of the estimates of component family failure rates, it can be expected that predicted unit failure rates will be closer to normal distributions. Evidence of this can be seen from the approximate ninety-five percent confidence intervals for the unit failure rates based on the predicted unit failures. Although still below ninety-five percent, the level of confidence appears to be greater than that for the confidence intervals for component family failure rates. This property will be advantageous when the reliability of a new unit is predicted.

2.3.2 Applications

Information regarding failure rates of electronic units in the field was not available when the computing work was done. As a result, at this time, there is no indication of how well the model fits actual conditions. If unit failure rate data is to be used to estimate component family failure rates, accurate methods of collecting data from users of electronic units must be developed and users must be convinced of the need of accurate data. As the quality

TABLE 1

PERCENTAGE OF APPROXIMATE 95% CONFIDENCE INTERVALS FOR
FAILURE RATES CONTAINING THE TRUE PARAMETER VALUE

COMPONENT FAMILIES

COMPONENT FAMILY	PERCENTAGE CONTAINING TRUE VALUE
1	92%
2	93%
3	93%

CONFIDENCE INTERVALS BASED ON PREDICTED UNIT FAILURE RATES

UNIT	PERCENTAGE CONTAINING TRUE VALUE
1	93%
2	95%
3	95%
4	96%
5	95%
6	95%
7	92%
8	92%
9	96%
10	95%

on incoming information improves, the estimates of component family failure rates should improve.

The method of maximum likelihood was applied to a single set of randomly generated approximately Poisson unit failures for one period of time. Ten distinct units made from components of three distinct families were considered. The test of fit statistic calculated from the predicted unit failure rates and observed failure rates was 6.15. This is less than 14.1, the five percent critical value for the Chi-squared distribution on seven degrees of freedom, indicating that this set of data fits the maximum likelihood model. Different starting values were tried for the iterative scheme. It was found that, for this set of generated failure rate data, the scheme converged quickly for starting values between 10^{-24} and 10^5 failures per ten million hours (Figure 4 and Figure 5). For this set of data the true component family failure rates per ten million hours were ten for the first family, five for the second, and one for the third. This wide range of values for which the method will converge will allow users of the method to proceed without having prior knowledge of approximate failure rates of the components. Future studies of this method, involving randomly generated unit failure rate data, should include more than one period of time.

A lack of sufficient unit failure rate data requires reliability engineers to group components into families. Care must be taken to insure that components are grouped into families of components having the same failure rates. Otherwise, predicted unit

Figure 4

N =	0	ALPHA(1) =	0.10000003E-23
		ALPHA(2) =	0.10000003E-23
		ALPHA(3) =	0.10000003E-23
N =	1	ALPHA(1) =	0.11217773E+02
		ALPHA(2) =	0.45475035E+01
		ALPHA(3) =	0.89707947E+00
N =	2	ALPHA(1) =	0.11386892E+02
		ALPHA(2) =	0.46041603E+01
		ALPHA(3) =	0.88496155E+00
N =	3	ALPHA(1) =	0.11390028E+02
		ALPHA(2) =	0.46050749E+01
		ALPHA(3) =	0.88474065E+00
N =	4	ALPHA(1) =	0.11390099E+02
		ALPHA(2) =	0.46050930E+01
		ALPHA(3) =	0.88473552E+00
N =	5	ALPHA(1) =	0.11390092E+02
		ALPHA(2) =	0.46050930E+01
		ALPHA(3) =	0.88473612E+00
N =	6	ALPHA(1) =	0.11390099E+02
		ALPHA(2) =	0.46050949E+01
		ALPHA(3) =	0.88473552E+00
N =	7	ALPHA(1) =	0.11390090E+02
		ALPHA(2) =	0.46050911E+01
		ALPHA(3) =	0.88473624E+00
N =	8	ALPHA(1) =	0.11390086E+02
		ALPHA(2) =	0.46050873E+01
		ALPHA(3) =	0.88473666E+00

Sequence of Converging Component Family Failure Rate Estimates using 10^{-24}
as Starting Values

Figure 5

N =	0	ALPHA(1) =	0.10000000E+06
		ALPHA(2) =	0.10000000E+06
		ALPHA(3) =	0.10000000E+06
N =	1	ALPHA(1) =	0.16000000E+02
		ALPHA(2) =	0.73750000E+01
		ALPHA(3) =	0.10000000E+01
N =	2	ALPHA(1) =	0.11416687E+02
		ALPHA(2) =	0.46204128E+01
		ALPHA(3) =	0.88267040E+00
N =	3	ALPHA(1) =	0.11390633E+02
		ALPHA(2) =	0.46053104E+01
		ALPHA(3) =	0.88469625E+00
N =	4	ALPHA(1) =	0.11390099E+02
		ALPHA(2) =	0.46050987E+01
		ALPHA(3) =	0.88473541E+00
N =	5	ALPHA(1) =	0.11390092E+02
		ALPHA(2) =	0.46050930E+01
		ALPHA(3) =	0.88473600E+00
N =	6	ALPHA(1) =	0.11390099E+02
		ALPHA(2) =	0.46050949E+01
		ALPHA(3) =	0.88473541E+00
N =	7	ALPHA(1) =	0.11390090E+02
		ALPHA(2) =	0.46050911E+01
		ALPHA(3) =	0.88473612E+00
N =	8	ALPHA(1) =	0.11390087E+02
		ALPHA(2) =	0.46050911E+01
		ALPHA(3) =	0.88473642E+00

Sequence of Converging Component Family Failure Rate Estimates using 10^5
as Starting Values

failure rates are likely to be poor estimates of the true unit failure rates. Results from accelerated tests and from tests in other fields may be of use in grouping components into families.

CHAPTER 3

YIELD OF COMPONENTS FROM THE YIELD OF UNITS

3.1 Introduction:

Faulty components, damage due to handling during production, and failures expected during normal use contribute to newly produced electronic components failing test procedures. A method of estimating the component family yields from the observed yields of units, the total number of each type of unit produced, and the component makeup of the observed units would enable reliability engineers to predict production yields of newly designed units.

The effect of the production process on one particular component is assumed to be independent of the effect on any other component. Hence, the number of acceptable components of a particular type within a particular unit after production will be a binomial observation. Let X_{ij} be a binomial random variable denoting the number of acceptable components of type j in a unit of type i , that is:

$$P[X_{ij} = x_{ij}] = \binom{q_{ij}}{x_{ij}} A_j^{x_{ij}} (1-A_j)^{q_{ij}-x_{ij}}$$
$$(x_{ij}=0, \dots, q_{ij}; j=1, \dots, M; i=1, \dots, N),$$

where q_{ij} is the number of components of type j being acceptable after production, N is the number of distinct types of units to be

used in the estimation procedure, and M is the number of distinct component families found in the N observed units. The probability of a unit of type i being accepted can be expressed as a joint binomial probability, that is:

$$P[X_{i1} = q_{i1}, \dots, X_{iM} = q_{iM}] = \prod_{j=1}^M A_j^{q_{ij}} \quad (i=1, \dots, N).$$

Denote:

$$p_i = \prod_{j=1}^M A_j^{q_{ij}} \quad (i=1, \dots, N).$$

It follows from the independence of the acceptability of components, that units are independently produced. Thus, the number of acceptable units of type i produced during a production period will also be binomial. Denoting by the random variable Y_i , the number of acceptable units produced during a production period, we get:

$$\begin{aligned} P[Y_i = y_i] &= \binom{n_i}{y_i} p_i^{y_i} (1-p_i)^{n_i - y_i} \\ &= \binom{n_i}{y_i} \left[\prod_{j=1}^M A_j^{q_{ij}} \right]^{y_i} \left(1 - \left[\prod_{j=1}^M A_j^{q_{ij}} \right] \right)^{n_i - y_i} \end{aligned} \quad (0 \leq y_i \leq n_i, i=1, \dots, N)$$

It follows that:

$$E \left[\frac{Y_i}{n_i} \right] = p_i \quad (i=1, \dots, N),$$

and:

$$\text{Var} \left[\frac{Y_i}{n_i} \right] = \frac{p_i(1-p_i)}{n_i} \quad (i=1, \dots, N).$$

Then using the normal approximation to the binomial distribution, an approximate $100(1-\epsilon)\%$ confidence interval for a unit of type i is:

$$\frac{y_i}{n_i} \pm z_{\epsilon/2} \sqrt{\frac{\frac{y_i}{n_i} (1 - \frac{y_i}{n_i})}{n_i}} \quad (i=1, \dots, N).$$

3.2 Method of Maximum Likelihood

Consider N distinct types of electronic units produced using components from M distinct component families. Using the distribution of acceptable components produced, the likelihood equation can be set up:

$$L(A_1, \dots, A_M | y_1, \dots, y_N) = \prod_{i=1}^N \binom{n_i}{y_i} \left[\prod_{j=1}^M A_j^{q_{ij}} \right]^{y_i} (1 - \left[\prod_{j=1}^M A_j^{q_{ij}} \right])^{n_i - y_i}$$

Maximizing the likelihood is equivalent to maximizing the logarithm of the likelihood:

$$\begin{aligned} \log L(A_1, \dots, A_M | y_1, \dots, y_N) \\ = \sum_{i=1}^N \left\{ \log \binom{n_i}{y_i} + y_i \sum_{j=1}^M q_{ij} \log A_j + (n_i - y_i) \log (1 - \left[\prod_{j=1}^M A_j^{q_{ij}} \right]) \right\} \end{aligned}$$

To maximize $\log L$, the derivatives with respect to A_s ($s=1, \dots, M$) are found and set equal to zero.

$$\frac{\partial \log L}{\partial A_s} = \sum_{i=1}^N \frac{q_{is} (y_i - n_i \left[\prod_{j=1}^M A_j^{q_{ij}} \right])}{(A_s - A_s \left[\prod_{j=1}^M A_j^{q_{ij}} \right])} \quad (s=1, \dots, M).$$

Set the derivatives equal to zero and solve for \hat{A}_s ($s=1, \dots, M$) where \hat{A}_s is the estimated yield for a component of the s^{th} component family:

$$\sum_{i=1}^N \frac{q_{is}(y_i - n_i [\prod_{j=1}^M \hat{A}_j^{q_{ij}}])}{(\hat{A}_s - \hat{A}_s [\prod_{j=1}^M \hat{A}_j^{q_{ij}}])} = 0 \quad (s=1, \dots, M).$$

The simplex method developed by Nelder and Mead (Appendix 2) is used to solve for the maximum likelihood estimates of the component family yields. This method proved to be preferable to the method of scoring. (See page 37.)

The estimated information matrix is used to estimate confidence intervals:

$$\frac{\partial^2 \log L}{\partial A_t \partial A_s} = \sum_{i=1}^N \frac{q_{is} q_{it} [\prod_{j=1}^M A_j^{q_{ij}}] (y_i - n_i)}{A_s A_t (1 - [\prod_{j=1}^M A_j^{q_{ij}}])^2} \quad (s=1, \dots, M; t=1, \dots, M),$$

$$E \left[\frac{-\partial^2 \log L}{\partial A_t \partial A_s} \right] = \sum_{i=1}^N \frac{n_i q_{is} q_{it} [\prod_{j=1}^M A_j^{q_{ij}}]}{A_s A_t (1 - [\prod_{j=1}^M A_j^{q_{ij}}])} = \mathcal{J}(s, t) \quad (s=1, \dots, M; t=1, \dots, M),$$

$$\hat{\mathcal{J}}(s, t) = \sum_{i=1}^N \frac{n_i q_{is} q_{it} [\prod_{j=1}^M \hat{A}_j^{q_{ij}}]}{A_s \hat{A}_t (1 - [\prod_{j=1}^M \hat{A}_j^{q_{ij}}])} \quad \begin{matrix} (s=1, \dots, M; \\ t=1, \dots, M). \end{matrix}$$

Then an approximate $100(1-\epsilon)\%$ confidence intervals for the s^{th} component family yield is

$$\hat{A}_s \pm z_{\epsilon/2} \sqrt{\hat{\mathcal{J}}^{-1}(s, s)} \quad (s=1, \dots, M),$$

where $z_{\epsilon/2}$ is the $100 \epsilon/2\%$ critical value for the normal distribution and $\hat{\mathcal{J}}^{-1}(s, s)$ is the (s, s) entry of the inverse of the estimated information matrix.

Yields of units can now be predicted using the estimated component family yields:

$$\hat{p}_0 = \prod_{j=1}^M \hat{A}_j^{q_{0j}},$$

where \hat{p}_0 is the predicted yield of any unit made of components from the M component families for which we estimated yields and q_{0j} is the number q_{0j} is the number of components of type j in that unit. The predicted yields of the N units used in the estimation procedure can be compared with the confidence intervals for unit yields based on the observed values.

An approximate test of fit can be performed using the normal approximation to the binomial distribution. The statistic

$$\sum_{i=1}^N \frac{(y_i - n_i \hat{p}_i)^2}{n_i \hat{p}_i (1 - \hat{p}_i)}$$

is asymptotically Chi squared on N-M degrees

of freedom.

3.3 Method of Weighted Least Squares

Consider N distinct types of electronic units produced using components from M distinct component families. Take the logarithm of the yield of a unit of type i:

$$\log p_i = \sum_{j=1}^M q_{ij} \log A_j \quad (i=1, \dots, N).$$

Let Y_i be the random variable for the acceptable number of units produced if a total of n_i units of type i are produced. Then, since the distribution of acceptable units produced is assumed to be binomial the exact mean and variance of Y_i/n_i are known. The exact

variance of $\log(Y_i/n_i)$, however, is unknown but can be approximated.

Let:

$$b\left(\frac{Y_i}{n_i}\right) = \log(Y_i/n_i) \quad (i=1, \dots, N),$$

$$b'\left(\frac{Y_i}{n_i}\right) = \frac{1}{Y_i/n_i} \quad (i=1, \dots, N).$$

By Taylor's Theorem:

$$b\left(\frac{Y_i}{n_i}\right) \approx b(p_i) + \left(\frac{Y_i}{n_i} - p_i\right) b'(p_i),$$

where y_i is an observed value of Y_i .

Then:

$$\begin{aligned} \text{Var}\left[b\left(\frac{Y_i}{n_i}\right)\right] &\approx \{b'(p_i)\}^2 \text{Var}\left[\frac{Y_i}{n_i}\right] \\ &= \left(\frac{1}{p_i}\right)^2 \frac{p_i(1-p_i)}{n_i} \\ &\approx \frac{n_i - y_i}{n_i y_i} \\ &= w_i^2, \text{ say} \quad (i=1, \dots, N). \end{aligned}$$

The method of weighted least squares can be applied:

$$\hat{A} = (Q_*' Q_*)^{-1} Q_*' y_*$$

where:

$$\hat{A} = \begin{bmatrix} \log \hat{A}_1 \\ \vdots \\ \log \hat{A}_M \end{bmatrix}, \quad y_* = \begin{bmatrix} \frac{\log y_1}{w_1} \\ \vdots \\ \frac{\log y_N}{w_N} \end{bmatrix}, \quad Q_* = [q_{ij}/w_i]_{N \times M}.$$

Approximate $100(1-\epsilon)\%$ confidence intervals for the logarithm of the component family yields are:

$$\log \hat{A}_s \pm t_{\varepsilon/2}^{(N-M)} \sqrt{(Q_*' Q_*)^{-1}_{ss} \hat{\sigma}^2} \quad (s=1, \dots, M),$$

where $t_{\varepsilon/2}^{(N-M)}$ is the 100 $\varepsilon/2\%$ critical value for the student's t distribution on $N-M$ degrees of freedom, $(Q_*' Q_*)^{-1}$ is the (s,s) entry of the matrix $(Q_*' Q_*)^{-1}$ and $\hat{\sigma}^2$ is an estimate of the residual variance:

$$\begin{aligned} \hat{\sigma}^2 &= \frac{(y_* - Q_* \hat{A})' (y_* - Q_* \hat{A})}{N-M} \\ &= \frac{y_*' y_* - \hat{A}' Q_*' y_*}{N-M} \end{aligned}$$

By taking the exponent of the bounds of the confidence intervals, approximate 100(1- ε)% confidence intervals for the estimates of the component family yields can be found:

$$\hat{A}_s \exp(\pm t_{\varepsilon/2}^{(N-M)} \sqrt{(Q_*' Q_*)^{-1}_{s,s} \hat{\sigma}^2}) \quad (s=1, \dots, M).$$

Yields of units can now be predicted using the estimates of component family yields:

$$\hat{p}_0 = \prod_{j=1}^M \hat{A}_j^{q_{0j}}$$

where \hat{p}_0 is the predicted yield of any unit composed of components for which estimates have been made and q_{0j} is the number of components of type j in that unit. Since

$$\log \hat{p}_0 = \sum_{j=1}^M q_{0j} \log \hat{A}_j,$$

it follows that:

$$\text{Var}(\log \hat{p}_0) = \text{Var}\left(\sum_{j=1}^M q_{0j} \log \hat{A}_j\right)$$

$$\begin{aligned}
&= \sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \text{Cov}(\log \hat{A}_j, \log \hat{A}_k) \\
&= \sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \hat{\sigma}^2 (Q_*' Q_*)^{-1}_{j,k} .
\end{aligned}$$

Then an approximate 100(1- ϵ)% confidence interval for the predicted yield will be:

$$\hat{P}_0 \cdot \exp(\pm z_{\epsilon/2} \sqrt{\sum_{k=1}^M \sum_{j=1}^M q_{0j} q_{0k} \hat{\sigma}^2 (Q_*' Q_*)^{-1}_{j,k}})$$

The approximate 100(1- ϵ)% confidence intervals for the unit yields based on the predicted yields can be compared with these based on the observed yields.

An approximate test of fit can be performed using the normal approximation to the binomial distribution.

The statistic $\sum_{i=1}^N \frac{(y_i - n_i \hat{p}_i)^2}{n_i \hat{p}_i (1 - \hat{p}_i)}$ is asymptotically Chi squared on

$N-M$ degrees of freedom.

3.4 Discussion and Recommendations

3.4.1 Monte Carlo Study:

Ten distinct artificial units, each made of components from three distinct families with known yields, were simulated. The number of each type of unit produced during a production period was chosen to represent possible actual conditions. One hundred samples of the number of accepted units of each of the ten types were randomly generated using the normal approximation to the binomial distribution. If Y_i is binomial with mean $n_i p_i$ and variance

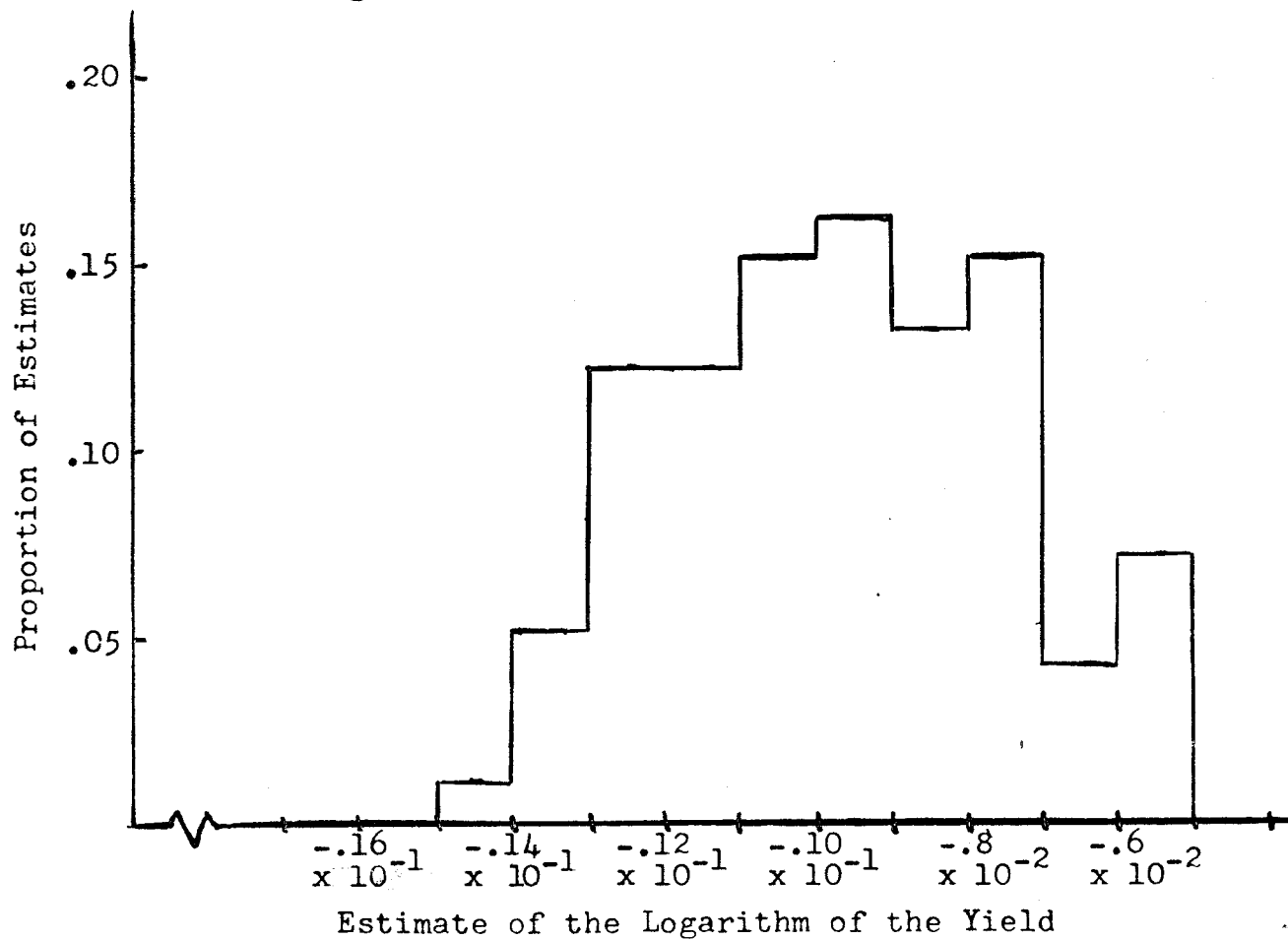
$n_i p_i(1-p_i)$, then Y_i is approximately normal with mean $n_i p_i$ and variance $n_i p_i(1-p_i)$. The method of weighted least squares was then applied to the one hundred samples.

Approximate ninety-five percent confidence intervals for each of the logarithms of the component family yields for the one hundred samples were calculated using the normal approximation commonly used in least squares analyses. The estimates of the logarithms of the component family yields made from the generated unit yield data appear to be approximately normal (Figures 6,7 and 8). Under actual conditions it can be expected that the same will hold true. The number of confidence intervals for each family containing the true parameter value indicates that the true level of confidence may be greater than ninety-five percent (Table 2). One explanation for this may be that the weights used to adjust the component makeup matrix Q were approximate. Another possible explanation may be the non-normality of the linearized unit yield data.

Future studies could try using the information matrix for the linearized problem as the variance-covariance matrix. Confidence intervals using the inverse of this information matrix would not then depend on the adjusted component makeup matrix. To determine this information matrix, let A_1, \dots, A_M be the M component family yields, L be the likelihood function for A_1, \dots, A_M with N observed unit yields, and q_{ij} be the number of components of type j in a unit of type i . It can be shown that:

Figure 6

Distribution of the One Hundred Monte Carlo
Estimates of the Logarithm of the Yield of Component Family 1

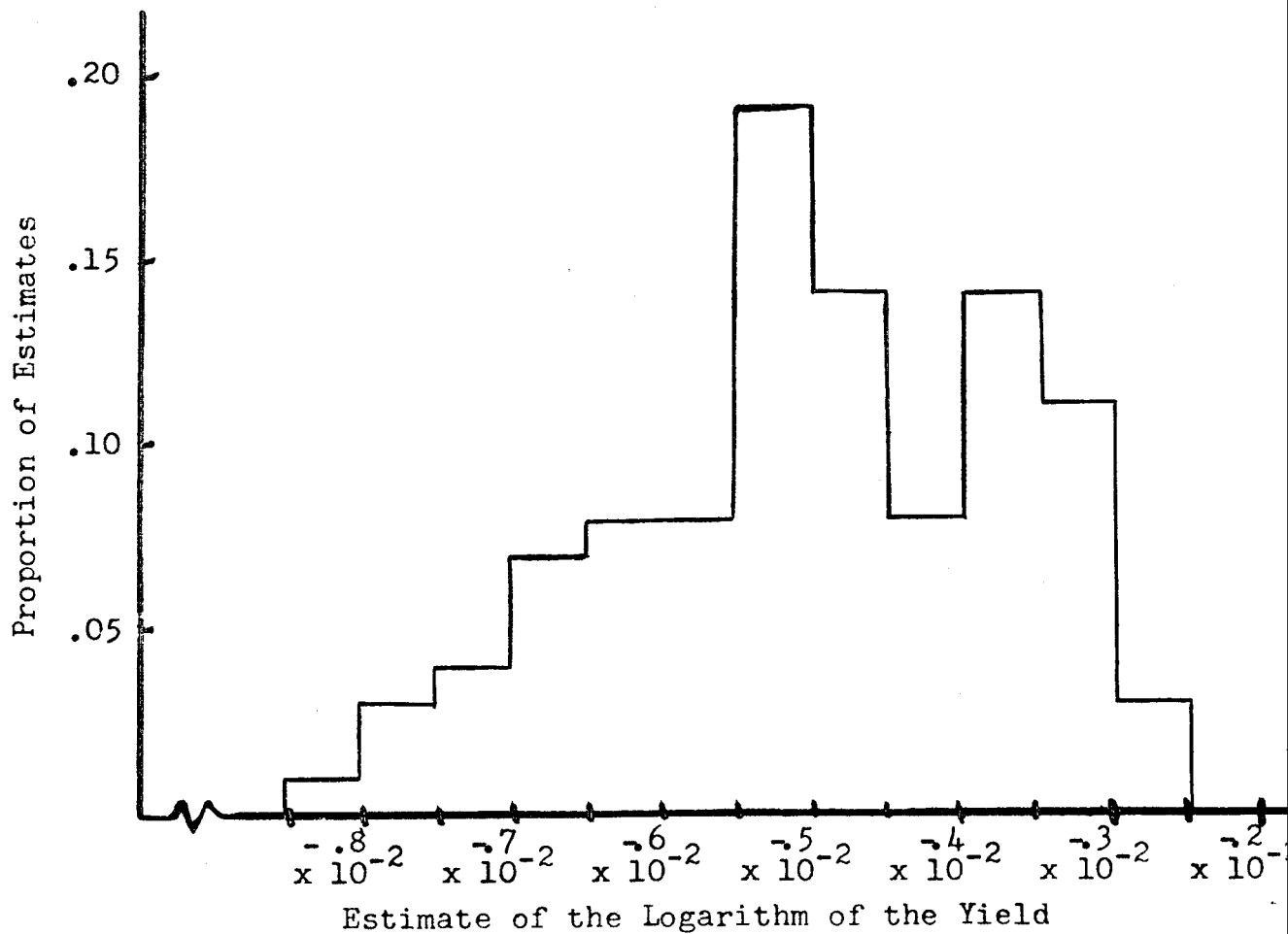


True Value: $\log(.99) = -.100 \times 10^{-1}$

Average of Estimates: $-.97283 \times 10^{-2}$
 $= \log(.99032)$

Figure 7

Distribution of the One Hundred Monte Carlo
Estimates of the Logarithm of the Yield of Component Family 2

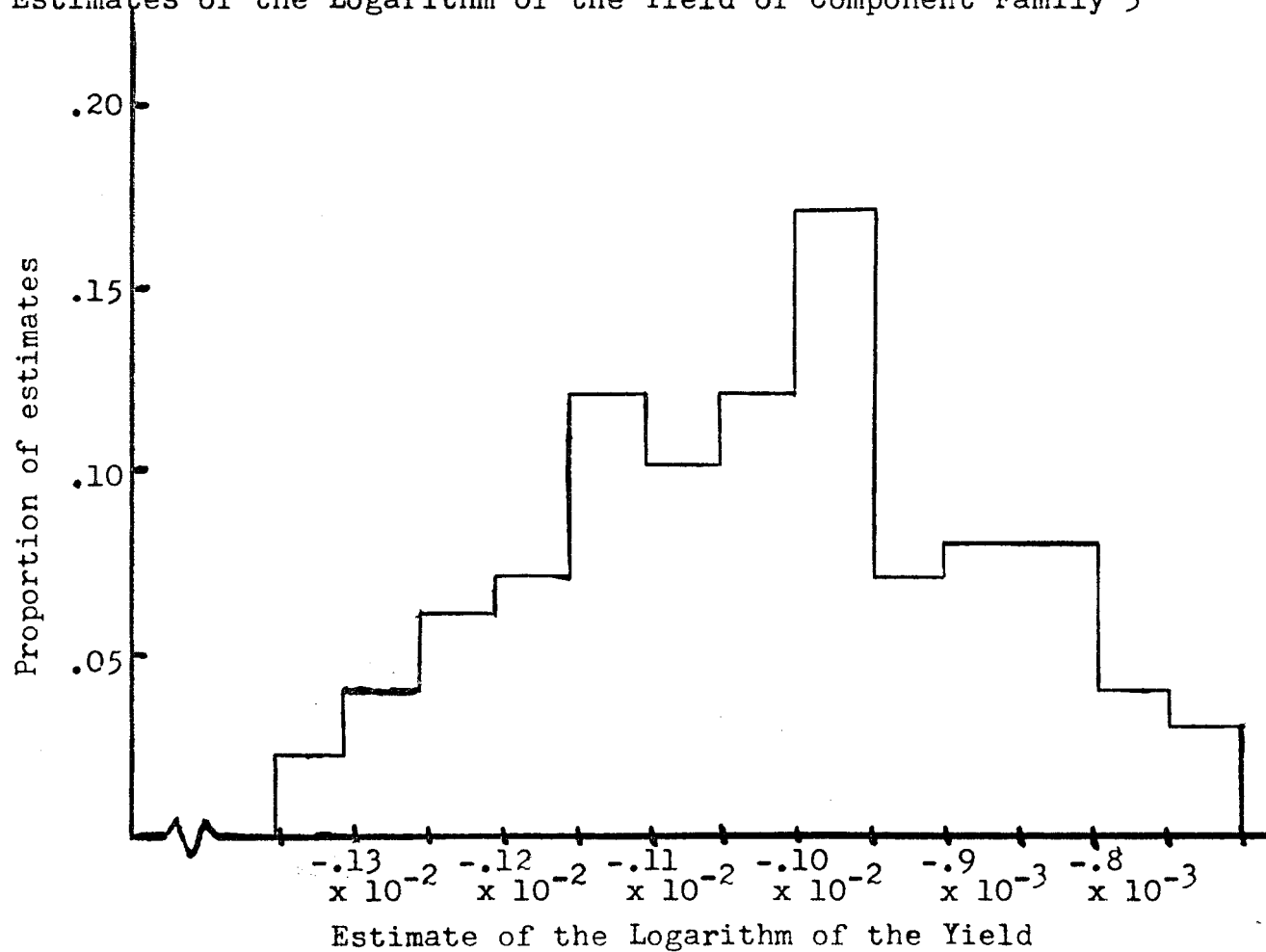


True Value: $\log(.995) = -.50125 \times 10^{-2}$

Average of Estimates: $-.50201 \times 10^{-2}$
 $= \log(.99499)$

Figure 8

Distribution of the One Hundred Monte Carlo
Estimates of the Logarithm of the Yield of Component Family 3



True Value: $\log(.999) = -.10005 \times 10^{-2}$

Average of Estimates: $-.10156 \times 10^{-2}$
 $= \log(.99898)$

TABLE 2

PERCENTAGE OF APPROXIMATE 95% CONFIDENCE INTERVALS FOR
YIELDS CONTAINING THE TRUE PARAMETER VALUE

COMPONENT FAMILIES

COMPONENT FAMILY	PERCENTAGE CONTAINING TRUE VALUE
1	97%
2	99%
3	97%

UNITS (CONFIDENCE INTERVALS BASED ON PREDICTED YIELDS)

UNIT	PERCENTAGE CONTAINING TRUE VALUE
1	96%
2	91%
3	94%
4	91%
5	90%
6	94%
7	89%
8	94%
9	92%
10	96%

$$\frac{\partial^2 \log L}{\partial \log A_t \partial \log A_s} = \frac{1}{A_s A_t} \frac{\partial^2 \log L}{\partial A_t \partial A_s} \quad (s=1, \dots, M; t=1, \dots, M).$$

Then using the results of Section 3.2:

$$\frac{\partial^2 \log L}{\partial \log A_i \partial \log A_s} = \sum_{i=1}^N \frac{q_{is} q_{it} \left[\prod_{j=1}^M A_j^{q_{ij}} \right] (y_i - n_i)}{A_s^2 A_t^2 \left(1 - \left[\prod_{j=1}^M A_j^{q_{ij}} \right] \right)^2}$$

(s=1, \dots, M; t=1, \dots, M).

It can then be shown that:

$$E \left[- \frac{\partial^2 \log L}{\partial \log A_t \partial \log A_s} \right] = \sum_{i=1}^N \frac{n_i q_{is} q_{it} \left[\prod_{j=1}^M A_j^{q_{ij}} \right]}{A_s^2 A_t^2 \left(1 - \left[\prod_{j=1}^M A_j^{q_{ij}} \right] \right)^2}$$

(s=1, \dots, M; t=1, \dots, M).

A likelihood ratio test was used to test equality of the estimated variance covariance matrix of the one hundred sets of component family yields and the inverse of the true information matrix (T.W. Anderson, 1958, Section 10.8). The calculated statistic was 304.44. The five percent Chi squared critical value on six degrees of freedom is 12.6, meaning that the hypothesis of equality of the two matrices is rejected at the five percent level. Although shown to be unequal, it appears that the inverse of the information matrix is an adequate approximation to the variance-covariance matrix for most purposes (Compare Table 3 and Table 4). The use of the inverse of the estimated information matrix in calculating confidence intervals should not greatly alter the level of confidence from ninety-five percent.

TABLE 3

ESTIMATED VARIANCE-COVARIANCE MATRIX FOR THE ONE HUNDRED SAMPLES
OF LOGARITHMS OF THE COMPONENT FAMILY YIELDS

4.9178×10^{-6}	5.6114×10^{-7}	-2.9472×10^{-7}
5.6114×10^{-7}	1.6996×10^{-6}	-5.2049×10^{-8}
-2.9472×10^{-7}	-5.2049×10^{-8}	2.4009×10^{-8}

TABLE 4

INVERSE OF THE TRUE INFORMATION MATRIX FOR THE LOGARITHMS
OF THE COMPONENT FAMILY YIELDS

4.4645×10^{-6}	2.9749×10^{-7}	-2.8201×10^{-7}
2.9749×10^{-7}	1.7344×10^{-6}	-4.7913×10^{-8}
-2.8301×10^{-7}	-4.7913×10^{-8}	1.9383×10^{-8}

Since the predicted logarithms of the unit yields are linear combinations of the estimates of the logarithms of the component family yields, it can be expected that the predicted logarithms of the unit yields will be better approximations to normal distributions. A poor estimate of the yield of components of the second family may explain why the level of confidence for some of the intervals based on predicted yields appear significantly different from ninety-five percent while others are relatively close. It appears that where components of the second family in a yield estimate, the level of confidence for the confidence interval for that estimate is further from ninety-five percent. (Compare Table 2 and Table 5). Having used only one hundred sets of observations, sampling error may explain the difference between the observed level of confidence and ninety-five percent. Further Monte Carlo studies with larger samples may be of use in making conclusions.

3.4.2 Applications

The method of predicting unit yields presently used treats an insertion as a component. However, an insertion is not a component but a process. An insertion may be a success or a failure, but, when units are tested after production, it is the components which are acceptable or unacceptable, not the insertions. A component may be inserted into a unit manually or by machine. If the probability of one type of insertion being successful is different from the probability of the other type being acceptable, then the yield of a

TABLE 5

COMPONENT FAMILY STRUCTURE OF THE ARTIFICIAL UNITS USED
FOR THE MONTE CARLO STUDY OF THE WEIGHTED
LEAST SQUARES METHOD FOR COMPONENT YIELDS

		COMPONENT FAMILY		
		1	2	3
Unit	1	27	3	450
	2	25	10	350
	3	31	0	375
	4	16	11	400
	5	10	25	200
	6	35	0	425
	7	29	29	325
	8	21	0	400
	9	21	9	428
	10	17	25	216

particular component family inserted manually should be estimated separately from the yield of components of that family inserted by machine.

Both the method of weighted least squares and the method of maximum likelihood were applied to a single set of randomly generated unit yields for those ten artificial units used in the Monte Carlo study of section 3.4.1. The results indicate that both methods work for the randomly generated approximately binomial data. However, in the case of the maximum likelihood method, numerical difficulties were encountered.

Using the weighted least squares estimates, the test of fit statistic for the randomly generated data was 2.23. The Chi squared critical value on seven degrees of freedom is 14.1. The test of fit statistic was also calculated for two of the samples used in the Monte Carlo study and were also found to be acceptable at the ninety-five percent level. It then appears that the weighted least squares method is satisfactory for approximately binomial observations of acceptable components. However, when the weighted least squares method was applied to actual production yields, the fit was not acceptable. Two sets of actual production data were used for which the units were made from five distinct families. The test of fit statistic for the one set of data was 10.13 which is greater than 7.81, the Chi squared five percent critical value on three degrees of freedom. For the other set of data, the statistic was 396.29 which is greater than 27.6, the Chi squared five percent critical

value on seventeen degrees of freedom. Although sampling error may be responsible for the very poor fit of the model to the second set of actual production yield data, a number of other factors may be responsible.

The present system of predicting yields of new units groups components into families which may not have the same yields. For example, resistors of all types are considered to be one family. However, it may be that resistors of different specifications and construction are affected differently during the production process. The possibility that the yield of a component inserted manually may differ from the yield of a component inserted by machine was not considered. Tests should be made to insure that all members of a family have the same yield. Otherwise, predicted unit yields are likely to be poor estimates of the true unit yields. Those component families used in the estimation of failure rates may not be appropriate for use in estimating yields.

A number of factors in the production process itself may cause the observed number of acceptable components to deviate from the binomial distribution. Tests may vary from one type of unit to another. If units are tested for any length of time, then those Poisson failures which can be expected during normal operation of a unit will noticeably affect the distribution of the number of units passing production tests. The yield of the first few units produced may be less than that for units produced after any initial production problems have been corrected. Human factors, such as one worker being distracted by another, may cause units to become unacceptable after production. The production process should

be checked to find out how these factors affect production. If units are produced in more than one location, checks should be made to insure that the yields are independent of location before results from different locations are combined to make yield estimates.

The method of maximum likelihood was initially tried using the method of scoring (Appendix 1) to maximize the likelihood. The program PREDMLE, designed to maximize the likelihood using the method of scoring was tested (Appendix 4) and the logic was found to be correct. Using the true unit yields as input and using the true component family yields as starting values, the iterative scheme converged after three steps. However, using other starting values close to the true component family yields, the estimates did not appear to be converging after seventy-five iterations (Table 6). This method was also tried with actual unit yield data from a production line. As anticipated, the sequence of component family yield estimates diverged. Weighted least squares estimates of the component family yields were used as starting values for the iterative procedure. However, after one hundred and fifty iterations, the component family yield estimates did not appear to be converging. The method of scoring was then discarded as a practical method of finding maximum likelihood estimates of component family yields.

The simplex optimization method of Nelder and Mead was then used to find those component family yield estimates which maximize the yield. This is the method described in section 3.2. Weighted least square estimates of the component family yields were used as

TABLE 6

ESTIMATED COMPONENT FAMILY YIELDS USING THE
METHOD OF SCORING TO MAXIMIZE THE LIKELIHOOD

Component Family	Starting Values	Estimated Yield after 3 Iterations	Expected Value of Estimate
1	.9900	.9900	.9900
2	.9950	.9950	.9950
3	.9990	.9990	.9990

Component Family	Starting Values	Estimated Yield after 3 Iterations	Expected Value of Estimate
1	.9925	.9996	.9900
2	.9950	.9969	.9950
3	.9975	.9982	.9990

one of the vertices of the initial simplex. When the method was applied to the randomly generated set of data, it was found that the likelihood increased as the procedure progressed (Figure 9). Although the method appears to work, the value of the likelihood remained constant after a number of steps. This was a result of the limited number of figures of accuracy kept by the computer. When the method was applied to actual observed yields of units produced, the same observations were made. One possible solution to the restricted number of figures of accuracy may be to use double precision in the computational work. It was also noted that, for both the randomly generated set of data and the actual observations, the maximum likelihood method generally gave a slightly smaller Chi-squared value than did the method of weighted least squares.

As an alternative to the method of maximum likelihood, the method of minimum Chi squared estimation (Kendall and Stuart, Volume 3, 1973, section 19.25) could be tried. This method minimizes the test of fit statistic:

$$\sum_{i=1}^N \frac{(n_i \hat{p}_i - y_i)^2}{n_i \hat{p}_i (1 - \hat{p}_i)}$$

where N is the number of distinct types of units produced, n_i is the number of units of type i produced, \hat{p}_i is the predicted yield of a unit of type i , and y_i is the observed number of units of type i accepted after production. One possible method of minimizing this statistic is to set equal to zero the derivatives of the statistic with respect to the estimated component family yield estimates. If the range of

Figure 9

Step by Step Results of Application of Simplex Method
of Maximizing the Likelihood For a Randomly Generated Set of Observations

NCOUNT = 1	SHRINK	LIKELIHOOD =	=0,370235303 E+04
NCOUNT = 2	EXPANSION	LIKELIHOOD =	=0,370235303 E+04
NCOUNT = 3	SHRINK	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 4	REFLECTION	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 5	SHRINK	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 6	SHRINK	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 7	SHRINK	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 8	SHRINK	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 9	REFLECTION	LIKELIHOOD =	=0,369542139 E+04
NCOUNT = 10	SHRINK	LIKELIHOOD =	=0,369541650 E+04
NCOUNT = 11	EXPANSION	LIKELIHOOD =	=0,369541650 E+04
NCOUNT = 12	SHRINK	LIKELIHOOD =	=0,369540625 E+04
NCOUNT = 13	REFLECTION	LIKELIHOOD =	=0,369540625 E+04
NCOUNT = 14	SHRINK	LIKELIHOOD =	=0,369540601 E+04
NCOUNT = 15	EXPANSION	LIKELIHOOD =	=0,369540601 E+04
NCOUNT = 16	SHRINK	LIKELIHOOD =	=0,369540259 E+04
NCOUNT = 17	REFLECTION	LIKELIHOOD =	=0,369540259 E+04
NCOUNT = 18	SHRINK	LIKELIHOOD =	=0,369540259 E+04
NCOUNT = 19	EXPANSION	LIKELIHOOD =	=0,369540259 E+04
NCOUNT = 20	SHRINK	LIKELIHOOD =	=0,369540161 E+04
NCOUNT = 21	EXPANSION	LIKELIHOOD =	=0,369540161 E+04
NCOUNT = 22	SHRINK	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 23	SHRINK	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 24	EXPANSION	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 25	REFLECTION	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 26	EXPANSION	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 27	SHRINK	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 28	EXPANSION	LIKELIHOOD =	=0,369540137 E+04
NCOUNT = 29	SHRINK	LIKELIHOOD =	=0,369540015 E+04
NCOUNT = 30	EXPANSION	LIKELIHOOD =	=0,369540015 E+04
NCOUNT = 31	SHRINK	LIKELIHOOD =	=0,369539990 E+04
NCOUNT = 32	EXPANSION	LIKELIHOOD =	=0,369539990 E+04
NCOUNT = 33	SHRINK	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 34	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 35	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 36	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 37	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 38	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 39	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 40	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 41	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 42	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 43	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 44	REFLECTION	LIKELIHOOD =	=0,369539844 E+04
NCOUNT = 45	REFLECTION	LIKELIHOOD =	=0,369539844 E+04

convergence is great enough, these equations may be solved using Newton's iterative method (Russell, 1970, Chapter 5). Otherwise the statistic may be minimized using the simplex method of Nelder and Mead. (See Appendix 2). One would expect that the number of figures of accuracy available with the computer is sufficient for making satisfactory estimates of component family yields.

Although the method of weighted least squares may give reasonable estimates of component yields, further work with this problem may be of value. The method of weighted least squares has the advantage of requiring comparatively few calculations. However, we can expect the maximum likelihood estimation method and the minimum Chi squared estimation method to fit the data better. It may be that a wide range of starting values can be used for the iterative scheme for the minimum Chi squared method and the sequence of estimates for this method may converge quickly. To use either the maximum likelihood or the minimum Chi squared methods for practical purposes, a method of calculating approximate confidence intervals must be found.

In order to make any of the methods of estimation better for practical use, there are two areas which should be investigated. The yields of the components within each family should be tested for equality. If equality among the components of a family does not exist, the components should be regrouped into families of components of equal yield. The second area to be investigated is the actual production process. One can expect that the closer the observed

number of units accepted after production is to a binomial observation, the better will be the estimates of component family yields. An investigation into these two areas may provide reliability engineers with better estimates of component yields and, hence, better predictions of unit yields.

APPENDIX 1

The Method of Scoring

The method of scoring (C.R. Rao, 1965, Section 5g) is an iterative scheme for finding maximum likelihood estimates of parameters. Define L as the likelihood function for the vector of parameters:

$$\underline{\theta} = \begin{bmatrix} \theta_1 \\ \vdots \\ \theta_N \end{bmatrix} .$$

Let:

$$S(\underline{\theta}) = \begin{bmatrix} \frac{\partial \log L}{\partial \theta} \\ \vdots \\ \frac{\partial \log L}{\partial \theta_N} \end{bmatrix} , \quad \mathcal{J}(\underline{\theta}) = E \left[\frac{\partial^2 \log L}{\partial \theta_i \partial \theta_j} \right]_{N \times N}$$

Let $H(\underline{\theta})$ be the N by N derivative matrix for $S(\underline{\theta})$.

Then:

$$E[-H(\underline{\theta})] = \mathcal{J}(\underline{\theta}) .$$

As a first approximation, one may take:

$$\mathcal{J}(\hat{\underline{\theta}}) \approx -H(\underline{\theta}) ,$$

where $\hat{\underline{\theta}}$ is the maximum likelihood estimate of $\underline{\theta}$.

Since a first order Taylor's expansion gives:

$$S(\underline{\theta}) \approx S(\hat{\underline{\theta}}) + (\underline{\theta} - \hat{\underline{\theta}}) H(\hat{\underline{\theta}}) ,$$

and:

$$S(\hat{\underline{\theta}}) = 0, \quad \text{and we derive the iterative scheme:}$$

$$\underline{\theta}_{\ell+1} = \underline{\theta}_{\ell} - H^{-1}(\underline{\theta}_{\ell}) \cdot S(\underline{\theta}_{\ell}) ,$$

which will converge to $\hat{\theta}$ if an initial value θ_0 sufficiently close to $\hat{\theta}$ is chosen. Replacing H by its expected value, we get:

$$\theta_{l+1} = \theta_l - \mathcal{J}^{-1}(\theta_l) \cdot S(\theta_l),$$

which is the iterative method of scoring.

APPENDIX 2

The Nelder-Mead Simplex Method:

The Nelder Mead simplex (Kowalik and Osborne, 1968, Section 2.6) is a direct search technique for finding an optimum value. The procedure as described here locates a maximum using a simplex, a set of $n+1$ points in n dimensions. The simplex is manipulated by reflecting the point at which the function f is the least, or by expanding or contracting the simplex

Let:

- (1) x_h be the vertex corresponding to $f(x_h) = \min_i f(x_i)$
($i=1, \dots, n+1$).
- (2) x_s be the vertex which corresponds to $f(x_s) = \max_i f(x_i)$, $i \neq h$.
- (3) x_ℓ be the vertex corresponding to $f(x_\ell) = \max_i f(x_i)$,
($i=1, \dots, n+1$).
- (4) x_0 be the centroid of all x_i , $i \neq h$ and is given by

$$x_0 = \frac{1}{n} \sum_{\substack{i=1 \\ i \neq h}}^{n+1} x_i .$$

Now define the three basic operations used:

- (1) Reflection, where x_h is replaced by

$$x_r = (1+\alpha)x_0 - \alpha x_h$$

where $\alpha > 0$ and is equal to the ratio of the distance $[x_r, x_0]$ to $[x_h, x_0]$.

(2) Expansion, where x_r is expanded in the direction along which the function value is expected to increase. The relation

$$x_e = \gamma x_r + (1-\gamma)x_0$$

is used where $\gamma > 1$ is the ratio of the distance $[x_e, x_0]$ to $[x_r, x_0]$.

(3) Contraction, where the simplex is contracted,

$$x_c = \beta x_h + (1-\beta)x_0,$$

where $0 < \beta < 1$ and is the ratio of the distance $[x_c, x_0]$ to $[x_h, x_0]$.

The technique proceeds as follows:

(i) From an initial simplex and evaluate the function at each of the $n+1$ vertices.

(ii) Try a reflection and evaluate the function at the reflected point.

(iii) If $f(x_h) \leq f(x_r) \leq f(x_\ell)$, replace x_h by x_r and return to step (i).

(iv) If $f(x_r) > f(x_\ell)$ it can be expected that an expansion in the direction $x_r - x_0$ could give us a greater value f or f . Replace x_h by x_r if $f(x_\ell) < f(x_e)$ and return to step (i). Otherwise replace x_h by x_r and return to step (i).

(v) If $f(x_h) < f(x_r) < f(x_s)$ replace x_h by x_r and try a contraction. If $f(x_h) < f(x_c)$, replace x_h by x_c and return to step (i). Otherwise the last simplex is shrunk about the point x_ℓ by the

relation

$$x_i' = \frac{1}{2} (x_i + x_\ell)$$

and return to (i).

APPENDIX 3

Programs for the Component Failure Rate Problem

The computing work for the problem of estimating component family failure rates involved two programs. Both programs are written in FORTRAN and both use the maximum likelihood method of estimating component family failure rates for one period of time. The program FAILMLE is designed for practical use and an external file is used as its source of unit failure rate data. The program MONTE generates one hundred random samples of unit failure rates for which component family failure rates are estimated. The input files for both programs are eighty columns long. The output files have a length of one hundred and thirty-three columns including carriage control.

Input for FAILMLE (see Figure 10) is unformatted and is completely general for any number of units observed and any number of component families. The first row of the input gives N , the number of distinct units observed, and then M , the number of distinct component families for which failure rates can be estimated. The first M columns of the second to $(N+1)$ st rows, inclusive, is the matrix $Q = [q_{ij}]_{N \times M}$ where q_{ij} is the number of components of the j^{th} family in a unit of type i . The $(M+1)$ st entry in the $(i+1)$ st row is the number of units of type i in use during the time period. The $(M+2)$ nd entry in the $(i+1)$ st row is the number of type i unit failures observed during that time period. The $(N+2)$ nd row give the length of the time period in units of ten million hours for which observations were made. The value in the $(N+3)$ rd row is given to the

M component family failure rates as starting values in the iterative procedure.

Input for MONTE is the same as that for FAILMLE except that M is restricted to three. Input for unit failures of one sample is required, but the results of the program are independent of this information. An alteration to the program would allow the omission of unit failures as input. MONTE could be generalized to allow for any number of component families and for any number of generated samples.

The external subroutines INFAIL and LAFAIL are called from both FAILMLE and MONTE. INFAIL determines the estimated information matrix as described in section 2.2 and LAFAIL calculates the predicted failure rates of those units which have been used in the estimation procedure. Three subroutines, SINV,EIGEN, and GAUSS, from the SSP FORTRAN library were used in the computing. SINV, which determines the inverse of a positive definite symmetric matrix, is called from INFAIL. The subroutine EIGEN is used to determine the eigenvectors and eigenvalues of the inverse of the estimated information matrix in the program FAILMLE. GAUSS, a normal random number generator, is used in MONTE to generate unit failures.

The approximate confidence intervals in both FAILMLE and MONTE are calculated at the ninety-five percent confidence level. Alterations in the program could be made which would allow different levels of confidence. FAILMLE could also be generalized to allow

for observations of unit failure rates for any number of time periods.

In order to check the logic of FAILMLE, the program was run treating the expected number of unit failures for a sample as the observed number of unit failures. The results (Table 7) indicate that the logic was correct. Differences between true values and the estimated values were due to round off errors.

Those calculations which were done by hand could be incorporated into the programs. The test of fit described in section 2.2 could be included in both MONTE and FAILMLE. Those calculations necessary to estimate the variance-covariance matrix of the parameter estimates found with MONTE could be included in the program. FAILMLE would be of more practical use if the program and its input were adjusted to predict point estimates and to determine confidence intervals for the reliability of new electronic units.

Figure 10

Input Format For The Program FAILMLE

10,3		
27,3,450,	1000,368	UNIT 1
25,10,350,	1500,488	UNIT 2
31,0,375,	200,69	UNIT 3
16,11,400,	1200,369	UNIT 4
10,25,200,	500,106	UNIT 5
35,0,425,	1800,698	UNIT 6
29,29,325,	900,342	UNIT 7
21,0,400,	2000,610	UNIT 8
21,9,428,	1400,478	UNIT 9
17,25,216,	1000,256	UNIT 10
,0005		
5		

TABLE 7

RESULTS OF TEST RUN ON THE PROGRAM FAILMLE

Component Family	Estimated Component Family Failure Rate	True Component Family Failure Rate
1	10.0680	10.0
2	4.9885	5.0
3	.9970	1.0

Unit	Estimated Unit Failure Rate	True Unit Failure Rate
1	735.4426	735.0
2	650.5281	650.0
3	685.9751	685.0
4	614.7542	615.0
5	424.7893	425.0
6	776.0962	775.0
7	760.6575	760.0
8	610.2202	610.0
9	683.0325	683.0
10	511.2166	511.0

PROGRAM LISTING - FAILMLE

```

C
C THIS PROGRAM USES THE MAXIMUM LIKELIHOOD METHOD OF ESTIMATION AND
C THE METHOD OF SCORING TO DETERMINE THE FAILURE RATES OF COMPONENT
C FAMILIES.
C
  DIMENSION Q(50,25),XINUSE(50),FAIL(50),XINF(25,25),XLAMDA(50),
  $ LWORK(25),R(25,25),PREV(25),MWORK(25),ALPHA(25),FAC(25),
  $ S(25),CONSD(25)
  READ(9,*)N,M
C
C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF COLUMNS
C (COMPONENT FAMILIES).
C
  CALL SOLVE(Q,XINUSE,FAIL,LWORK,MWORK,ALPHA,M,N,FAC,S,XLAMDA,XINF,
  $ PREV,R,CONSD)
  STOP
  END
C
  SUBROUTINE SOLVE(Q,XINUSE,FAIL,LWORK,MWORK,ALPHA,M,N,FAC,S,
  $ XLAMDA,XINF,PREV,R,CONSD)
  DIMENSION Q(N,M),XINUSE(N),FAIL(N),XINF(M,M),S(M),LWORK(M),
  $ MWORK(M),R(M,M),PREV(M),ALPHA(M),FAC(M),XLAMDA(N),
  $ CONSD(M)
C
  WRITE(8,200)
200  FORMAT(20X,'DATA MATRIX: ',/,/,/)
C
  DO 10 I=1,N
  READ(9,*)(Q(I,J),J=1,M),XINUSE(I),FAIL(I)
  WRITE(8,210)(Q(I,J),J=1,M)
210  FORMAT(3X,25F4,0)
  10  CONTINUE
C
  READ(9,*) TIME
  WRITE(8,220)
220  FORMAT(1H1)
  WRITE(8,230)
230  FORMAT(29X,'UNIT!',15X,'NUMBER IN USE!',10X,'NUMBER OF FAILURES!',
  $ /)
C
  DO 15 I=1,N
  WRITE(8,240)I,XINUSE(I),FAIL(I)
240  FORMAT(30X,I2,2(20X,F5,0))
  15  CONTINUE
C
  WRITE(8,250)TIME
250  FORMAT(/,/,40X,'TIME IN UNITS OF 10 MILLION HOURS =',F10,6)
C
C SET UP INITIAL VALUES.
C
  NIT=0
  READ(9,*) START
C
  DO 20 J=1,M
  ALPHA(J)=START

```

```

20  CONTINUE
C
    WRITE(8,220)
    WRITE(8,260) NIT
260  FORMAT(/,15X,'N = ',I3)
    WRITE(8,270)(J,ALPHA(J),J=1,M)
270  FORMAT(25X,'ALPHA(',I2,',') =',E16,8)
C
C BEGIN THE ITERATIVE PROCEDURE.
C
500  NIT=NIT+1
C
C WE WISH TO KEEP THE OLD VALUES OF ALPHA TO TEST FOR CONVERGENCE.
C
    DO 25 J=1,M
    PREV(J)=ALPHA(J)
25  CONTINUE
C
    WRITE(8,260)NIT
C
    CALL LAFAIL(N,M,XLAMDA,Q,ALPHA)
C
C DETERMINE THE SCORE VECTOR,
C
    DO 30 J=1,M
    S(J)=0.0
    DO 35 I=1,N
    F=FAIL(I)/XLAMDA(I) - TIME*XINUSE(I)
    S(J)=S(J)+Q(I,J)*F
35  CONTINUE
30  CONTINUE
C
    CALL INFAIL(N,M,Q,XINUSE,TIME,XLAMDA,XINF,LWORK,MWORK,
    $ CONSD)
C
C DETERMINE THE ADJUSTMENT FACTOR
C
    DO 40 J=1,M
    FAC(J)=0.0
    DO 45 JJ=1,M
    FAC(J)=FAC(J)+XINF(J,JJ)*S(JJ)
45  CONTINUE
40  CONTINUE
C
C DETERMINE THE NEW ESTIMATES OF COMPONENT FAMILY FAILURE RATES,
C
    DO 50 J=1,M
    ALPHA(J)=ALPHA(J)+FAC(J)
50  CONTINUE
C
    WRITE(8,270)(J,ALPHA(J),J=1,M)
C
    DO 55 J=1,M
    IF(ABS(ALPHA(J)-PREV(J)).GT.0.000005) GOTO 520
55  CONTINUE

```

PROGRAM LISTING - FAILMLE (Cont'd)

```

C
    GOTO 510
C
520  IF(NIT,LT,100)GOTO 500
510  CALL LAFAIL(N,M,XLAMDA,Q,ALPHA)
    CALL INFAIL(N,M,Q,XINUSE,TIME,XLAMDA,XINF,LWORK,MWORK,
$ CONDSO)
C
    WRITE(8,220)
    WRITE(8,280)
280  FORMAT(50X,'COVARIANCE MATRIX',/)
    WRITE(8,290)(J,J=1,M)
290  FORMAT(16(13X,I2),/)
C
    DO 60 I=1,M
    WRITE(8,300)I,(XINF(I,J),J=1,I)
300  FORMAT(2X,I2,16(2X,E13,7))
60   CONTINUE
C
C DETERMINE APPROXIMATE CONFIDENCE INTERVALS FOR OUR ESTIMATES OF
C THE FAILURE RATES.
C
    WRITE(8,220)
    WRITE(8,310)
310  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR COMPONENT',
$ ' FAILURE RATES:',/,/)
    WRITE(8,320)
320  FORMAT(7X,'COMPONENT',6X,'ESTIMATED',8X,'UNCONDITIONAL',12X,
$ 'CONDITIONAL')
    WRITE(8,330)
330  FORMAT(8X,'FAMILY',6X,'FAILURE RATE',7X,'VARIANCE C,I,',
$ 12X,'VARIANCE C,I,',/,)
    WRITE(8,340)
340  FORMAT(10X,2(' '),10X,8(' '),6X,19(' '),5X,19(' '))
C
    DO 65 J=1,M
    COMPLB=ALPHA(J)-1.96*SQRT(XINF(J,J))
    COMPUB=ALPHA(J)+1.96*SQRT(XINF(J,J))
    CONDLB=ALPHA(J)-1.96*CONDSO(J)
    CONDUB=ALPHA(J)+1.96*CONDSO(J)
    WRITE(8,350)J,ALPHA(J),COMPLB,COMPUB,CONDLB,CONDUB
350  FORMAT(10X,I2,10X,F8,5,' ',5X,'(',F8,5,' ',F8,5,' )',
$ 5X,'(',F8,5,' ',F8,5,' )')
65   CONTINUE
C
    WRITE(8,220)
C
C DETERMINE CONFIDENCE INTERVALS FOR THE UNIT FAILURE RATES FROM
C THE OBSERVED FAILURES AND FROM THE ESTIMATED FAILURE RATES.
C
    WRITE(8,360)
360  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR UNIT',
$ ' FAILURE RATES:',/,/)
    WRITE(8,370)
370  FORMAT(9X,'UNIT',17X,'FOR OBSERVED',40X,'FOR ESTIMATES',/,/)

```


PROGRAM LISTING - FAILMLE (Cont'd)

```

WRITE(8,380)
380  FORMAT(10X,2(' '),5X,39(' '),15X,39(' '),/)
C
DO 70 I=1,N
PHI=FAIL(I)/(XINUSE(I)*TIME)
POISLB=PHI-1.96*SQRT(PHI)
POISUB=PHI+1.96*SQRT(PHI)
ESTVAR=0.0
C
DO 75 J=1,M
DO 80 K=1,M
ESTVAR=ESTVAR+Q(I,J)*Q(I,K)*XINF(J,K)
80  CONTINUE
75  CONTINUE
C
ESTLB=XLAMDA(I)-1.96*SQRT(ESTVAR)
ESTUB=XLAMDA(I)+1.96*SQRT(ESTVAR)
WRITE(8,390)I,PHI,POISLB,POISUB,XLAMDA(I),ESTLB,ESTUB
390  FORMAT(10X,I2,5X ,F10.5,' ',5X,'(',F10.5,' ',F10.5,')',15X,F10.5,
S ' ',5X,'(',F10.5,' ',F10.5,')')
70  CONTINUE
C
C DETERMINE PRINCIPAL COMPONENTS, THAT IS BY CALCULATING THE
C EIGENVALUES AND THE EIGENVECTORS WE CAN DETERMINE NEW BASES
C FOR OUR COMPONENTS WHICH WILL NOT BE CORRELATED.
C
CALL EIGEN(XINF,R,M,0)
WRITE(8,220)
C
DO 85 J=1,M
WRITE (8,400)J,XINF(J,J)
400  FORMAT(/,20X,'EIGENVALUE(',I2,') = ',E16.8,/)
WRITE(8,410)(J,I,R(I,J),I=1,M)
410  FORMAT(25X,'EIGENVECTOR(',I2,',' ,I2,') = ',E16.8)
85  CONTINUE
C
RETURN
END

```

```

C
C THIS PROGRAM USES THE MAXIMUM LIKELIHOOD METHOD OF ESTIMATION AND
C THE METHOD OF SCORING TO DETERMINE THE FAILURE RATES OF COMPONENT
C FAMILIES.
C
  DIMENSION Q(50,25),XINUSE(50),FAIL(50),XINF(25,25),XLAMDA(50),
  $ LWORK(25),R(25,25),PREV(25),MWORK(25),ALPHA(25),FAC(25),
  $ S(25),CONSDSD(25)
  READ(9,*)N,M
C
C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF COLUMNS
C (COMPONENT FAMILIES).
C
  CALL SOLVE(Q,XINUSE,FAIL,LWORK,MWORK,ALPHA,M,N,FAC,S,XLAMDA,XINF,
  $ PREV,R,CONSDSD)
  STOP
  END
C
  SUBROUTINE SOLVE(Q,XINUSE,FAIL,LWORK,MWORK,ALPHA,M,N,FAC,S,
  $ XLAMDA,XINF,PREV,R,CONSDSD)
  DIMENSION Q(N,M),XINUSE(N),FAIL(N),XINF(M,M),S(M),LWORK(M),
  $ CMPFL(3),RATE(10),XMEAN(10),S1(10),S2(10),
  $ DEV(10),XBAR(3),SUM(3),
  $ MWORK(M),R(M,M),PREV(M),ALPHA(M),FAC(M),XLAMDA(N),
  $ CONSDSD(M)
C
  WRITE(8,200)
200  FORMAT(20X,'DATA MATRIX:',/,/,/)
C
  DO 10 I=1,N
  READ(9,*)(Q(I,J),J=1,M),XINUSE(I),FAIL(I)
  WRITE(8,210)(Q(I,J),J=1,M)
210  FORMAT(3X,25F4.0)
  10  CONTINUE
C
  READ(9,*) TIME
  WRITE(8,250)TIME
250  FORMAT(/,/,40X,'TIME IN UNITS OF 10 MILLION HOURS =',F10.6)
C
  WRITE(8,220)
220  FORMAT(1H1)
  CMPFL(1)=10.
  CMPFL(2)=5.
  CMPFL(3)=1.
C
  WRITE(8,221)
221  FORMAT(18X,'COMPONENT FAMILY',10X,'FAILURE RATE',/)
  WRITE(8,222)(J,CMPFL(J),J=1,M)
222  FORMAT(25X,12,20X,F5.1)
C
C DETERMINE AND PRINT THE TRUE COMPONENT FAMILY FAILURE RATES.
C
  WRITE(8,220)
  WRITE(8,223)
223  FORMAT(24X,'UNIT',15X,'UNITS IN FIELD',13X,'TRUE FAILURE RATE',/)

```

PROGRAM LISTING - MONTE (Cont'd)

```

C
DO 11 I=1,N
RATE(I)=0.0
DO 21 J=1,M
RATE(I)=RATE(I)+Q(I,J)*CMPFL(J)
21 CONTINUE
WRITE(8,224)I,XINUSE(I),FAIL(I)
224 FORMAT(25X,12,20X,F5.0,20X,F8.0)
XMEAN(I)=XINUSE(I)*TIME*RATE(I)
DEV(J)=SQRT(XMFAN(I))
S1(I)=0.0
S2(I)=0.0
11 CONTINUE
C
WRITE(8,220)
IX=87
DO 61 J=1,M
XBAR(J)=0.0
SUM(J)=0.0
61 CONTINUE
C
DO 41 NSTEP = 1,100
C
C GENERATE APPROXIMATE POISSON RANDOM NUMBERS TO BE USED AS OBSERVED
C NUMBER OF UNIT FAILURES IN THE FIELD.
C
DO 51 I=1,N
500 CALL GAUSS(IX,DEV(I),XMEAN(I),FAIL(I))
IF(FAIL(I).LT.0.0)GOTO 500
51 CONTINUE
C
C SET UP INITIAL VALUES.
C
NIT=0
C
DO 20 J=1,M
ALPHA(J)=CMPFL(J)
20 CONTINUE
C
C BEGIN THE ITERATIVE PROCEDURE.
C
600 NIT=NIT+1
C
C WE WISH TO KEEP THE OLD VALUES OF ALPHA TO TEST FOR CONVERGENCE.
C
DO 25 J=1,M
PREV(J)=ALPHA(J)
25 CONTINUE
C
C
CALL LAFAIL(N,M,XLANDA,Q,ALPHA)
C
C DETERMINE THE SCORE VECTOR.
C

```

PROGRAM LISTING - MONTE (Cont'd)

```

DO 30 J=1,M
S(J)=0.0
DO 35 I=1,N
F=FAIL(I)/XLAMDA(I) - TIME*XINUSE(I)
S(J)=S(J)+Q(I,J)*F
35 CONTINUE
30 CONTINUE
C
CALL INFAIL(N,M,Q,XINUSE,TIME,XLAMDA,XINF,LWORK,MWORK,
$ CONSDSD)
C
C DETERMINE THE ADJUSTMENT FACTOR
C
DO 40 J=1,M
FAC(J)=0.0
DO 45 JJ=1,M
FAC(J)=FAC(J)+XINF(J,JJ)*S(JJ)
45 CONTINUE
40 CONTINUE
C
C DETERMINE THE NEW ESTIMATES OF COMPONENT FAMILY FAILURE RATES,
C
DO 50 J=1,M
ALPHA(J)=ALPHA(J)+FAC(J)
50 CONTINUE
C
C
DO 55 J=1,M
IF(ABS(ALPHA(J)-PREV(J)).GT.0.000005) GOTO 520
55 CONTINUE
C
GOTO 510
C
520 IF(NIT.LT.100)GOTO 600
510 CALL LAFAIL(N,M,XLAMDA,Q,ALPHA)
CALL INFAIL(N,M,Q,XINUSE,TIME,XLAMDA,XINF,LWORK,MWORK,
$ CONSDSD)
C
C DETERMINE APPROXIMATE CONFIDENCE INTERVALS FOR OUR ESTIMATES OF
C THE FAILURE RATES,
C
WRITE(8,310)
310 FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR COMPONENT',
$ ' FAILURE RATES: ',/,/)
WRITE(8,320)
320 FORMAT(7X,'COMPONENT',6X,'ESTIMATED',8X,'UNCONDITIONAL',12X,
$ 'CONDITIONAL')
WRITE(8,330)
330 FORMAT(8X,'FAMILY',6X,'FAILURE RATE',7X,'VARIANCE C.I.',
$ 12X,'VARIANCE C.I.',/,)
WRITE(8,340)
340 FORMAT(10X,2(' '),10X,8(' '),6X,19(' '),5X,19(' '))
C
DO 65 J=1,M
COMPLB=ALPHA(J)-1.96*SQRT(XINF(J,J))

```

```

COMPUB=ALPHA(J)+1.96*SQRT(XINF(J,J))
CONDLB=ALPHA(J)-1.96*CONDSO(J)
CONDOB=ALPHA(J)+1.96*CONDSO(J)
WRITE(8,350)J,ALPHA(J),COMPLB,COMPUB,CONDLB,CONDOB
350  FORMAT(10X,I2,10X,F8.5,' ':1,5X,'( ',F8.5,' ',F8.5,' )',
$ 5X,'( ',F8.5,' ',F8.5,' )')
XBAR(J)=XBAR(J)+ALPHA(J)
SUM(J)=SUM(J)+ALPHA(J)**2
65  CONTINUE
C
C
C DETERMINE CONFIDENCE INTERVALS FOR THE UNIT FAILURE RATES FROM
C THE OBSERVED FAILURES AND FROM THE ESTIMATED FAILURE RATES,
C
WRITE(8,360)
360  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR UNIT',
$ ' FAILURE RATES',/,/)
WRITE(8,370)
370  FORMAT(9X,'UNIT',17X,'FOR OBSERVED',40X,'FOR ESTIMATES',/,/)
WRITE(8,380)
380  FORMAT(10X,2(' '),5X,39(' '),15X,39(' '),/)
C
DO 70 I=1,N
PHI=FAIL(I)/(XINUSE(I)*TIME)
POISLB=PHI-1.96*SQRT(PHI)
POISUB=PHI+1.96*SQRT(PHI)
ESTVAR=0.0
C
DO 75 J=1,M
DO 80 K=1,M
ESTVAR=ESTVAR+Q(I,J)+Q(I,K)*XINF(J,K)
80  CONTINUE
75  CONTINUE
C
ESTLB=XLAMDA(I)-1.96*SQRT(ESTVAR)
ESTUB=XLAMDA(I)+1.96*SQRT(ESTVAR)
WRITE(8,390)I,PHI,POISLB,POISUB,XLAMDA(I),ESTLB,ESTUB
390  FORMAT(10X,I2,5X ,F10.5,' ':1,5X,'( ',F10.5,' ',F10.5,' )',15X,F10.5,
$ ' ':1,5X,'( ',F10.5,' ',F10.5,' )')
S1(I)=S1(I)+XLAMDA(I)
S2(I)=S2(I)+XLAMDA(I)**2
70  CONTINUE
C
41  CONTINUE
WRITE(8,220)
WRITE(8,375)
375  FORMAT(20X,'95% CONFIDENCE INTERVALS FOR THE ',
$ ' COMPONENT FAILURE RATE ESTIMATES',/,)
WRITE(8,381)
381  FORMAT(17X,'COMPONENT',12X,'ESTIMATE',12X,
$ 'CONFIDENCE INTERVAL',6X,'ACTUAL FAILURE RATE',/,)
WRITE(8,385)
385  FORMAT(20X,2(' '),15X,9(' '),11X,21(' '),10X,9(' '))
C
DO 71 J=1,M

```

PROGRAM LISTING - MONTE (Cont'd)

```

SUM(J)=(SUM(J)-((XBAR(J)**2)/100.))/99.
XBAR(J)=XBAR(J)/100.
XLB=XBAR(J)-1.96*SQRT(SUM(J))
XUB=XBAR(J)+1.96*SQRT(SUM(J))
WRITE(8,395)J,XBAR(J),XLB,XUB,CMFPL(J)
395  FORMAT(20X,12,15X,F9.4,':',10X,'( ',F9.4,' ',F9.4,' )',
$ 10X,F9.5)
71  CONTINUE
C
WRITE(8,220)
WRITE(8,400)
400  FORMAT(20X,'95% CONFIDENCE INTERVALS FOR UNIT FAILURE RATE',
$ ' ESTIMATES:',/)
WRITE(8,410)
410  FORMAT(19X,'UNIT',15X,'ESTIMATE',12X,
$ 'CONFIDENCE INTERVAL',/)
WRITE(8,385)
C
DO 81 I=1,N
S2(I)=(S2(I)-((S1(I)**2)/100.))/99.
S1(I)=S1(I)/100.
XLB=S1(I)-1.96*SQRT(S2(I))
XUB=S1(I)+1.96*SQRT(S2(I))
WRITE(8,395)I,S1(I),XLB,XUB,RATE(I)
81  CONTINUE
C
RETURN
END

```

SUBROUTINE LISTING - INFAL

```

SUBROUTINE INFAL(N,M,Q,XINUSE,TIME,XLAMDA,XINF,LWORK,MWORK,
& CONDSO)

```

```

C
C THIS SUBROUTINE DETERMINES THE INFORMATION MATRIX FOR THE FAILURE RATE
C PROBLEM AND ITS INVERSE.

```

```

C
C DIMENSION Q(N,M),XINUSE(N),XINF(M,M),XLAMDA(N),LWORK(M),MWORK(M),
& A(325),CONDSO(M)

```

```

C
DO 10 J=1,M
DO 15 JJ=1,J
XINF(J,JJ)=0.0
DO 20 I=1,N
XINF(J,JJ)=XINF(J,JJ)+TIME*XINUSE(I)*Q(I,J)*Q(I,JJ)/XLAMDA(I)
20 CONTINUE
15 CONTINUE
CONDSO(J)=1.0/SQRT(XINF(J,J))
10 CONTINUE

```

```

C
DO 25 J=2,M
JMIN=J-1
DO 30 JJ=1,JMIN
XINF(JJ,J)=XINF(J,JJ)
30 CONTINUE
25 CONTINUE

```

```

C
DO 35 J=1,M
CONTINUE
LSUM=0
DO 40 J=1,M
DO 45 K=1,J
LSUM=LSUM+1
A(LSUM)=10.E7*XINF(J,K)
45 CONTINUE
40 CONTINUE

```

```

C
EPS=10.E-6
CALL SINVA(A,M,EPS,IER)

```

```

C
LSUM=0
DO 50 J=1,M
DO 55 K=1,J
LSUM=LSUM+1
XINF(J,K)=10.E7*A(LSUM)
XINF(K,J)=XINF(J,K)
55 CONTINUE
50 CONTINUE

```

```

C
DO 60 J=1,M
CONTINUE
DO 65 J=1,M
CONTINUE
RETURN
END

```

```
      SUBROUTINE LAFAIL(N,M,XLAMDA,Q,ALPHA)
C
C THIS SUBROUTINE DETERMINES ESTIMATES OF THE UNIT FAILURE RATES.
C
      DIMENSION XLAMDA(N),Q(N,M),ALPHA(M)
C
      DO 10 I=1,N
      XLAMDA(I)=0.0
      DO 15 J=1,M
      XLAMDA(I)=XLAMDA(I)+ALPHA(J)*Q(I,J)
15      CONTINUE
10      CONTINUE
C
      RETURN
      END
```


APPENDIX 4

Program for the Component Yield Problem

The computing work for the problem of estimating component family yields involved five programs. All are written in FORTRAN. The programs LINLSQ and CARLO use the method of weighted least squares. LINLSQ is designed for practical use while CARLO, which generates one hundred random samples of unit yields, is designed to study the properties of the estimates. The programs PREDMLE, COMB and SIMPLEX are designed to find maximum likelihood estimates of component family yields. PREDMLE uses a common starting value for the component family yield estimates and uses the method of scoring to find those estimates which maximize the likelihood. Using those estimates determined by the method of weighted least squares as starting values, the program COMB uses the method of scoring to find maximum likelihood estimates of component family yields. The program SIMPLEX uses the Nelder Mead Simplex method of finding maximum likelihood estimates of the component family yields. The method of weighted least squares is used to determine one of the vertices of the initial simplex used in SIMPLEX. The output file for all five programs has a length of one hundred and thirty-three columns including the carriage control.

Input for LINLSQ (Figure 11) is read from an external file having a length of eighty columns. It is unformatted and is general for any number of units observed and any number of component families. The first row of the input gives N, the number of distinct component families for which yields

can be estimated. The first M columns of the second to (N+1)st rows inclusive is the matrix $Q = [q_{ij}]_{N \times M}$ where q_{ij} is the number of components of the j^{th} family in a unit of type i . The (M+1)st entry in the (i+1)st row is the number of units of type i produced during the production period. The (M+2)nd entry in the (i+1)st row is the number of units of type i accepted during the production period. The (N+2)nd row gives the 97.5 percent critical value of the student's t distribution on $N-M$ degrees of freedom.

LINLSQ calls three subroutines, GMPRD, SINV, and EIGEN, from the SSP FORTRAN library. GMPRD determines the product of two general matrices. SINV calculates the inverse of a positive definite symmetric matrix and is used to determine the estimated variance-covariance matrix of the estimated component family yields. EIGEN is used to determine the eigenvectors and eigenvalues of that matrix.

The logic of LINLSQ was tested by using as input the expected number of acceptable units for a sample for which the component family yields are known. The program was adjusted to allow for the fact that there would be no variance in the input data. The results (Table 8) indicated that the logic was correct. Differences between the true values and the estimates were due to round off error.

Input for CARLO is the same as that for LINLSQ except that M is restricted to the value three. Input for the number of acceptable units of each type for one sample is required, but the results of the program would allow the omission of this input. CARLO could be

generalized to allow for any number of component families and for any number of generated samples. Three SSP subroutines GAUSS, GMPRD, and SINV are required for CARLO. GAUSS, a normal random number generator, is used to generate the number of acceptable units of each type.

Input for PREDMLE is the same as that for LINLSQ except that the entry in the (N+2)nd row gives a value which is given to the M component family yield estimates as starting values for the iterative procedure. PREDMLE calls the subroutine MINV from the SSP FORTRAN library in order to determine the inverse of the information matrix. The same data used to test LINLSQ was used to test the logic of PREDMLE. To start the iterative procedure in the test, the true component family yields were used as starting values. Test results (Table 9) indicate that the logic is correct.

The input for COMB is the same as that for LINLSQ. Five external subroutines are called from COMB. The subroutines SINV, GMPRD, and EIGEN are called from the SSP FORTRAN library. COMYLD calculates predicted unit yields from estimates of component family yields. COMINF calculates the estimated information matrix and its inverse.

The input for SIMPLEX is identical to that for LINLSQ except that no entry in the (N+2)nd row of the external data file is required. The subroutines GMPRD and SINV are called from the SSP FORTRAN library. As well, seven other subroutines, XCALC, XPLACE, XREF, XCONTR, XCENT, XSHR, and XPAND and the function XF are called externally

from SIMPLEX. The purposes of these subprograms are described in the initial comments of their listings.

With the exception of CARLO, all of the above programs were originally designed for practical use. Due to numerical problems, however, only LINLSQ can be used with any degree of success.

All approximate confidence intervals are calculated at the ninety-five percent confidence level. Alterations to the programs and their input could be made which would allow for different levels of confidence.

Those calculations which were done by hand using results from LINLSQ and CARLO could be incorporated into the programs. The test of fit described in section 3.3 could be included in both LINLSQ and CARLO. Those calculations necessary to estimate the variance-covariance matrix of the parameter estimates in CARLO could be included in the program. LINLSQ would be of more practical use if the program and its input were adjusted to predict point estimates and determine confidence intervals for the yields of newly designed electronic units.

Figure 11

Input Format For The Program LINLSQ

10,3			
27,3,450,	1000,553		UNIT 1
25,10,350,	500,144		UNIT 2
31,0,375,	800,574		UNIT 3
16,11,400,	750,101		UNIT 4
10,25,200,	150,92		UNIT 5
35,0,425,	650,496		UNIT 6
29,29,325,	125,79		UNIT 7
21,0,400,	600,241		UNIT 8
21,9,428,	850,337		UNIT 9
17,25,216,	350,219		UNIT 10
2.365			

TABLE 8

RESULTS OF TEST RUN ON THE PROGRAM LINLSQ

Component Family	Estimated Component Family Yield	True Component Family Yield
1	.9899	.9900
2	.9949	.9950
3	.9990	.9990

TABLE 9

RESULTS OF TEST RUN ON THE PROGRAM PREDMLE

Component Family	Estimated Component Family Yield	True Component Family Yield
1	.9900	.9900
2	.9950	.9950
3	.9990	.9990

PROGRAM LISTING - LINLSQ

C THIS PROGRAM TAKES THE LOGARITHM OF THE UNIT YIELDS TO FORM A LINEAR
 C EQUATION IN THE LOGARITHMS OF THE COMPONENT YIELDS, THESE EQUATIONS
 C ARE SOLVED USING MULTIPLE REGRESSION,

```
C
  DIMENSION Q(50,25),Y(50),ADJYLD(50,1),QTRANS(25,50),CMPYLD(25),
  $ L(25),W(50),CONS(25,1),MWORK(25),NEW(50),DER(25,25),Z(25,50),
  $ A(325),R(25,25),QADJ(50,25),YIELD(50)
  REAL NEW
  READ(9,*) N,M
```

C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF
 C COLUMNS (COMPONENT FAMILIES).

```
C
  CALL OLS(N,MWORK,Q,YIELD,QTRANS,CMPYLD,L,M,NEW,
  $ DER,Z,CONS,Y,W,A,ADJYLD,QADJ,R)
  STOP
  END
```

```
C
  SUBROUTINE OLS(N,MWORK,Q,YIELD,QTRANS,CMPYLD,L,M,
  $ NEW,DER,Z,CONS,Y,W,A,ADJYLD,QADJ,R)
  DIMENSION Q(N,M),A(325),ADJYLD(N,1),QTRANS(M,N),
  $ CMPYLD(M),R(M,M),W(N),Y(N),L(M),MWORK(M),NEW(N),
  $ DER(M,M),QADJ(N,M),YIELD(N),Z(M,N),CONS(M,1)
  REAL NEW
```

```
C
  WRITE(8,200)
  200 FORMAT(20X,'DATA MATRIX:',/,/,/)
```

```
C
  DO 10 I=1,N
  READ(9,*)(Q(I,J),J=1,M),NEW(I),Y(I)
  WRITE(8,210)(Q(I,J),J=1,M)
  210 FORMAT(3X,25F4.0)
  10 CONTINUE
```

```
C
  WRITE(8,220)
  220 FORMAT(1H1)
  WRITE(8,230)
  230 FORMAT(/,/,/)
```

C CALCULATE THE YIELDS AND ADJUST THE YIELDS AND THE Q MATRIX FOR
 C UNEQUAL VARIANCES. THEN PRINT OUT THE UNITS ACCEPTED, THE NUMBER
 C TESTED, THE YIELD AND THE ADJUSTED YIELDS.

```
C
  WRITE(8,240)
  240 FORMAT(14X,'UNIT',13X,'UNITS TESTED',15X,'UNITS ACCEPTED',
  $ 14X,'UNIT YIELD',13X,'ADJUSTED YIELD',/,/)
```

```
C
  DO 15 I=1,N
  YIELD(I)=Y(I)/NEW(I)
  W(I)=SQRT((NEW(I)-Y(I))/(NEW(I)*Y(I)))
  ADJYLD(I,1)=ALOG(YIELD(I))/W(I)
  DO 20 J=1,M
  QADJ(I,J)=Q(I,J)/W(I)
```

PROGRAM LISTING - LINLSQ (Cont'd)

```

20  CONTINUE
    WRITE(8,250)I,NFW(I),Y(I),YIELD(I),ADJYLD(I,1)
250  FORMAT(15X,I2,2(20X,F5.0),19X,F7.4,17X,F9.4)
15  CONTINUE
C
C DETERMINE THE TRANSPOSE OF THE ADJUSTED Q MATRIX,
C
    DO 25 I=1,N
    DO 30 J=1,M
    QTRANS(J,I)=QADJ(I,J)
30  CONTINUE
25  CONTINUE
C
C NOW WE CAN PERFORM THE ACTUAL REGRESSION,
C
    CALL GMPRD(QTRANS,QADJ,DER,M,N,M)
C
C THE MATRIX DER CONSISTS OF NON NEGATIVE ENTRIES, HENCE WE CAN
C SCALE THE MATRIX SO THAT THE INVERSE OF A MATRIX WITH A SMALLER
C RANGE OF VALUES CAN BE DETERMINED, THIS WILL REDUCE THE CHANCES
C OF THE PROGRAM CRASHING THROUGH A REGISTER OVERFLOW OR UNDERFLOW,
C
    ZZ=1000.*FLOAT(N)
    DO 35 J=1,M
    DO 40 JJ=1,M
    DER(J,JJ)=DER(J,JJ)/ZZ
40  CONTINUE
35  CONTINUE
C
C WE DETERMINE THE INVERSE OF DER USING THE SSP SUBROUTINE SINV
C WHICH DETERMINES THE INVERSE OF POSITIVE DEFINITE SYMMETRIC MATRICES,
C
    LSUM=0
    DO 45 J=1,M
    DO 50 K=1,J
    LSUM=LSUM+1
    A(LSUM)=DER(J,K)
50  CONTINUE
45  CONTINUE
C
    EPS=,001
    CALL SINV(A,M,EPS,IER)
C
    LSUM=0
    DO 55 J=1,M
    DO 60 K=1,J
    LSUM=LSUM+1
    DER(J,K)=A(LSUM)
    DER(K,J)=DER(J,K)
60  CONTINUE
55  CONTINUE
C
C NOW WE HAVE TO RESTORE DER TO ITS ORIGINAL SCALING BEFORE WE
C CAN USE IT.
C

```


PROGRAM LISTING - LINLSQ (Cont'd)

```

DO 65 J=1,M
DO 70 JJ=1,M
DER(J, JJ)=DER(J, JJ)/ZZ
70 CONTINUE
65 CONTINUE
C
CALL GMPRO(DER, QTRANS, Z, M, M, N)
CALL GMPRO(7, ADJYLD, CONS, M, N, 1)
WRITE(8, 220)
WRITE(8, 230)
C
SIGMA=0.0
DO 75 I=1,N
E=0.0
DO 80 J=1,M
E=E+QADJ(I, J)*CONS(J, 1)
80 CONTINUE
E=ADJYLD(I, 1)-E
SIGMA=SIGMA+E**2
75 CONTINUE
NM=N-M
SIGMA=SIGMA/FLOAT(NM)
DO 85 J=1,M
DO 90 JJ=1,M
DER(J, JJ)=DER(J, JJ)*SIGMA
90 CONTINUE
85 CONTINUE
C
WRITE(8, 260)
260 FORMAT(50X, 'COVARIANCE MATRIX', /)
WRITE(8, 270)(J, J=1, M)
270 FORMAT(16(13X, I2), /)
DO 95 I=1, M
WRITE(8, 280) I, (DER(I, J), J=1, I)
280 FORMAT(2X, I2, 16(2X, E13.7))
95 CONTINUE
READ(9, *) T
C
C DETERMINE CONFIDENCE INTERVALS FOR THE ESTIMATES OF THE LOGARITHM
C OF THE COMPONENT YIELDS AND FOR THE COMPONENT YIELD ESTIMATES,
C
WRITE(8, 220)
WRITE(8, 230)
WRITE(8, 290) NM
290 FORMAT(25X, 'APPROXIMATE 95% CONFIDENCE INTERVALS ON', I2, 1X,
$ 'DEGREES OF FREEDOM:', /)
WRITE(8, 300)
300 FORMAT(3X, 'COMPONENT', 12X, 'LOG OF COMPONENT YIELD', 43X,
$ 'COMPONENT YIELD', /)
WRITE(8, 310)
310 FORMAT(10X, 2(' '), 5X, 50(' '), 15X, 36(' '))
DO 100 J=1, M
XLB=CONS(J, 1)-T*SQRT(DER(J, J))
UB=CONS(J, 1)+T*SQRT(DER(J, J))
CMPYLD(J)=EXP(CONS(J, 1))

```

```

EXPLB=EXP(XLB)
EXPUB=EXP(UB)
WRITE(8,320)J,CONS(J,1),XLB,UB,CMPLYD(J),EXPLB,EXPUB
320  FORMAT(10X,I2,5X,E14,6,5X,'(,E14,6,',',E14,6,')',15X,F8,5,5X,
$ '(,E10,5,',',E10,5,')')
100  CONTINUE
C
C FIND APPROXIMATE CONFIDENCE INTERVALS FOR THE UNIT YIELDS USING
C BOTH THE OBSERVED YIELDS AND THE ESTIMATED YIELDS.
C
WRITE(8,220)
WRITE(8,230)
WRITE(8,330)
330  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR UNIT ',
$ 'YIELDS:',/,/,/)
WRITE(8,340)
340  FORMAT(9X,'UNIT',14X,'FOR OBSERVED',35X,'FOR ESTIMATES',/)
WRITE(8,350)
350  FORMAT(10X,2(' '),5X,33(' '),15X,37(' '))
C
DO 105 I=1,N
FAC=YIELD(I)*(1.0-YIELD(I))/NEW(I)
FAC=1.96*SQRT(FAC)
BINLB=YIELD(I)-FAC
BINUB=YIELD(I)+FAC
ESTYLD=0.0
ESTVAR=0.0
C
DO 110 J=1,M
ESTYLD = ESTYLD+Q(I,J)*CONS(J,1)
C
DO 115 K=1,M
ESTVAR=ESTVAR+Q(I,K)*Q(I,J)*DER(J,K)
115  CONTINUE
110  CONTINUE
C
SD=SQRT(ESTVAR)
ESTLB=EXP(ESTYLD-1.96*SD)
ESTUB=EXP(ESTYLD+1.96*SD)
ESTYLD=EXP(ESTYLD)
WRITE(8,360)I,YIELD(I),BINLB,BINUB,ESTYLD,ESTLB,ESTUB
360  FORMAT(10X,I2,5X,F8,5,':',5X,'(,F8,5,',',F8,5,')',15X,
$ F8,5,':',5X,'(,E10,5,',',E10,5,')')
105  CONTINUE
C
C DETERMINE PRINCIPAL COMPONENTS, THAT IS BY CALCULATING THE
C EIGENVECTORS, WE CAN DETERMINE NEW BASES FOR OUR COMPONENTS WHICH
C WILL BE INDEPENDENT.
C
CALL EIGEN(DER,R,M,0)
WRITE(8,220)
C
DO 120 J=1,M
WRITE(8,370)J,DER(J,J)
370  FORMAT(/,20X,'EIGENVALUE(',I2,') = ',E16,8,/)

```

PROGRAM LISTING - LINLSQ (Cont'd)

```
380 WRITE(8,380)(J,I,R(I,J),I=1,M)
120 FORMAT(25X,'EIGENVECTOR(',I2,',',I2,',') = ',E16.8)
C CONTINUE
RETURN
END
```

PROGRAM LISTING - CARLO

C THIS PROGRAM GENERATES 100 SAMPLES OF YIELD DATA AND COMPUTES
 C CONFIDENCE INTERVALS FOR THE ESTIMATES USING THE RESULTS OF ALL
 C OF THE SAMPLES. THE YIELD ESTIMATES FOR EACH SAMPLE IS FOUND USING
 C THE METHOD OF THE PROGRAM LINLSQ.

C
 DIMENSION Q(50,25),Y(50),ADJYLD(50,1),QTRANS(25,50),CMPYLD(25),
 \$ P(50),AC(25),XMEAN(50),DEV(50),XBAR(25),
 \$ SUM(25),S1(50),S2(50),
 \$ L(25),W(50),CONS(25,1),MWORK(25),NEW(50),DER(25,25),Z(25,50),
 \$ A(325),R(25,25),QADJ(50,25),YIELD(50)
 REAL NEW
 READ(9,*) N,M

C
 C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF
 C COLUMNS (COMPONENT FAMILIES).

C
 CALL OLS(N,MWORK,Q,YIELD,QTRANS,CMPYLD,L,M,NEW,
 \$ P,AC,XMEAN,DEV,XBAR,SUM,S1,S2,
 \$ DER,Z,CONS,Y,W,A,ADJYLD,QADJ,R)
 STOP
 END

C
 SUBROUTINE OLS(N,MWORK,Q,YIELD,QTRANS,CMPYLD,L,M,
 \$ NEW,P,AC,XMEAN,DEV,XBAR,SUM,S1,S2,
 \$ DER,Z,CONS,Y,W,A,ADJYLD,QADJ,R)
 DIMENSION Q(N,M),A(325),ADJYLD(N,1),QTRANS(M,N),
 \$ CMPYLD(M),R(M,M),W(N),Y(N),L(M),MWORK(M),NEW(N),
 \$ P(N),AC(M),XMEAN(N),DEV(N),XBAR(M),SUM(M),
 \$ S1(10),S2(10),
 \$ DER(M,M),QADJ(N,M),YIELD(N),Z(M,N),CONS(M,1)
 REAL NEW

C
 WRITE(6,200)
 200 FORMAT(20X,'DATA MATRIX:',/,/,)

C
 DO 10 I=1,N
 READ(9,*)(Q(I,J),J=1,M),NEW(I),Y(I)
 WRITE(6,210)(Q(I,J),J=1,M)
 210 FORMAT(3X,25F4,0)
 10 CONTINUE

C
 WRITE(6,220)
 220 FORMAT(1H1)

C
 AC(1)=.99
 AC(2)=.995
 AC(3)=.999

C
 WRITE(6,231)
 231 FORMAT(22X,'COMPONENT',16X,'YIELD',/)
 WRITE(6,232)(J,AC(J),J=1,M)
 232 FORMAT(25X,I2,20X,F5,3)

C
 C DETERMINE AND PRINT THE TRUE UNIT YIELDS.

C

PROGRAM LISTING - CARLO (Cont'd)

```

WRITE(6,220)
WRITE(6,240)
240 FORMAT(24X,'UNIT',16X,'UNITS TESTED',17X,
S 'TRUE UNIT YIELD',/)
C
DO 11 I=1,N
P(I)=0.0
DO 21 J=1,M
P(I)=P(I)+Q(I,J)*ALOG(AC(J))
21 CONTINUE
P(I)=EXP(P(I))
WRITE(6,250)I,NEW(I),P(I)
250 FORMAT(25X,I2,20X,F5,0,20X,F10,8)
XMEAN(I)=P(I)*NEW(I)
DEV(I)=SQRT(XMEAN(I)*(1.0-P(I)))
S1(I)=0.0
S2(I)=0.0
11 CONTINUE
C
WRITE(6,220)
IX=79
READ(9,*)T
C
DO 61 J=1,M
XBAR(J)=0.0
SUM(J)=0.0
61 CONTINUE
C
DO 41 NSTEP=1,100
C
C GENERATE APPROXIMATE BINOMIAL OBSERVATIONS TO BE USED AS
C THE NUMBER OF UNITS ACCEPTED.
C
DO 51 I=1,N
500 CALL GAUSS(IX,DEV(I),XMEAN(I),Y(I))
IF(Y(I).LT.0.0)GOTO 500
IF(Y(I).GT.NEW(I))GOTO 500
51 CONTINUE
C
C CALCULATE THE YIELDS AND ADJUST THE YIELDS AND THE Q MATRIX FOR
C UNEQUAL VARIANCES. THEN PRINT OUT THE UNITS ACCEPTED, THE NUMBER
C TESTED, THE YIELD AND THE ADJUSTED YIELDS.
C
DO 15 I=1,N
YIELD(I)=Y(I)/NEW(I)
W(I)=SQRT((NEW(I)-Y(I))/(NEW(I)*Y(I)))
ADJYLD(I,1)=ALOG(YIELD(I))/W(I)
DO 20 J=1,M
QADJ(I,J)=Q(I,J)/W(I)
20 CONTINUE
15 CONTINUE
C
C DETERMINE THE TRANSPOSE OF THE ADJUSTED Q MATRIX.
C
DO 25 I=1,N

```

PROGRAM LISTING - CARLO (Cont'd)

```

DO 30 J=1,M
QTRANS(J,I)=QADJ(I,J)
30 CONTINUE
25 CONTINUE
C
C NOW WE CAN PERFORM THE ACTUAL REGRESSION.
C
CALL GMPRD(QTRANS,QADJ,DER,M,N,M)
C
C THE MATRIX DER CONSISTS OF NON NEGATIVE ENTRIES. HENCE WE CAN
C SCALE THE MATRIX SO THAT THE INVERSE OF A MATRIX WITH A SMALLER
C RANGE OF VALUES CAN BE DETERMINED. THIS WILL REDUCE THE CHANCES
C OF THE PROGRAM CRASHING THROUGH A REGISTER OVERFLOW OR UNDERFLOW.
C
ZZ=1000.*FLOAT(N)
DO 35 J=1,M
DO 40 JJ=1,M
DER(J,JJ)=DER(J,JJ)/ZZ
40 CONTINUE
35 CONTINUE
C
C WE DETERMINE THE INVERSE OF DER USING THE SSP SUBROUTINE SINV
C WHICH DETERMINES THE INVERSE OF POSITIVE DEFINITE SYMMETRIC MATRICES.
C
LSUM=0
DO 45 J=1,M
DO 50 K=1,J
LSUM=LSUM+1
A(LSUM)=DER(J,K)
50 CONTINUE
45 CONTINUE
C
EPS=.001
CALL SINV(A,M,EPS,IER)
C
LSUM=0
DO 55 J=1,M
DO 60 K=1,J
LSUM=LSUM+1
DER(J,K)=A(LSUM)
DER(K,J)=DER(J,K)
60 CONTINUE
55 CONTINUE
C
C NOW WE HAVE TO RESTORE DER TO ITS ORIGINAL SCALING BEFORE WE
C CAN USE IT.
C
DO 65 J=1,M
DO 70 JJ=1,M
DER(J,JJ)=DER(J,JJ)/ZZ
70 CONTINUE
65 CONTINUE
C
CALL GMPRD(DER,QTRANS,Z,M,M,N)
CALL GMPRD(Z,ADJYLD,CONS,M,N,1)

```

PROGRAM LISTING - CARLO (Cont'd)

```

C
  SIGMA=0,0
  DO 75 I=1,N
    E=0,0
    DO 80 J=1,M
      E=E+QADJ(I,J)*CONS(J,1)
80    CONTINUE
      E=ADJYLD(I,1)-E
      SIGMA=SIGMA+E**2
75    CONTINUE
      NM=N-M
      SIGMA=SIGMA/FLOAT(NM)
      DO 85 J=1,M
        DO 90 JJ=1,M
          DER(J,JJ)=DER(J,JJ)*SIGMA
90    CONTINUE
85    CONTINUE
C
C
C DETERMINE CONFIDENCE INTERVALS FOR THE ESTIMATES OF THE LOGARITHM
C OF THE COMPONENT YIELDS AND FOR THE COMPONENT YIELD ESTIMATES.
C
  WRITE(6,290)NM
290  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS ON',I2,1X,
  $ 'DEGREES OF FREEDOM:',I,/)
  WRITE(6,300)
300  FORMAT(3X,'COMPONENT',12X,'LOG OF COMPONENT YIELD',43X,
  $ 'COMPONENT YIELD',/)
  WRITE(6,310)
310  FORMAT(10X,2(I=1),5X,50(I=1),15X,36(I=1))
  DO 100 J=1,M
    XLB=CONS(J,1)-T*SQRT(DER(J,J))
    UB=CONS(J,1)+T*SQRT(DER(J,J))
    CMPYLD(J)=EXP(CONS(J,1))
    XBAR(J)=XBAR(J)+CMPYLD(J)
    SUM(J)=SUM(J)+CMPYLD(J)**2
    EXPLB=EXP(XLB)
    EXPUB=EXP(UB)
    WRITE(6,320)J,CONS(J,1),XLB,UB,CMPYLD(J),EXPLB,EXPU
320  FORMAT(10X,I2,5X,E14,6,5X,'( ',E14,6,' ',', ',E14,6,' ')',15X,F8,5,5X,
  $ '( ',E10,5,' ',', ',E10,5,' ')')
100  CONTINUE
C
C FIND APPROXIMATE CONFIDENCE INTERVALS FOR THE UNIT YIELDS USING
C BOTH THE OBSERVED YIELDS AND THE ESTIMATED YIELDS.
C
  WRITE(6,220)
  WRITE(6,330)
330  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR UNIT ',
  $ 'YIELDS:',/,/,/)
  WRITE(6,340)
340  FORMAT(9X,'UNIT',14X,'FOR OBSERVED',35X,'FOR ESTIMATES',/)
  WRITE(6,350)
350  FORMAT(10X,2(I=1),5X,33(I=1),15X,37(I=1))
C

```

PROGRAM LISTING - CARLO (Cont'd)

```

DO 105 I=1,N
FAC=YIELD(I)*(1.0-YIELD(I))/NEW(I)
FAC=1.96*SQRT(FAC)
BINLB=YIELD(I)-FAC
BINUB=YIELD(I)+FAC
ESTYLD=0.0
ESTVAR=0.0
C
DO 110 J=1,M
ESTYLD = ESTYLD+Q(I,J)*CONS(J,1)
C
DO 115 K=1,M
ESTVAR=ESTVAR+Q(I,K)*Q(I,J)*DER(J,K)
115 CONTINUE
110 CONTINUE
C
SD=SQRT(ESTVAR)
ESTLB=EXP(ESTYLD-1.96*SD)
ESTUB=EXP(ESTYLD+1.96*SD)
ESTYLD=EXP(ESTYLD)
360 WRITE(6,360)I,YIELD(I),BINLB,BINUB,ESTYLD,ESTLB,ESTUB
$ F8,5,'!',5X,'(1,F8,5,'!',F8,5,'!)',15X,
$ F8,5,'!',5X,'(1,E10,5,'!',E10,5,'!)'
S1(I)=S1(I)+ESTYLD
S2(I)=S2(I)+ESTYLD**2
105 CONTINUE
C
41 CONTINUE
WRITE(6,220)
WRITE(6,370)
370 FORMAT(20X,'95% APPROXIMATE CONFIDENCE INTERVALS FOR THE I,
$ ICOMPONENT YIELD ESTIMATES',/)
WRITE(6,380)
380 FORMAT(17X,'COMPONENT',12X,'ESTIMATE',12X,
$ 'CONFIDENCE INTERVAL',/)
WRITE(6,385)
385 FORMAT(20X,2('!'),15X,9('!'),11X,21('!'))
C
DO 71 J=1,M
SUM(J)=(SUM(J)-((XBAR(J)**2)/100.))/99.
XBAR(J)=XBAR(J)/100.
XLB=XBAR(J)-1.96*SQRT(SUM(J))
XUB=XBAR(J)+1.96*SQRT(SUM(J))
WRITE(6,390)J,XBAR(J),XLB,XUB
390 FORMAT(20X,I2,15X,F9,6,'!',10X,'(1,F9,6,'!',F9,6,'!)'
71 CONTINUE
C
WRITE(6,220)
WRITE(6,400)
400 FORMAT(20X,'95% CONFIDENCE INTERVALS FOR UNIT YIELD I,
$ ESTIMATES',/)
WRITE(6,410)
410 FORMAT(19X,'UNIT',15X,'ESTIMATE',12X,
$ 'CONFIDENCE INTERVAL',/)
WRITE(6,385)

```


PROGRAM LISTING - CARLO (Cont'd)

```
DO 81 I=1,N
S2(I)=(S2(I)-((S1(I)**2)/100.))/99.
S1(I)=S1(I)/100.
XLB=S1(I)-1.96*SQRT(S2(I))
XUB=S1(I)+1.96*SQRT(S2(I))
WRITE(6,390)I,S1(I),XLB,XUB
CONTINUE

RETURN
END
```

81
C

PROGRAM LISTING - PREDMLE

```

C
C THIS PROGRAM USES THE MAXIMUM LIKELIHOOD ESTIMATION METHOD AND THE
C METHOD OF "SCORING" TO DETERMINE THE YIELD OF COMPONENTS DURING
C PRODUCTION.
C
  DIMENSION Q(35,25),NEW(35),YIELD(35),Y(35),AHAT(25),
  U INF(25,25),L(25),MM(25),S(35),FAC(25),K(35),
  U BB(35,25,25),PREV(25)
  REAL NEW,INF,K
  READ(9,*)N,M
C
C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF COLUMNS
C (COMPONENT FAMILIES).
C
  CALL SCORE(N,M,Q,NEW,YIELD,Y,AHAT,PREV,INF,L,MM,S,FAC,K,BB)
  STOP
  END
C
  SUBROUTINE SCORE(N,M,Q,NEW,YIELD,Y,AHAT,PREV,INF,L,MM,S,FAC,K,
  U BB)
  DIMENSION Q(N,M),NEW(N),YIELD(N),Y(N),AHAT(M),PREV(M),INF(M,M),
  U L(M),MM(M),S(N),FAC(M),K(N),BB(N,M,M)
  REAL NEW,INF,K
C
  DO 35 I=1,N
  READ(9,*)(Q(I,J),J=1,M),NEW(I),Y(I)
35  CONTINUE
C
C DETERMINE CONSTANTS WHICH WILL BE USED THROUGHOUT THE ITERATIVE
C PROCEDURE.
C
  DO 21 I=1,N
  DO 31 KK=1,M
  DO 41 LL=1,MM
  BB(I,KK,LL)=NEW(I)*Q(I,KK)*Q(I,LL)
41  CONTINUE
31  CONTINUE
21  CONTINUE
C
C INITIALIZE THE VALUES
C
  MMM=M-1
C
  NIT=0
  READ(9,*) START
  DO 85 J=1,M
  AHAT(J)=START
85  CONTINUE
C
  WRITE(7,500)NIT
500  FORMAT(/,7X,'NIT = ',I3)
  WRITE(7,550)(J,AHAT(J),J=1,M)
550  FORMAT(15X,'AHAT(',I2,') = ',E13.6)
C

```

PROGRAM LISTING - PREDMLE (Cont'd)

```

C NOW WE BEGIN THE ITERATIVE PROCEDURE.
C
10  NIT=NIT+1
C
    DO 95 J=1,M
    PREV(J)=AHAT(J)
95  CONTINUE
C
C DETERMINE THE ESTIMATES OF THE UNIT ACCEPTANCE PROBABILITIES.
C
    DO 205 I=1,N
    K(I)=0.0
    DO 215 J=1,M
    K(I)=K(I)+G(I,J)*ALOG(AHAT(J))
215 CONTINUE
    K(I)=EXP(K(I))
205 CONTINUE
C
C DETERMINE THE INFORMATION MATRIX AND ITS INVERSE.
C
    DO 105 KK=1,M
    DO 115 LL=1, KK
    INF(KK,LL)=0.0
    DO 100 I=1,N
    INF(KK,LL)=INF(KK,LL)+BB(I, KK, LL)*K(I)/(1.0-K(I))
100 CONTINUE
    INF(KK,LL)=INF(KK,LL)/(AHAT(KK)*AHAT(LL))
115 CONTINUE
105 CONTINUE
C
    DO 110 KK=1,MMM
    III=KK+1
    DO 120 LL=III,M
    INF(KK,LL)=INF(LL, KK)
120 CONTINUE
110 CONTINUE
C
    CALL MINV(INF, M, D, L, MM)
C
C DETERMINE THE SCORE VECTOR.
C
    DO 125 J=1,M
    B=0.0
    DO 135 I=1,N
    B=G(I,J)*(Y(I)-NEW(I))*K(I)
    B=B/(AHAT(J)*(1.0-K(I)))
    S(J)=S(J)+B
135 CONTINUE
125 CONTINUE
C
C DETERMINE THE ADJUSTMENT FACTOR
C
    DO 165 J=1,M
    FAC(J)=0.0
    DO 175 JJ=1,M

```

PROGRAM LISTING - PREDMLE (Cont'd)

```
FAC(J)=FAC(J)+INF(J,JJ)*S(JJ)
175 CONTINUE
165 CONTINUE
C
C DETERMINE THE NEW VALUE OF AHAT.
C
DO 185 J=1,M
AHAT(J)=AHAT(J)+FAC(J)
185 CONTINUE
C
DO 225 J=1,M
IF(AHAT(J).LT.0.75)AHAT(J)=0.75
IF(AHAT(J).GT.1.25)AHAT(J)=1.25
225 CONTINUE
WRITE(7,500) NIT
WRITE(7,550)(J,AHAT(J),J=1,M)
C
DO 195 J=1,M
IF(ABS(AHAT(J)-PREV(J)).GT.0.0000005) GOTO 20
195 CONTINUE
RETURN
C
20 IF(NIT.LT.75)GOTO 10
RETURN
END
```

PROGRAM LISTING - COMB

```

C THIS PROGRAM USES THE METHOD OF THE PROGRAM LINLSQ TO FIND ESTIMATES
C OF THE COMPONENT YIELDS WHICH CAN THEN BE USED AS STARTING VALUES FOR
C FINDING MAXIMUM LIKELIHOOD ESTIMATES USING THE METHOD OF SCORING.
C
  DIMENSION Q(40,20),Y(40),ADJYLD(40,1),QTRANS(20,40),CMPYLD(20),
  $ BB(40,20,20),CONSD(20),S(20),FAC(20),
  $ LWORK(20),W(40),CONS(20,1),MWORK(20),NEW(40),DER(20,20),Z(20,40),
  $ A(320),P(20,20),QADJ(40,20),YIELD(40)
  REAL NEW
  READ(9,*) N,M
C
C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF
C COLUMNS (COMPONENT FAMILIES).
C
  CALL OLS(N,M,Q,YIELD,QTRANS,CMPYLD,LWORK,MWORK,NEW,
  $ DER,Z,CONS,Y,W,A,ADJYLD,QADJ,R,BB,CONSD,S,FAC)
  STOP
  END
C
  SUBROUTINE OLS(N,M,Q,YIELD,QTRANS,CMPYLD,LWORK,MWORK,
  $ NEW,DER,Z,CONS,Y,W,A,ADJYLD,QADJ,R,BB,CONSD,S,FAC)
  DIMENSION Q(N,M),A(325),ADJYLD(N,1),QTRANS(M,N),
  $ BB(N,M,M),CONSD(M),S(M),FAC(M),
  $ CMPYLD(M),R(M,M),W(N),Y(N),LWORK(M),MWORK(M),NEW(N),
  $ DER(M,M),QADJ(N,M),YIELD(N),Z(M,N),CONS(M,1)
  REAL NEW
C
  WRITE(6,200)
200  FORMAT(20X,'DATA MATRIX:',/,/,)
C
  DO 10 I=1,N
  READ(9,*)(Q(I,J),J=1,M),NEW(I),Y(I)
  WRITE(6,210)(Q(I,J),J=1,M)
210  FORMAT(3X,25F4.0)
  10  CONTINUE
C
  WRITE(6,220)
220  FORMAT(1H1)
  WRITE(6,230)
230  FORMAT(/,/)
C
C CALCULATE THE YIELDS AND ADJUST THE YIELDS AND THE Q MATRIX FOR
C UNEQUAL VARIANCES. THEN PRINT OUT THE UNITS ACCEPTED, THE NUMBER
C TESTED AND THE YIELDS.
C
  WRITE(6,240)
240  FORMAT(14X,'UNIT',13X,'UNITS TESTED',15X,'UNITS ACCEPTED',
  $ 14X,'UNIT YIELD',/)
C
  DO 15 I=1,N
  YIELD(I)=Y(I)/NEW(I)
  W(I)=SQRT((NEW(I)-Y(I))/(NEW(I)*Y(I)))
  ADJYLD(I,1)=ALOG(YIELD(I))/W(I)
  DO 20 J=1,M
  QADJ(I,J)=Q(I,J)/W(I)

```

PROGRAM LISTING - COMB (Cont'd)

```

20  CONTINUE
    WRITE(6,250) I,NEW(I),Y(I),YIELD(I)
250  FORMAT(15X,I2,2(20X,F5.0),19X,F7.4)
15  CONTINUE
C
C DETERMINE THE TRANSPOSE OF THE ADJUSTED Q MATRIX.
C
    DO 25 I=1,N
    DO 30 J=1,M
    QTRANS(J,I)=QADJ(I,J)
30  CONTINUE
25  CONTINUE
C
C NOW WE CAN PERFORM THE ACTUAL REGRESSION.
C
    CALL GMPRD(QTRANS,QADJ,DER,M,N,M)
C
C THE MATRIX DER CONSISTS OF NON NEGATIVE ENTRIES. HENCE WE CAN
C SCALE THE MATRIX SO THAT THE INVERSE OF A MATRIX WITH A SMALLER
C RANGE OF VALUES CAN BE DETERMINED. THIS WILL REDUCE THE CHANCES
C OF THE PROGRAM CRASHING THROUGH A REGISTER OVERFLOW OR UNDERFLOW.
C
    ZZ=1000.*FLOAT(N)
    DO 35 J=1,M
    DO 40 JJ=1,M
    DER(J,JJ)=DER(J,JJ)/ZZ
40  CONTINUE
35  CONTINUE
C
C WE DETERMINE THE INVERSE OF DER USING THE SSP SUBROUTINE SINV
C WHICH DETERMINES THE INVERSE OF POSITIVE DEFINITE SYMMETRIC MATRICES.
C
    LSUM=0
    DO 45 J=1,M
    DO 50 K=1,J
    LSUM=LSUM+1
    A(LSUM)=DER(J,K)
50  CONTINUE
45  CONTINUE
C
    EPS=.001
    CALL SINV(A,M,EPS,IER)
C
    LSUM=0
    DO 55 J=1,M
    DO 60 K=1,J
    LSUM=LSUM+1
    DER(J,K)=A(LSUM)
    DER(K,J)=DER(J,K)
60  CONTINUE
55  CONTINUE
C
C NOW WE HAVE TO RESTORE DER TO ITS ORIGINAL SCALING BEFORE WE
C CAN USE IT.
C

```

PROGRAM LISTING - COMB (Cont'd)

```

DO 65 J=1,M
DO 70 JJ=1,M
DER(J, JJ) =DER(J, JJ) /ZZ
70 CONTINUE
65 CONTINUE
C
CALL GMPRD(DER, QTRANS, Z, M, M, N)
CALL GMPRD(Z, ADJYLD, CONS, M, N, 1)
WRITE(6, 220)
WRITE(6, 230)
C
DO 19 J=1, M
CMPYLD(J) =EXP(CONS(J, 1))
19 CONTINUE
C
C DETERMINE THE CONSTANTS WHICH WILL BE USED THROUGHOUT THE ITERATIVE
C PROCEDURE.
C
DO 21 I=1, N
DO 31 KK=1, M
DO 41 LL=1, KK
BB(I, KK, LL) =NEW(I) *Q(I, KK) *Q(I, LL)
41 CONTINUE
31 CONTINUE
21 CONTINUE
C
C INITIALIZE THE VALUES
C
MMM=M-1
NIT=0
WRITE(6, 600) NIT
600 FORMAT(/, 7X, 'NIT = ', I3)
WRITE(6, 550) (J, CMPYLD(J), J=1, M)
550 FORMAT(15X, 'CMPYLD(', I2, ') = ', E13.6)
C
C NOW BEGIN THE ITERATIVE PROCEDURE
C
500 NIT=NIT+1
DO 95 J=1, M
CONS(J, 1) =CMPYLD(J)
95 CONTINUE
C
CALL COMYLD(W, Q, M, N, CMPYLD)
CALL COMINF(BB, M, N, DER, W, CONDS, LWORK, MWORK, CMPYLD)
C
C DETERMINE THE SCORE VECTOR.
C
DO 125 J=1, M
B=C.0
DO 135 I=1, N
B=Q(I, J) * (Y(I) -NEW(I) *W(I))
B=B/(CMPYLD(J) * (1.0 -W(I)))
S(J) =S(J) +B
135 CONTINUE

```

PROGRAM LISTING - COMB (Cont'd)

```

125  CONTINUE
C
    DO 235 J=1,M
    FAC(J)=0.0
    DO 245 JJ=1,M
    FAC(J)=FAC(J)+DER(J,JJ)*S(JJ)
245  CONTINUE
235  CONTINUE
C
C DETERMINE THE NEW ESTIMATE OF THE COMPONENT YIELD
C
    DO 185 J=1,M
    CMPYLD(J)=CMPYLD(J)+FAC(J)
185  CONTINUE
C
    WRITE(6,600)NIT
    WRITE(6,550)(J,CMPYLD(J),J=1,M)
C
    DO 195 J=1,M
    IF(ABS(CMPYLD(J)-CONS(J,1)).GT.0.00005) GOTO 510
195  CONTINUE
    RETURN
C
510  IF(NIT.LT.150)GOTO 500
    IF(NIT.EQ.250)RETURN
    WRITE(6,260)
260  FORMAT(50X,'COVARIANCE MATRIX',/)
    WRITE(6,270)(J,J=1,M)
270  FORMAT(16(13X,I2),/)
    DO 96 I=1,M
    WRITE(6,280)I,(DER(I,J),J=1,I)
280  FORMAT(2X,I2,16(2X,E13.7))
96   CONTINUE
    READ(9,*)T
C
C DETERMINE APPROXIMATE CONFIDENCE INTERVALS FOR OUR COMPONENT
C FAMILY YIELD ESTIMATES.
C
    WRITE(6,220)
    WRITE(6,230)
    WRITE(6,290)
290  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR',
$ ' COMPONENT YIELDS',/,/)
    WRITE(6,300)
300  FORMAT(7X,'COMPONENT',6X,'ESTIMATED',8X,'UNCONDITIONAL',
$ 16X,'CONDITIONAL')
    WRITE(6,305)
305  FORMAT(8X,'FAMILY',10X,'YIELD',10X,'VARIANCE C.I.',
$ 16X,'VARIANCE C.I.',/)
    WRITE(6,310)
310  FORMAT(10X,2(' - '),10X,8(' - '),6X,19(' - '),5X,23(' - '))
C
    DO 100 J=1,M
    COMPLB=CMPYLD(J)-1.96*SQRT(DER(J,J))
    COMPUB=CMPYLD(J)+SQRT(DER(J,J))

```


PROGRAM LISTING - COMB (Cont'd)

```

CONDLB=CMPYLD (J) - 1.96*CONDS D (J)
CONDUB=CMPYLD (J) + 1.96*CONDS D (J)
WRITE (6,390) J,CMPYLD (J) ,COMPLB,COMPUB,CONDLB,CONDUB
390  FORMAT (10X,I2,10X,F8.5,':',5X,'(',F8.5,',',F8.5,')',
$ 5X,'(',F10.5,',',F10.5,')')
100  CONTINUE
C
C PRINT OUT THE ESTIMATED UNIT YIELDS AND COMPARE WITH THAT OBSERVED.
C
WRITE (6,220)
WRITE (6,230)
WRITE (6,330)
330  FORMAT (9X,'UNIT',11X,'YIELD ESTIMATE',9X,'OBSERVED YIELD',
$ 4X,'95% C.I. FOR OBSERVED YIELD',/)
WRITE (6,410)
410  FORMAT (10X,2 ('-'),2 (15X,8 ('-')),15X,19 ('-'))
C
DO 105 I=1,N
FACT=YIELD (I) * (1.0-YIELD (I)) /NEW (I)
FACT=1.96*SQRT (FACT)
BINLB=YIELD (I) -FACT
BINUB=YIELD (I) +FACT
WRITE (6,420) I,W (I),YIELD (I),BINLB,BINUB
420  FORMAT (10X,I2,2 (15X,F8.5),15X,'(',F8.5,',',F8.5,')')
105  CONTINUE
C
C DETERMINE PRINCIPAL COMPONENTS, THAT IS BY CALCULATING THE
C EIGENVECTORS, WE CAN DETERMINE NEW BASES FOR OUR COMPONENTS WHICH
C WILL BE INDEPENDENT.
C
CALL EIGEN (DER,R,M,0)
WRITE (6,220)
C
DO 120 J=1,M
WRITE (6,370) J,DER (J,J)
370  FORMAT (/ ,20X,'EIGENVALUE (' ,I2,') = ',E16.8,/)
WRITE (6,380) (J,I,R (I,J),I=1,M)
380  FORMAT (25X,'EIGENVECTOR (' ,I2,',' ,I2,') = ',E16.8)
120  CONTINUE
C
RETURN
END

```

SUBROUTINE LISTING - COMYLD

C THIS SUBROUTINE DETERMINES THE ESTIMATES OF THE UNIT YIELDS.

```

C
  SUBROUTINE COMYLD(W,Q,M,N,CMPYLD)
  DIMENSION W(N),Q(N,M),CMPYLD(M)
C
  DO 10 I=1,N
  W(I)=0.0
  DO 15 J=1,M
  W(I)=W(I)+Q(I,J)*ALOG(CMPYLD(J))
15  CONTINUE
  W(I)=EXP(W(I))
10  CONTINUE
C
  RETURN
  END

```

SUBROUTINE LISTING - COMINF

C THIS SUBROUTINE CALCULATES THE INFORMATION MATRIX.

```

C
  SUBROUTINE COMINF(BB,M,N,XINF,W,CONSD,LWORK,MWORK,CMPYLD)
  DIMENSION BB(N,M,M),XINF(M,M),W(N),LWORK(M),MWORK(M),
$ CONSD(M),CMPYLD(M)
C
  DO 10J=1,M
  DO 15K=1,J
  XINF(J,K)=0.0
  DO 20 I=1,N
  XINF(J,K)=XINF(J,K)+BB(I,J,K)*W(I)/(1.0-W(I))
20  CONTINUE
  XINF(J,K)=XINF(J,K)/(CMPYLD(J)*CMPYLD(K))
  XINF(K,J)=XINF(J,K)
  IF(J.EQ.K) CONSD(J)=1.0/SQRT(XINF(J,J))
15  CONTINUE
10  CONTINUE
C
  CALL MINV(XINF,M,D,LWORK,MWORK)
C
  RETURN
  END

```

C THIS PROGRAM TAKES THE LOGARITHM OF THE UNIT YIELDS TO FORM A LINEAR
 C EQUATION IN THE LOGARITHMS OF THE COMPONENT YIELDS. THESE EQUATIONS
 C ARE SOLVED USING MULTIPLE REGRESSION. THESE ESTIMATES ARE THEN
 C USED TO CONSTRUCT THE VERTICES OF A SIMPLEX WHICH WILL BE USED
 C TO DETERMINE THE MAXIMUM LIKELIHOOD ESTIMATES OF THE COMPONENT
 C YIELDS.

C
 C DIMENSION Q(50,25),Y(50),YIELD(50),QTRANS(25,50),CMPYLD(25),
 \$ L(25),W(50),CONS(25,1),MWORK(25),NEW(50),DER(25,25),Z(25,50),
 \$ VERT(26,25),CENT(25),FLIKE(26),VERTR(25),VERTE(25),AHAT(25),
 \$ VERTC(25),CONSDS(25),ADJYLD(50,1),QADJ(50,25),A(325),EST(50)
 REAL NEW
 READ(9,*) N,M

C
 C N IS THE NUMBER OF ROWS (UNITS) & M IS THE NUMBER OF
 C COLUMNS (COMPONENT FAMILIES).
 MPLUS=M+1

C
 C CALL OLS(A,N,EST,MWORK,Q,YIELD,QTRANS,CMPYLD,L,M,NEW,
 \$ DER,Z,CONS,Y,W,VERT,CENT,FLIKE,VERTR,VERTE,AHAT,VERTC,MPLUS,
 \$ QADJ,ADJYLD,CONSDS)
 STOP
 END

C
 C SUBROUTINE OLS(A,N,EST,MWORK,Q,YIELD,QTRANS,CMPYLD,L,M,NEW,
 \$ DER,Z,CONS,Y,W,VERT,CENT,FLIKE,VERTR,VERTE,AHAT,VERTC,MPLUS,
 \$ QADJ,ADJYLD,CONSDS)
 DIMENSION Q(N,M),VERT(MPLUS,M),CENT(M),FLIKE(MPLUS),YIELD(N),
 \$ CMPYLD(M),EST(N),QTRANS(M,N),W(N),Y(N),L(M),MWORK(M),NEW(N),
 \$ DER(M,M),VERTR(M),VERTE(M),AHAT(M),VERTC(M),Z(M,N),CONS(M,1),
 \$ A(325),CONSDS(M),ADJYLD(N,1),QADJ(N,M)
 REAL NEW

C
 C WRITE(6,200)
 200 FORMAT(20X,'DATA MATRIX',/,/,)

C
 C DO 10 J=1,N
 READ(9,*)(Q(I,J),J=1,M),NEW(I),Y(I)
 WRITE(6,210)(Q(I,J),J=1,M)
 210 FORMAT(3X,25F4,0)
 10 CONTINUE

C
 C WRITE(6,220)
 220 FORMAT(1H1)

C
 C CALCULATE THE YIELDS AND ADJUST FOR UNEQUAL VARIANCES.

C
 C WRITE(6,230)
 230 FORMAT(14X,'UNIT',13X,'UNITS TESTED',15X,'UNITS ACCEPTED',
 \$ 14X,'UNIT YIELD',13X,'ADJUSTED YIELD',/)

C
 C DO 15 I=1,N
 YIELD(I)=Y(I)/NEW(I)
 W(I)=SQRT((NEW(I)-Y(I))/(NEW(I)*Y(I)))
 ADJYLD(I,1)=ALOG(YIELD(I))/W(I)

PROGRAM LISTING - SIMPLEX (Cont'd)

```

DO 20 J=1,M
QADJ(I,J)=Q(I,J)/W(I)
20 CONTINUE
WRITE(6,240)I,NEW(I),Y(I),YIELD(I),ADJYLD(I,1)
240 FORMAT(15X,I2,2(20X,F5,0),19X,F7,4,17X,F9,4)
15 CONTINUE
C
C DETERMINE THE TRANSPOSE OF THE ADJUSTED Q MATRIX.
C
DO 25 I=1,N
DO 30 J=1,M
QTRANS(J,I)=QADJ(I,J)
30 CONTINUE
25 CONTINUE
C
C NOW WE CAN PERFORM THE ACTUAL REGRESSION.
C
CALL GMPRD(QTRANS,QADJ,DER,M,N,M)
C
C THE MATRIX DER CONSISTS OF NON NEGATIVE ENTRIES. HENCE WE CAN
C SCALE THE MATRIX SO THAT THE INVERSE OF A MATRIX WITH A SMALLER
C RANGE OF VALUES CAN BE DETERMINED. THIS WILL REDUCE THE CHANCES
C OF THE PROGRAM CRASHING THROUGH A REGISTER OVERFLOW OR UNDERFLOW.
C
ZZ=10000.*FLOAT(N)
C
DO 35 J=1,M
DO 40 JJ=1,M
DER(J,JJ)=DER(J,JJ)/ZZ
40 CONTINUE
35 CONTINUE
C
C WE DETERMINE THE INVERSE OF DER USING THE SSP SUBROUTINE SINV
C WHICH DETERMINES THE INVERSE OF POSITIVE DEFINITE SYMMETRIC MATRICES.
C
LSUM=0
C
DO 45 J=1,M
DO 50 K=1,J
LSUM=LSUM+1
A(LSUM)=DER(J,K)
50 CONTINUE
45 CONTINUE
C
EPS=.001
CALL SINV(A,M,EPS,IER)
LSUM=0
C
DO 55 J=1,M
DO 60 K=1,J
LSUM=LSUM+1
DER(J,K)=A(LSUM)
DER(K,J)=DER(J,K)
60 CONTINUE

```

PROGRAM LISTING - SIMPLEX (Cont'd)

```

55  CONTINUE
C
C NOW WE HAVE TO RESTORE DER TO ITS ORIGINAL SCALING BEFORE WE
C CAN USE IT.
C
    DO 65 J=1,M
    DO 70 JJ=1,M
    DER(J,JJ)=DER(J,JJ)/ZZ
70  CONTINUE
65  CONTINUE
C
    CALL GMPRD(DER,QTRANS,Z,M,M,N)
    CALL GMPRD(Z,ADJYLD,CONS,M,N,1)
C
    DO 75 J=1,M
    CMPYLD(J)=EXP(CONS(J,1))
75  CONTINUE
C
    WRITE(6,220)
    WRITE(6,250)
250  FORMAT(30X,'STARTING VALUES FOR THE SIMPLEX PROCEDURE:')
    WRITE(6,260)(I,CMPYLD(I),I=1,M)
260  FORMAT(15X,'COMPONENT YIELD('I,I2,') = ',F15,7)
    ALPHA=1.0
    BETA=.5
    GAMMA=1.5
C
C DETERMINE THE VERTICES OF AN M DIMENSIONAL SIMPLEX WITH WHICH TO
C START THE SIMPLEX PROCEDURE.
C
    NCOUNT=0
    NSTOP=M*15
    WRITE(6,220)
C
    DO 80 J=1,M
    VERT(1,J)=CMPYLD(J)
80  CONTINUE
C
    DO 85 I=1,M
    DO 90 J=1,M
    VERT(I+1,J)=CMPYLD(J)
    IF(I.EQ,J)VERT(I+1,J)=CMPYLD(J)*.0005
90  CONTINUE
85  CONTINUE
C
    CALL XCALC(N,M,Q,MPLUS,VERT,FLIKE,AHAT,Y,NEW)
C
C AT THIS POINT WE CAN ACTUALLY BEGIN THE SIMPLEX PROCEDURE.
C
500  IF(NCOUNT.GE.NSTOP) GOTO 550
    CALL XCENT(M,MPLUS,VERT,CENT)
    NCOUNT=NCOUNT+1
C
C FIRST WE TRY A REFLECTION OF THE VERTEX WHICH GIVES A MINIMUM
C VALUE TO THE LIKELIHOOD FUNCTION.

```

PROGRAM LISTING - SIMPLEX (Cont'd)

```

CALL XREF(M,MPLUS,ALPHA,VERT,CENT,VERTR)
FLIKER=XF(N,M,Q,VERTR,Y,NEW)
1 IF(FLIKE(1),GE,FLIKER,AND,FLIKER,GE,FLIKE(M))GOTO 510
2 IF(FLIKER,GT,FLIKE(1)) GOTO 520
3 IF(FLIKE(M),GT,FLIKER,AND,FLIKER,GT,FLIKE(M+1)) GOTO 530
4 IF(FLIKE(M+1),GT,FLIKER) GOTO 540
WRITE(6,270)
270 FORMAT(10X,'PROCEDURE HALTED!')
RETURN
C
C IF CONDITIONS OF STATEMENT 1 ARE SATISFIED, WE REPLACE THE VERTEX WITH
C MINIMUM LIKELIHOOD FUNCTION WITH THE REFLECTED POINT AND THEN RESTART
C THE PROCEDURE.
C
510 CALL XPLACE(M,MPLUS,VERT,FLIKE,VERTR,FLIKER)
WRITE(6,280)NCOUNT,FLIKE(1)
280 FORMAT(10X,'NCOUNT =',I4,10X,'REFLECTION!',9X,'LIKELIHOOD = ',
$ E18,10)
GOTO 500
C
C IF CONDITIONS OF STATEMENT 2 ARE SATISFIED WE TRY AN EXPANSION AND
C THEN RESTART THE PROCEDURE.
C
520 CALL XPAND(M,GAMMA,VERTE,CENT,VERTR)
FLIKEE=XF(N,M,Q,VERTE,Y,NEW)
IF(FLIKEE,GT,FLIKE(1))CALL XPLACE(M,MPLUS,VERT,FLIKE,VERTE,FLIKEE)
IF(FLIKEE,LE,FLIKE(1))CALL XPLACE(M,MPLUS,VERT,FLIKE,VERTR,FLIKER)
WRITE(6,290)NCOUNT,FLIKE(1)
290 FORMAT(10X,'NCOUNT =',I4,10X,'EXPANSION!',10X,
$ 'LIKELIHOOD = ',E18,10)
GOTO 500
C
C IF CONDITIONS OF STATEMENT 3 ARE SATISFIED WE TRY A CONTRACTION.
C IF SUCCESSFUL WE RESTART THE PROCEDURE, OTHERWISE WE SHRINK THE
C SIMPLEX ABOUT THE POINT WITH THE HIGHEST LIKELIHOOD VALUE.
C
530 CALL XCONTR(M,MPLUS,BETA,VERT,VERTC,CENT)
FLIKEC=XF(N,M,Q,VERTC,Y,NEW)
IF(FLIKEC,GE,FLIKE(M+1)) GOTO 540
IF(FLIKE(M+1),GT,FLIKEC)CALL XPLACE(M,MPLUS,VERT,FLIKE,VERTC,
$ FLIKEC)
WRITE(6,300)NCOUNT,FLIKE(1)
300 FORMAT(10X,'NCOUNT =',I4,10X,'CONTRACTION!',10X,
$ 'LIKELIHOOD = ',E18,10)
GOTO 500
C
C IF CONTRACTION FAILS WE SHRINK THE SIMPLEX ABOUT THE VERTEX WHICH
C HAS THE GREATEST LIKELIHOOD VALUE.
C
540 CALL XSHR(M,MPLUS,VERT,FLIKE)
CALL XCALC(N,M,Q,MPLUS,VERT,FLIKE,AHAT,Y,NEW)
WRITE(6,310)NCOUNT,FLIKE(1)
310 FORMAT(10X,'NCOUNT =',I4,10X,'SHRINK!',13X,'LIKELIHOOD = ',
$ E18,10)

```

PROGRAM LISTING - SIMPLEX (Cont'd)

```

      GOTO 500
C
C DETERMINE THE UNIT YIELDS IN ORDER TO ESTIMATE THE COVARIANCE MATRIX.
C
550  LSUM=0.0
C
      DO 95 I=1,N
      W(I)=0.0
      DO 100 J=1,M
      W(I)=W(I)+Q(I,J)*ALOG(VERT(1,J))
100  CONTINUE
      W(I)=EXP(W(I))
95   CONTINUE
C
C ESTIMATE THE VARIANCE-COVARIANCE MATRIX.
C
      DO 105 J=1,M
      DO 110 K=1,J
      LSUM=LSUM+1
      A(LSUM)=0.0
C
      DO 115 I=1,N
      IF(Q(I,J).EQ.0.0)GOTO 115
      IF(Q(I,K).EQ.0.0)GOTO 115
      XNUM=NEW(I)*Q(I,K)*Q(I,J)*W(I)
      DEN=VERT(1,J)*VERT(1,K)*(1.0-W(I))
      A(LSUM)=A(LSUM)+XNUM/DEN
115  CONTINUE
C
      IF(K.EQ.J)CONDS(D(J))=1.0/SQRT(A(LSUM))
      A(LSUM)=A(LSUM)/ZZ
110  CONTINUE
105  CONTINUE
C
      EPS=10.E-5
      CALL SINVA(A,M,EPS,IER)
      LSUM=0
C
      DO 120 J=1,M
      DO 125 K=1,J
      LSUM=LSUM+1
      DER(J,K)=A(LSUM)/ZZ
      DER(K,J)=DER(J,K)
125  CONTINUE
120  CONTINUE
C
      WRITE(6,220)
      WRITE(6,320)
320  FORMAT(50X,'COVARIANCE MATRIX',/)
      WRITE(6,330)(J,J=1,M)
330  FORMAT(16(13X,I2),/)
C
      DO 130 J=1,M
      WRITE(6,340)J,(DER(I,J),I=1,J)
340  FORMAT(2X,I2,16(2X,E13.7))

```

PROGRAM LISTING - SIMPLEX (Cont'd)

```

130 CONTINUE
C
C DETERMINE APPROXIMATE CONFIDENCE INTERVALS FOR OUR COMPONENT
C FAMILY YIELD ESTIMATES,
C
      WRITE(6,220)
      WRITE(6,350)
350  FORMAT(25X,'APPROXIMATE 95% CONFIDENCE INTERVALS FOR',
$ 1 COMPONENT YIELDS!','/)
      WRITE(6,360)
360  FORMAT(7X,'COMPONENT',6X,'ESTIMATED',8X,'UNCONDITIONAL',
$ 16X,'CONDITIONAL')
      WRITE(6,370)
370  FORMAT(8X,'FAMILY',10X,'YIELD',10X,'VARIANCE C.I.',
$ 16X,'VARIANCE C.I.',/)
      WRITE(6,380)
380  FORMAT(10X,2(' '),10X,8(' '),6X,19(' '),5X,23(' '))
C
      DO 135 J=1,M
      COMPLB=VERT(1,J)-1.96*SQRT(DER(J,J))
      COMPUB=VERT(1,J)+1.96*SQRT(DER(J,J))
      CONDLB=VERT(1,J)-1.96*CONDSO(J)
      CONDUB=VERT(1,J)+1.96*CONDSO(J)
      WRITE(6,390)J,VERT(1,J),COMPLB,COMPUB,CONDLB,CONDUB
390  FORMAT(10X,I2,10X,F8.5,'!',5X,'(1,F8.5,1,1,F8.5,1)!',
$ 5X,'(1,F10.5,1,1,F10.5,1)')
135  CONTINUE
C
C PRINT OUT THE ESTIMATED YIELD AND COMPARE WITH THAT OBSERVED,
C
      WRITE(6,220)
      WRITE(6,400)
400  FORMAT(9X,'UNIT',11X,'YIELD ESTIMATE',9X,
$ 1OBSERVED YIELD',4X,'95% C.I. FOR OBSERVED YIELD',/)
      WRITE(6,410)
410  FORMAT(10X,2(' '),2(15X,8(' ')),15X,19(' '))
C
      DO 140 I=1,N
      FAC=YIELD(I)*(1.0-YIELD(I))/NEW(I)
      FAC=1.96*SQRT(FAC)
      BINLB=YIELD(I)-FAC
      BINUB=YIELD(I)+FAC
      WRITE(6,420)I,W(I),YIELD(I),BINLB,BINUB
420  FORMAT(10X,I2,2(15X,F8.5),15X,'(1,F8.5,1,1,F8.5,1)')
140  CONTINUE
C
      RETURN
      END

```


SUBROUTINE LISTING - XCALC

```

SUBROUTINE XCALC(N,M,Q,MPLUS,VERT,FLIKE,AHAT,Y,NEW)

```

```

C
C THIS SUBROUTINE CALCULATES THE VALUES OF THE LIKELIHOOD FUNCTION AT
C ALL OF THE VERTICES AND SORTS THE VERTICES IN ORDER OF SIZE OF THEIR
C LIKELIHOOD FUNCTIONS (LARGEST TO SMALLEST).

```

```

C
  DIMENSION VERT(MPLUS,M),Y(N),NEW(N),FLIKE(MPLUS),AHAT(M),Q(N,M)
  REAL NEW

```

```

C
  DO 10 I=1,MPLUS
  DO 15 J=1,M
  AHAT(J)=VERT(I,J)
15 CONTINUE
  FLIKE(I)=XF(N,M,Q,AHAT,Y,NEW)
10 CONTINUE

```

```

C
  DO 20 I=1,M
  IPLUS=I+1
  DO 25 II=IPLUS,MPLUS
  IF(FLIKE(I),GE,FLIKE(II)) GOTO 25
  DO 30 J=1,M
  TEMP=VERT(I,J)
  VERT(I,J)=VERT(II,J)
  VERT(II,J)=TEMP
30 CONTINUE
  TEMP=FLIKE(I)
  FLIKE(I)=FLIKE(II)
  FLIKE(II)=TEMP
25 CONTINUE
20 CONTINUE

```

```

C
  RETURN
  END

```

```

SUBROUTINE XPLACE(M,MPLUS,VERT,FLIKE,VERTR,FLIK)
C
C THIS SUBROUTINE PLACES OUR NEW VERTEX IN THE PROPER ORDER AMONGST THE
C OTHER VERTICES
C
  DIMENSION VERT(MPLUS,M),FLIKE(MPLUS),VERTR(M)
C
C REPLACE THE VERTEX WITH THE LEAST LIKELIHOOD BY OUR NEWLY CHOSEN
C VERTEX.
C
  FLIKE(MPLUS)=FLIK
  DO 10 J=1,M
  VERT(MPLUS,J)=VERTR(J)
10  CONTINUE
C
  DO 15 I=1,M
  IF(FLIKE(MPLUS-I).GE.FLIKE(MPLUS-I))GOTO 500
  DO 20 J=1,M
  TEMP=VERT(MPLUS-I,J)
  VERT(MPLUS-I,J)=VERT(MPLUS-I+1,J)
  VERT(MPLUS-I+1,J)=TEMP
20  CONTINUE
  TEMP=FLIKE(MPLUS-I)
  FLIKE(MPLUS-I)=FLIKE(MPLUS-I+1)
  FLIKE(MPLUS-I+1)=TERM
15  CONTINUE
C
500  RETURN
  END

```

SUBROUTINE LISTING - XREF

```

SUBROUTINE XREF(M,MPLUS,ALPHA,VERT,CENT,VERTR)
C
C THIS SUBROUTINE FINDS A POINT REFLECTED THROUGH THE CENTROID
C FROM THE VERTEX AT WHICH THE FUNCTION IS MINIMUM.
C
  DIMENSION VERT(MPLUS,M),CENT(M),VERTR(M)
  DO 10 J=1,M
  VERTR(J)=(1,0+ALPHA)*CENT(J)-ALPHA*VERT(MPLUS,J)
10  CONTINUE
C
  RETURN
  END

```

FUNCTION LISTING - XF

```
FUNCTION XF(N,M,Q,AHAT,Y,NEW)
```

```

C
C THIS FUNCTION SUBPROGRAM DETERMINES THE LOGARITHM OF THE
C LIKELIHOOD FUNCTION AT A PARTICULAR VERTEX. THE LIKELIHOOD
C FUNCTION WILL HAVE A MAXIMUM AT THE SAME POINT AS THE LOG
C OF THE LIKELIHOOD FUNCTION.
C
  DIMENSION Q(N,M),NEW(N),Y(N),AHAT(M)
  REAL NEW
  XF=0.0
  DO 15 I=1,N
  XK=0.0
  DO 25 J=1,M
  XK=XK+Q(I,J)*ALOG(AHAT(J))
25 CONTINUE
  IF(XK,GE.0,0)GOTO 35
  XK=Y(I)*XK+(NEW(I)-Y(I))*ALOG(1.0-EXP(XK))
  XF=XF+XK
15 CONTINUE
  RETURN
35 XF=16,E=65
RETURN
  END

```

SUBROUTINE LISTING - XCONTR

```
SUBROUTINE XCONTR(M,MPLUS,BETA,VERT,VERTC,CENT)
```

```

C
C THIS SUBROUTINE DECREASES THE SIZE OF THE SIMPLEX BY MOVING THE
C REFLECTED VERTEX IN.
C
  DIMENSION VERT(MPLUS,M),VERTC(M),CENT(M)
C
  DO 10 J=1,M
  VERTC(J)=BETA*VERT(MPLUS,J)+(1.0-BETA)*CENT(J)
10 CONTINUE
C
  RETURN
  END

```

SUBROUTINE LISTING - XCENT

```

SUBROUTINE XCENT(M,MPLUS,VERT,CENT)
C THIS SUBROUTINE LOCATES THE CENTROID OF THE SIMPLEX EXCLUDING THE
C VERTEX HAVING THE LEAST LIKELIHOOD.
C
  DIMENSION VERT(MPLUS,M),CENT(M)
  DO 15 I=1,M
  CENT(I)=0,0
  DO 25 J=1,M
  CENT(I)=CENT(I)+VERT(J,I)
25 CONTINUE
  CENT(I)=CENT(I)/FLOAT(M)
15 CONTINUE
  RETURN
  END

```

SUBROUTINE LISTING - XSHR

```

SUBROUTINE XSHR(M,MPLUS,VERT,FLIKE)
C THIS SUBROUTINE SHRINKS THE SIMPLEX,RETAINING THE VERTEX WITH THE
C MAXIMUM LIKELIHOOD.
C
  DIMENSION VERT(MPLUS,M),FLIKE(MPLUS)
  DO 15 I=1,M
  DO 25 J=1,M
  VERT(I+1,J)=(VERT(I+1,J)+VERT(1,J))/2,0
25 CONTINUE
15 CONTINUE
  RETURN
  END

```

SUBROUTINE LISTING - XPAND

```
      SUBROUTINE XPAND(M,GAMMA,VERTE,CENT,VERTR)
```

```
  C  
  C THIS SUBROUTINE EXPANDS THE REFLECTION IN THE DIRECTION ALONG WHICH  
  C A FURTHER IMPROVEMENT OF THE LIKELIHOOD VALUE IS EXPECTED
```

```
  C  
  C      DIMENSION VERTE(M),CENT(M),VERTR(M)
```

```
  C  
  C      DO 10 J=1,M  
  C      VERTE(J)=GAMMA*VERTR(J)+(1,0-GAMMA)*CENT(J)  
  C      CONTINUE
```

```
  C  
  C      RETURN  
  C      END
```

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