

MINICOMPUTER CONTROL
OF A LATEX REACTOR

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By

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ABSTRACT

A minicomputer software and hardware system was developed to monitor and control the particle size growth in the emulsion polymerization of vinyl acetate. The basis of the on line detector was a UV spectrophotometer which measured turbidity as a function of wavelength.

A preliminary investigation was made to develop a technique for converting turbidity measurements into particle size distributions.

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1. INTRODUCTION

Emulsion polymerization is an important process by which several types of polymers are produced commercially as latices. An important property of the latex is the particle size distribution which influences the stability and film forming characteristics of the latex. A significant percentage of latices produced commercially do not meet particle size specifications and must therefore be recycled or discarded as waste. This provides motivation for the development of a control strategy to reduce the number of off grade batches, and thus the incentive for this study. The purpose of this work was to develop a computer monitoring and control system for particle growth. This should enable some future investigator to study emulsion polymerization on line and in great depth, and develop appropriate control strategy.

The computer system was developed specifically for polyvinyl acetate latices. However, with minor modifications the system should be applicable to any emulsion polymerization. Polyvinyl acetate was chosen here as a great deal of technical information was available through the studies by Keung (1) and Goosney (2). In particular, Keung(1) showed, using tedious off line measurements, that the particle size development could be followed through measurements of

turbidity with a UV spectrophotometer. He showed that the weight average and number average particle diameters could be calculated from a measurement of absorbance at two wavelengths. This measurement makes an estimation of the mean and variance of the distribution, important parameters. The detector response at different wavelengths must be sensitive to these parameters; although, for control purposes, it is not necessary to specify particle size distribution, but the turbidity profile at fixed wavelengths could also be used.

In this study the minicomputer was able to considerably reduce the amount of work and time involved in measuring absorbance as a function of wavelength. The system could prepare a sample automatically every two minutes. This frequency was much greater than the manual monitoring which had a frequency of one sample every twenty minutes. The absorbance (equivalent to light scattering at 180°) provided a convenient and cheap method of measurement, which could be related to the particle size distribution.

2. THEORY OF EMULSION POLYMERIZATION

The classical theory of emulsion polymerization has been detailed elsewhere (1,3). This discussion is limited to the emulsion polymerization of vinyl acetate.

The reaction is carried out as a batch system. At the start of the reaction, the mixture consists of approximately 60 wt % water, 40 wt % vinyl acetate monomer, 1 wt % sodium lauryl sulphate and $\frac{1}{2}$ wt % potassium persulphate. The mixture is stirred vigorously to produce an emulsion which can be considered to consist of three phases. The first phase, water - the dispersion medium, contains potassium persulphate, the initiator, as a solute. A second phase is large monomer droplets, having a size of 1 to 10 microns, held stable by small amounts of emulsifier. The third phase consists of micelles. A micelle is a group of emulsifier molecules which have come together to form a small spherical aggregate of approximately 50 Å diameter. One end of the emulsifier molecule is hydrophilic and the other hydrophobic. The hydrophobic ends cluster together in the centre of the micelle. Monomer tends to diffuse from the water phase into the centre of the micelle, to form a monomer swollen micelle.

The number of micelles in the mixture is very large compared with the number of monomer droplets, providing an extremely large surface area for the capture of initiator

radicals. Thus most of the free radicals, formed in the aqueous phase via initiator decomposition, tend to enter micelles rather than monomer droplets. As soon as a radical enters a micelle the polymerization takes place rapidly within the micelle, because of the high monomer concentration. As the polymer particle grows, more monomer is absorbed from the monomer droplets which act as a reservoir. Also, as the particle grows, more emulsifier molecules adsorb causing unstung micelles to dissolve into the water phase. As the polymerization continues, we find at about 10 to 15% conversion that all the micelles have either become a polymer particle or dissolved into the water. This is considered as the end of the first stage of polymerization. At this point the total number of particles is fixed.

In the second stage polymer particles continue to grow and the monomer continues to diffuse out of the monomer droplets into the dispersion medium and then into the growing polymer particles. The end of the second stage is defined as when there is no monomer remaining as droplets. During this stage, monomer concentration in the polymer particles remains constant.

In the final stage of polymerization, there is no monomer left to diffuse into the particles, and the concentration of monomer drops in the polymer particle. In the final stages of polymerization it is possible for the polymer particles to coalesce. This will occur if the particles are small and there is insufficient emulsifier to stabilise them.

In summary, during stage one particles are nucleated and the total number of particles fixed. In stage two, particles grow but the total number is constant. Finally, in stage three there is a small shrinkage in particle size due to the density difference between monomer and polymer.

3. JUSTIFICATION FOR DIGITAL CONTROL

Digital control is essential due to the time limitation when control must be initiated and the complexity of calculations required. The first stage of polymerization occurs within the first 15 to 30 minutes of reaction. Measurements of particle size distribution and rate of growth must be made during this period and converted to the required control action, else the total number of particles is fixed. To control the variance of the distribution we must control in stage one.

Naturally, it is important that measurements be made as early as possible and the measurement is accurate. Most measurements of particle size distribution such as angular light scattering and electron microscope require extensive preparation of samples and the results may not be obtained until hours after the reaction is completed, a little late for process control. Measurement of the absorbance (light scattering at 180°) of the solution can be obtained very quickly using a UV spectrophotometer. However, in order to make such a measurement, a sample must be prepared quickly, accurately and consistently. This preparation involves diluting the latex solution with an accurate volume of diluent, and filling the light transmission cell with the prepared sample. This can not be done manually with

any degree of efficiency. Using the minicomputer, such a sample could be prepared every two minutes, or even more frequently.

4. DESCRIPTION OF THE HARDWARE

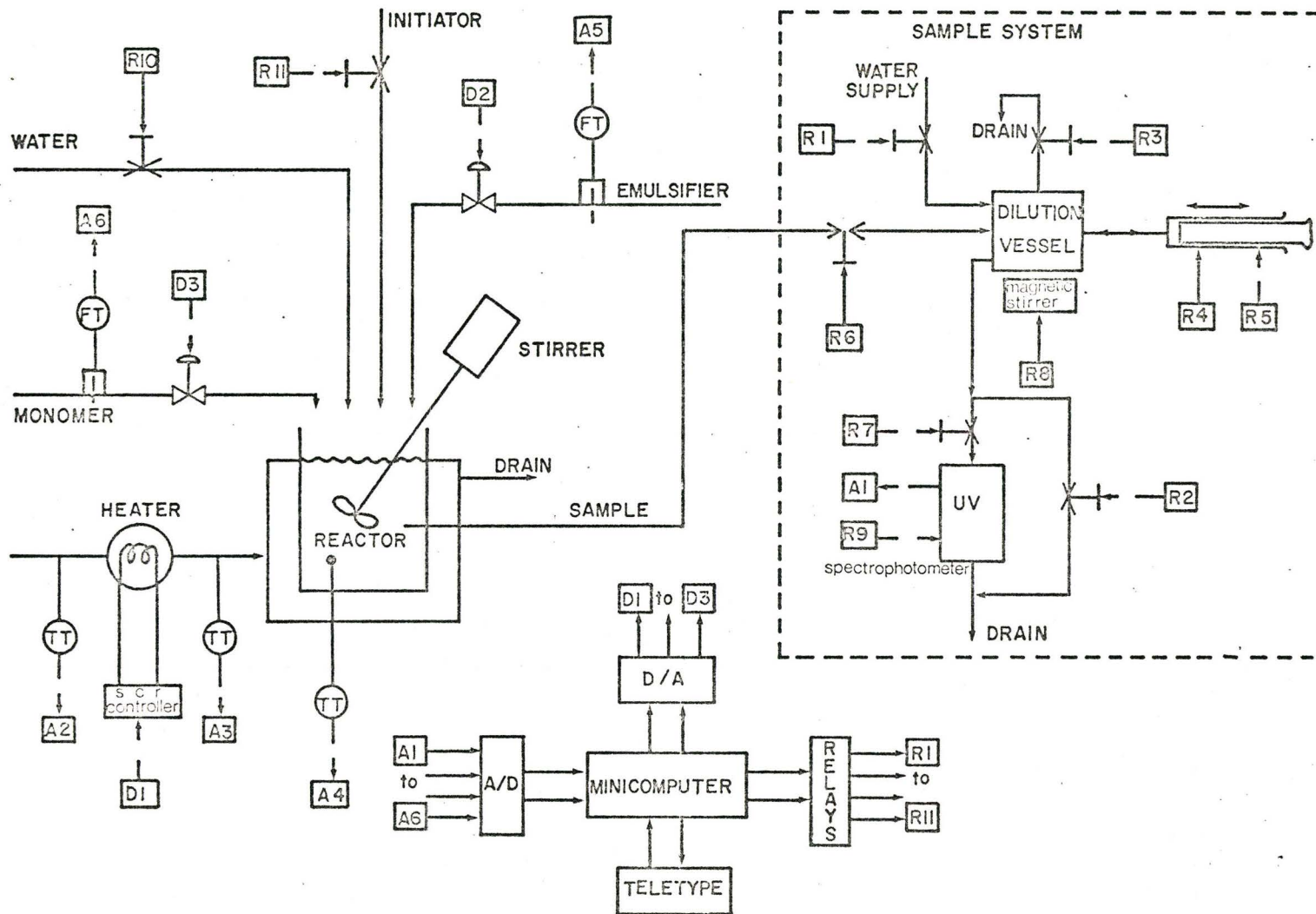
4.1 Process Equipment

Figure 1 is a schematic representation of the process equipment. The apparatus may be considered in four parts; the feed system, the temperature control system, the reaction system and the sampling system. They will be described in the above order.

The feed system consists of three vessels that hold the water-emulsifier mixture, the monomer, and the initiator solution. Each of these vessels is purged with nitrogen to eliminate oxygen. These mixtures are gravity fed to the reactor via three 1/8" stainless steel ASCO solenoid valves (120V, N.C.) which can be operated manually or by the computer. It is essential that the process streams do not contact brass or copper. The copper ions deactivate the catalyst.

Temperature is controlled in the reactor using a hot and cold water flow. The hot water is taken from the building supply and further heated using an electric heater to 70°C. The cold water, also from building supply runs at about 10°C. Water flow used in the experiments was about 2 litres/minute. The two water streams are controlled by means of 1/4" brass ASCO solenoid valves (120V, N.C.) which are interfaced to the computer (see section 4.2).

Fig.1 COMPUTER CONTROL OF A LATEX REACTOR



The reaction takes place in a 3 litre glass flask, surrounded by a water jacket through which the water heating/cooling passes. Inlets in the top of the vessel allow access by the feed streams, stirrer with speed control, thermometer, thermocouple, sample tube, nitrogen purge and a reflux condenser.

The sampling system is composed of a 250 ml earlenmeyer flask in which the concentrated latex from the reactor is diluted with distilled water. The vessel contents are mixed using a magnetic stirrer and then passed through a flow through light transmission cell where the absorbance is measured at different wavelengths using a UV spectrophotometer. All parts of the sampling system are interfaced to the mini-computer. Detailed operation of the sampling system can be found in section 5.4.

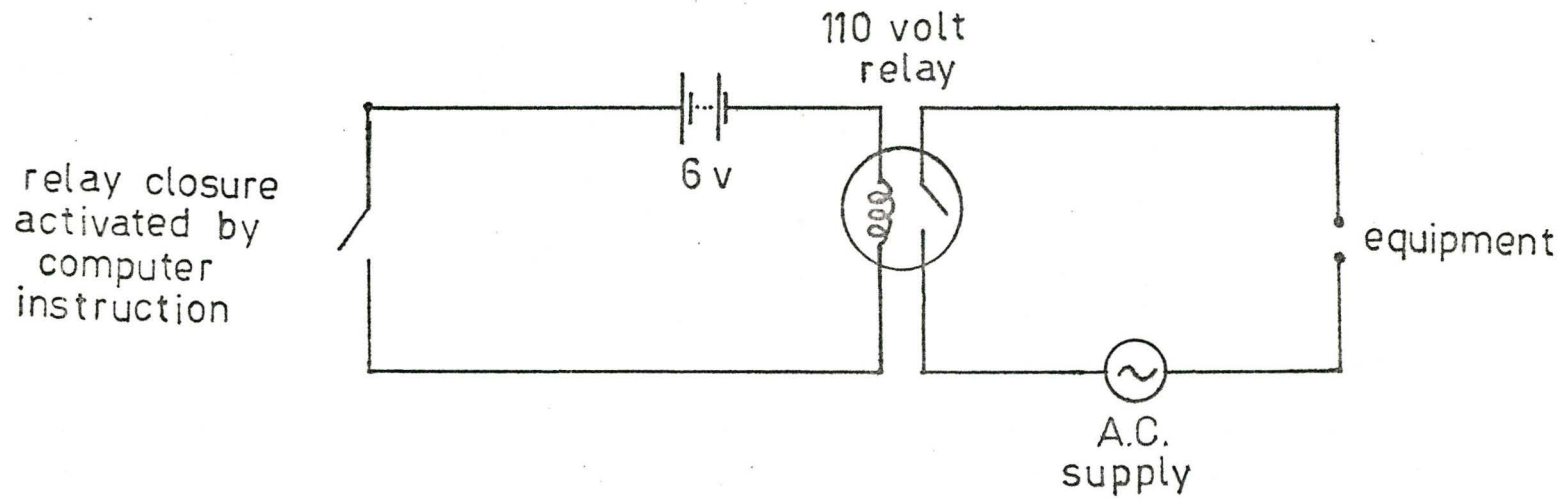
4.2 Control Computer and Process Interface

A dedicated minicomputer of the NOVA family (Data General manufacture) with 4K core was used to monitor and control the reaction. Each instruction and data storage location has a 16 bit word length. The machine has four accumulators, two of which can be used as index registers.

Peripherals included with this computer are a real time clock, power failure detector, teletypewriter, 16 A/D input channels and 16 relay outputs. The teletypewriter is used for loading the computer program via paper tape, operator communication with the system, and printing a log of the process conditions as the reaction progresses. Temperatures

within the reactor and jacket are measured using chromo-alumel thermocouples, then amplified with a temperature transmitter to provide a 0 to 10 volt input signal to the computer. The 16 relay outputs can only be used at low voltage (6V). When closed, they activate a second relay which closes the 110 volt supply circuit. When this secondary power supply is activated and the particular circuit is switched to computer control, the solenoid valve opens or the appropriate equipment is activated. Figure 2 describes this relay action. The real time clock allows the computer to keep track of physical time. A pulse is issued by the clock every one hundredth of a second, causing an interrupt to the CPU. The system then marks the passage of this time interval and can thus interface practically with the process.

Fig 2 RELAY INTERFACE TO PROCESS



5. DESCRIPTION OF THE SOFTWARE

In this section the method by which a digital computer can operate in a real time environment is described. After a basic overview of the computer handling in section 5.1, the actual system package developed for the latex reactor is described in section 5.2. The details of each routine are given in sections 5.3, 5.4 and 5.5. In section 5.6 a procedure for startup of the system is given.

5.1 Real Time Data Processing

The following will describe how the processing takes place in the particular system used in this study. Further detailed discussion may be found elsewhere (4).

In real time data processing it is always necessary for the computer to do two or more actions simultaneously. For example, it may be necessary to supply the operator an important message at the same time that a measurement of the temperature in a reactor is required. However, in a computer there is just one place where logical action can occur. This is the CPU (central processing unit). The CPU always works in the same manner. An instruction consisting of 16 bits is picked out of memory at an address indicated in the CPU. Depending on the configuration of these bits, the CPU performs a certain action. This action might consist of

obtaining a word from core and storing it in one of its four working registers (called accumulators) or perhaps to instruct the CPU that its next instruction is to be obtained from a certain storage location. The instruction set used for this type of programming is called assembly, where the instruction implicitly tells the CPU what to do. This is apart from the higher level languages such as fortran. However, all computers operate in a similar manner to that described above (with slight differences such as length of instruction word and number of working registers). These high level language programs must be converted to machine language. A program that makes this translation is called a compiler. The advantage in using assembly language is that very efficient use of core space is possible whereas a compiler, which has to be general in nature, must sacrifice this efficiency. On the other hand, high level programs allow for ease of programming.

A typical instruction for the CPU takes less than one microsecond to execute. To print a character, a teletype takes approximately one tenth of a second or 100,000 microseconds. If the CPU could not do any further processing until the teletype had finished printing, the CPU would be idle for 99.999% of this time period. In order to circumvent this problem, interface devices such as A/D converter or teletype can cause an interrupt of the currently executing instructions of the CPU. Now the instruction to print a letter on the teletype can be issued by the CPU and can then

carry on with other tasks, returning to service the teletype 100,000 instructions later.

In the configuration used in this system there are 6 devices with which the CPU can communicate. These are the A/D converter, D/A converter, relays, real time clock and teletype in and out. The actual instructions which service these devices are contained in RTOS (real time operating system), a program package supplied by Data General (5). The user programs communicate with RTOS by a series of pseudo-instructions, described in table 1. Using RTOS, it is no longer necessary for the user to worry about handling device interrupts or scheduling the running of tasks. This is all handled by RTOS in response to these pseudo-instructions.

TABLE 1: Communication with RTOS

Pseudo instruction	Meaning
.IOX	Input/Output to requested device
.RCV	Suspend this task until .XMIT allows this task to proceed
.XMIT	Allow suspended task to proceed
.XMIT@	Allow suspended task to proceed but do proceed with this task until message received.
.WAIT	Suspend this task for a given time interval
.FORK	Create a new task
.QUIT	This task has been completed, drop from system
.PTY	Set this task to priority specified (higher priority tasks are given execution preference by RTOS)

5.2 Configuration of the System

This computer system was created in order to provide ease of communication between the operator and the computer. The system is set up to receive a series of keywords via the teletype so that communication is almost conversational.

To begin operator interaction with the computer system, a CTRL A character is issued at the keyboard. The system is always waiting for this instruction. Upon issuance, the system terminates all output to the teletype, generates a line feed and carriage return and then awaits further instructions. These instructions consist of a word followed by a space. At present the allowable words are LOG, CHANGE, FROM, TO, READ, STOP, SCHEDULE, READOCT and START. The computer then carries out the appropriate software code related to the specific instruction. The code is called a "communication" routine, the details of which can be found in section 5.3.

Normally, upon reading the first word above, a second word is expected indicating either a data location within the system or a task which is to be executed. Possible data locations that the operator needs access are described in the particular task routines described in section 5.4. The tasks currently in the system are SAMPLE, INITIATOR, MONOMER, EMULSIFIER and CONTROLT, each described in detail in section 5.4. CONTROLT bears the meaning control temperature, the other tasks are self explanatory.

The software is rigged to allow easy expansion of the system to accept new tasks, data locations, and "dynamic" or communication words. Only two additional storage locations are required (see service routine INPUT) for the system to recognize a new word. Also, it is possible for different words to represent the same task or data location. For example it may be desirable to have both SAMPLE and SAMPLING refer to the same task so that the operator can issue the command START SAMPLING.

Another type of routine within the system is called the service routine. These routines are not directly accessed by the operator. Each service routine is used by more than one task to perform a particular function. They are necessary to conserve computer memory.

In summary, there are three types of routines within the system. The first type is the communication routine which allows the operator to control system execution. The second performs the tasks related to the physical system. The third type, the service routines are used by the tasks to perform a given function and conserve core space.

5.3 Communication Routines:

All operator interactions with the system are controlled by the system executive, INTER. This program initialises the system, and then continually waits for an indication that the operator wishes to communicate. The operator accomplishes this by issuing a CTRL A character from the teletype. Upon receiving this character, a

carriage return and line feed is issued to the teletype and CPU control is transferred to program INPUT. INTER then remains inactive until a CTRL A is again used. Program INPUT reads a name from the teletype. This name must be one of the communication routines described below. Control is then transferred to the appropriate routine.

CHANGE: This word is required whenever the operator wishes to alter the contents of a data location. The routine requests INPUT to read the name of a data location. If the word is acceptable, control is then transferred to INPUT to obtain the next communications word, usually FROM or TO.

FROM: This word, usually used after a CHANGE command, reads the current value of the specified data location. RTBDØ (a service routine described in section 5.5) is then called to print the value on the teletype in base 10 notation.

TO: The final word required in altering a data location. RTDBØ is used to read the new value. The routine then stores that value in the data location specified after the CHANGE word. A carriage return and line feed is then issued to the teletype. The system is then ready to accept further input.

READ: This word is typed when the contents of a data location are desired. Upon reading this word, INPUT is called to receive the name of the data location. The current value is then printed on the teletype in base 10 using the service routine RTBDØ. After printing, control is not passed to INTER but remains with READ. Further data locations can be read by merely typing their name. To access other communi-

cation routines, a CTRL A must be issued.

READOCT: This routine is similar to READ routine with the exception that the contents of the data location are printed in octal (base 8).

STOP: If the operator wishes to terminate a currently executing task, he can type STOP and then the name of the task. There is no effect if the task named is already dormant.

START: Use this word to begin execution of one of the system tasks. INPUT is used to obtain the name of the task. The command has no effect on the system if an attempt to start a task that is already executing.

SCHEDULE: If a task is needed at some future time, but not immediately, then the SCHEDULE command is used. Following this word, the operator should enter the name of the task. The system then responds with "TO START AT", and the operator should then enter the time in minutes and seconds relative to the start of reaction. The system response is "TO STOP AT" and the operator enters the time when the task should be stopped. The system then converts the two input times to seconds and stores these values in PINIT (a service routine for program initiation).

5.4 Task Routines

Each of the task routines can be started or stopped by the operator either directly or through program SCHEDULE. There are presently six tasks in the system SAMPLE, EMULSIFIER, MONOMER, INITIATOR, CONTROLT and LOG. They are each described

in detail below.

SAMPLE:

The function of this routine is to take an accurate volume of sample from the reactor, dilute with distilled water, mix to a uniform solution of known dilution, transfer the solution to the UV analyser, and start the UV analyser routine.

It performs this task by setting ten computer relays to either the closed (bit set to 1) or the open (bit set to 0) position. These low voltage relay circuits in turn activate 110 volt relay circuits which activate the solenoid valves and automatic syringe of the physical sampling system. The relationship between the computer relays and the physical sampling system is given in table 2.

Before taking the next sample, the task checks that the time necessary for taking a sample (120 seconds) does not exceed the allotted time interval set by the operator SMPLINT. Another check is made on the other operator input SMPLVOL, the volume of sample to be taken. The program ensures that the volume does not exceed the maximum volume of the syringe. If either of these values is out of range, the routine does not take a sample during this interval. No further checks are necessary at this point since altering the sample volume or interval does not affect the routine until the next sample is taken.

Upon completing the above checks the routine begins opening and closing relays in a set time sequence, at the end of which the routine is ready to take another sample. An

Table 2: Relays used in SAMPLE routine

Relay No.	Physical action when relay closed
1	Solenoid valve connecting dilution vessel to gravity feed tank is opened.
2	Valve connecting dilution vessel to drain is opened.
3	Air bleed valve atop the dilution vessel is opened.
4	Power connected to automatic syringe.
5	With power to syringe, the syringe infuses (when not set syringe withdraws).
6	Valve between reactor and dilution vessel opens.
7	Valve between dilution vessel and UV analyzer cell opens.
8	The stirrer is started.
9	Connects the reactor sample line to vacuum.
10	Valve to reactor is opened.

internal subroutine RESET is used to call the relay routine and wait the desired time interval. Below is a list of each of the relay configurations used by this routine in the sequence in which they are called.

Relay configuration 1: 0007 Time: PURGE: 3 secs

Action: The reaction mixture is opened to vacuum in order to purge the sample line with the current reacting mixture. In the present set up 3 seconds was found to be adequate.

However, if the length of sample line or amount of vacuum is altered, this interval should be changed. If PURGE should be changed, MINTM (the minimum time to complete a sample) should have a corresponding adjustment.

Relay configuration 2: 0125 Time: DRAW: 20 secs.

Action: A known volume of sample is withdrawn from the reactor into the dilution vessel. The current reaction time is saved for later use by UVANS in SSEC.

Relay configuration 3: 0004 Time: STINT: 5 secs.

Action: The stirrer only is activated during this time interval. At the end of this interval, the sample is ready for measurement by UVANS. A message is sent to UVANS to indicate that a sample has been prepared and is about to be transferred.

Relay configuration 4: 0310 Time: UVINT: 25 secs.

Action: The air bleed valve and valve to UV analyzer cell are opened. The prepared solution flows by gravity through the UV cell to drain. An interval of 25 secs was found necessary to completely purge the line and cell of the previous sample.

Relay configuration 5: 0610 Time: UVINT: 25 secs

Action: The main drain valve of the dilution vessel is also opened to reduce time required to empty.

Relay configuration 6: 0600 Time: EMINT: 15 secs

Action: Valve to UV spectrophotometer is closed to ensure no air gets into the UV cell. These 15 secs are used to complete emptying of the dilution vessel of all polymer sample.

Relay configuration 7: 1400 Time: FSHTM: 10 secs

Action: The dilution vessel is flushed with distilled water from the gravity feed tank.

Relay configuration 8: 1340 Time: DRAW: 20 secs

Action: The dilution vessel is filled with water and the syringe emptied. The air bleed is open to allow filling. This interval is the same as the syringe withdrawal time so that the syringe is in the correct position to take the next sample.

Relay configuration 9: 1200 Time: FILLR-DRAW: 15 secs

Action: Until the dilution vessel is completely filled, water from the gravity feed tank is allowed into the vessel.

Relay configuration 10: 1022 Time: SLFSH: 10 secs

Action: In order to ensure consistent readings from sample to sample, the sample line is backflushed as far as the vacuum system.

Relay configuration 11: 0000 Time: SMPLINT-MINTM

Action: All valves are closed and program remains dormant until next sample.

EMULSIFIER, MONOMER, INITIATOR:

These three routines have been grouped together since their functions and coding are similar. They are routines for controlling the rate of addition of each to the reactor. A relay is set by each routine to open a solenoid valve and allow the respective feed to flow by gravity into the reactor. A controlled "rate" of addition is accomplished by allowing the particular solenoid valve to be open for only a portion of each second that passes. Thus an approximation of constant flowrate is obtained.

The rates of addition to the reactor can be adjusted by the CHANGE variable command. The names for the flowrates of emulsifier, monomer and initiator are respectively FLOWE, FLOWM and FLOWI. It should be noted that these are the flowrates that will occur when the respective tasks are started either by the START or SCHEDULE commands.

CONTROLT :

This routine controls the temperature of the reacting mixture. The task is started by typing START (or SCHEDULE) CONTROLT at the teletype. This starts the routine that records and stores the reactor and jacket temperatures. However no control actually occurs unless TYPECONTROL is set to 1.

With TYPECONTROL set to 1, on-off control is initiated. That is the two solenoid valves controlling the hot and cold water supplies to the reactor jacket are opened as necessary. At present the interval for control is set at 1 second, however this can be altered by the variable TEMPCINT (tempera-

ture control interval), the control interval in units of seconds.

LOG:

This is the logging routine which outputs on the teletype printer pertinent data as the reaction progresses. It is the one task which does not require the START command. When command input has been completed simply type LOG<space> and the routine starts printing the data at the current logging interval LOGINT (units are in seconds). The routine stops printing whenever a CTRL A is entered on the teletype.

5.5 SERVICE ROUTINES:

There are seven service routines presently included in the system. They are RTDBØ, RTBDØ, MATHS, INFCE, CLOCK, PINIT and INPUT. The function of these programs is to provide a service which can be accessed by communication routines, task routines or by other service routines. Each will be described in detail below.

RTDBØ: This routine is called when a number is to be input via the teletype by the operator. The routines name is derived from its function, real time decimal to binary conversion. The program reads a decimal number of up to 5 digits plus sign from the teletype, converts these digits to a single binary word and then returns to the calling program with the result in accumulator 1.

Upon entering this routine, the character "#" is printed on the teletype. This is to indicate to the operator

that this routine has been entered and a decimal number of up to 5 digits is expected. The routine will accept as input "+", "-", space, or a digit 0 through 9. Any other character or symbol (other than CTRL A) causes the routine to terminate input. Transfer is made to the beginning of the routine, clearing all registers and printing "#" once more. This allows the operator to reenter a number whenever a typing error occurs. Typing CTRL A causes all current execution of I/O to be terminated and control transferred to INTER. A space indicates the end of the number and is the normal termination of this routine. The calculation of the binary number is completed and return is made to the calling program with the result in AC1.

RTBDØ: This is the reverse of the previous program. The routine's service is to take a binary number transmitted via ACØ, convert the number to base 10 and print the result on the teletype. AC1 should contain the necessary printing information. For the purpose of this program, AC1 is considered to consist of two 8 bit integers. The first 8 bits contain the position of the decimal point in the number to be printed. The value is equal to the number of digits after the decimal point. No decimal point is printed if the first 8 bits are all zero. The remaining 8 bits indicate the number of characters to be printed. This number is exclusive of the decimal point or the space which is always printed at the end of a number. If the value is negative, then the word in ACØ is printed in octal, no decimal point is used, and 6 digits are always printed. If the value is zero then the word in ACØ is printed in decimal

but only the minimum number of characters necessary to complete the number are used. This option is especially useful when the number of digits is not known and a special format is not desired such as in the READ and CHANGE commands.

MATHS: This service routine is actually a collection of all the math routines required by the system. The routines are all re-entrant which means that more than one task can access the routines at the same time without affecting the result. A re-entrant task stores all working numbers either in the calling program or accumulators. Each routine is described separately below.

BIDEC: This routine converts the binary number supplied through AC0 to ascii code. The ascii code is stored in the first 6 locations following the call statement. The seventh location following the call is used by BIDEC as a temporary storage register. The first location contains the sign of the converted number; ascii "-" for negative numbers and ascii "0" for positive numbers. The call sequence for BIDEC would then appear in the calling program as:

```
JSR @ <location of address of BIDEC>
.BLK 7
<Return>
```

MULTY: This is a simple single precision multiply routine. AC0 is multiplied by AC1 and the result returned in AC0 and AC1. The high order part of the result is in AC0 and the low order in AC1.

DIVID: This is the single precision divide routine. Upon calling this routine AC0 and AC1 should contain the numerator

and AC2 the denominator. The result of the division is returned in AC1.

INFCE: This program is a collection of routines which handle input/output to the various devices. Each of these routines acts independently of the others.

RELYS: Output to the relays is controlled by this routine. The routine maintains a record of the current bit pattern of the relays and outputs the new pattern whenever called from the other tasks. The call sequence is:

```
.FORK
1
RELYS
```

AC0 should contain the new relay configuration. Each bit represents a relay channel. The respective bit is set to 1 to close the relay and 0 to open. AC1 should contain the relays that should not be changed at this time. For example, if the contents of AC0 are 051000 and AC1 are 100777, then relays 2, 4 and 7 will be closed and 3, 5 and 6 will be opened. The contact positions of relays 1 and 8 through 16 will remain as they were.

TT00: This routine outputs a string of characters in byte format (two ascii characters per word) to the teletype. The last byte of the string is a null character (000). The call sequence is:

```
JSR TT00
<address of byte pointer>
<Return>
```

The byte pointer contains a numerical value equal to twice the address location of the first byte in the character string.

TRANS: At the present TRANS reads all 16 of the A/D input

channels continuously whenever the CPU is not busy with other parts of the system. It runs at the lowest priority. Note, that when the system is expanded to include long and time consuming calculations, it will be necessary to split CPU time between these and TRANS. It will be necessary to increase the priority of TRANS and create CPU time for the long calculations by use of the .WAIT command.

TRANS contains a coarse type of digital filter used on A/D channels 0 and 1. A continuous average of the last 37 readings from these two channels is maintained. In the present system this was found to be an acceptable method of measuring temperature. However, as the CPU becomes overloaded, a more sophisticated filter can be written. There is no evidence of time delay using this method of measurement. CONTROLT uses the measurements once every second in controlling the reactor temperatures and, during this time period, many averages are computed.

CLOCK: This routine keeps track of the real time. The time of day can be accessed by the operator using the CHANGE and READ commands and the words HOUR, MINUTE and SECOND. CLOCK also maintains a record of the time relative to the start of reaction. This can be accessed by REACTIME from the teletype. From within the system, routines can access these values by reading the locations of HOUR, MINIT, SECND and RTIME. CLOCK uses the .WAIT command to determine the passage of one second, then increments SECND and RTIME. When SECND and MINIT reach a value of 60, MINIT and HOUR respectively are incremented. Time is based on a 12 hour clock, thus HOUR is set to 1 when-

ever 13 is reached.

PINIT: This section coordinates the execution of tasks as set by the SCHEDULE command. With the passage of each second, a "pulse" is received from the CLOCK routine. PINIT then checks its stack of programs to determine if any should be started or stopped at this time. The stack of programs, ITEMS, is a list of starting locations of tasks with the times when they should be started and stopped. Three locations are used for each SCHEDULE command. At present there is room for 7 programs. This can be increased by merely lengthening the ITEM table.

INPUT: Routine INPUT reads a word from the teletype. The word is terminated by a space. Each character, as entered, is coded by taking the 7 bit ascii configuration and adding to the previously calculated code and shifting the result one bit to the left. The code formed in this manner, upon being terminated with a space, is compared with a table of codes. If the code is found in the table, INPUT returns to the calling program with the core address, associated with the code, in accumulator 1. If the code of the input word is not found in the table, then INPUT causes the error message NO to be printed and control is passed to the program executive, INTER.

INPUT can be entered at three separate locations, INPTT, INPTP and INPTD. Entry to the program at these addresses causes a different table of acceptable codes to be used. INPTT is called when the address of a task routine is required; only task names will be found in the table searched

by INPUT. INPTP is used when one of the system programs or communications routines are desired, and INPTD for the address of a data location. As an example of how INPUT is used, consider the command line

```
READ TEMPSP
```

After issuing CTROL A, the executive is called into action, terminating the log routine and entering INPUT at INPTP. INPUT then reads the character string READ<space>. Upon encountering the space character, INPUT completes the code which for this word is 2152. The code is compared with the items in the code table for communication routines. In this case the code is found, so INPUT loads the address corresponding to the READ communication routine into accumulator 1. Control of the CPU is transferred back to INTER which then calls the READ routine at the address supplied by INPUT. READ routine now needs the address of a data location, so INPUT is again called but this time at INPTD. TEMPSP<space> is then read from the teletype. The resultant code, 11556, is compared with the table of data locations. The code is found, so INPUT loads the address corresponding to the input word and returns it via AC1 to the READ routine.

The routine was written in the above manner for two reasons. Firstly separate tables were used so that when a data location is required, the address of a routine cannot be obtained. Similarly the system will not start executing a string of data. Secondly input words are not limited by length so that names can closely approximate real words. Thus operator communication with the system is easy to follow.

5.6 STARTUP AND RUN PROCEDURE

This procedure is limited to the startup and running of the computer system. Procedure relating to the reaction itself may be found elsewhere (Keung(1)).

- (i) Charge the monomer, emulsifier and initiator to the respective feed tanks.
- (ii) Load the computer program into core.
- (iii) Set the current time and time until the reaction is to start using the CHANGE command.
- (iv) Set the time when the computer should feed the reactor with monomer, emulsifier and initiator using the SCHEDULE command.
- (v) Set the reaction temperature using CHANGE TEMPSP and start the temperature control routine with START CONTROLT
- (vi) Schedule the sample routine and set desired sample volume (SAMPLE VOL) and sample interval (SAMPLINT).
- (vii) Start the logging routine.

6. EXPERIMENTAL RESULTS AND DISCUSSION

6.1 TEMPERATURE CONTROL

A simple on-off control scheme on hot and cold water supply was used to control the reactor temperature with the computer. This type of control was sufficiently accurate for these experiments. The reactor temperature was held within $\frac{1}{4}^{\circ}\text{C}$ of the desired set point at all times.

6.2 INDUCTION PERIOD

An important problem encountered in industrial reactors for vinyl acetate polymerization is determining the start of reaction. Depending on the amount of oxygen and other impurities present in the feed materials, there is a certain length of time, called the induction period, in which no reaction takes place. This induction time can be anywhere from 0 to 60 minutes.

In this study the induction period was determined accurately by monitoring the absorption near the start of the reaction. This is demonstrated in table 3. Three readings prior and two readings following the start of reaction are given. The time interval between measurement is 5 minutes. The absorbance values are those obtained from the UV analyser, corrected for baseline and multiplied by 1000. A significant increase in absorbance can be seen at the start of the reaction.

Experiments 6 through 8 were not included in table 3. In experiment 6 no reaction occurred after 2 hours; at which

time the experiment was aborted. The absorbance remained constant throughout the experiment. This lack of reaction occurred when the reactants were fed via the feed tanks rather than being added manually. Brass solenoid valves were used. The copper in the brass probably interfered with the initiator making it inactive. This has been reported by other investigators (6). After this experiment, stainless steel solenoid valves were ordered but did not arrive before the conclusion of this study. Experiments 7 and 8 were not included in the table since there was no detectable induction period. This was attributed to the improved procedure of removing trace amounts of oxygen from the supply nitrogen by bubbling the gas through a 5% pyrogallol solution in 2N sodium hydroxide.

TABLE 3: Corrected Absorbance Readings at the Start of Reaction (Wavelength = 3000 Å)

Experiment No.	Ax1000 Sample 1	Ax1000 Sample 2	Ax1000 Sample 3	Start of Reaction	Ax1000 Sample 4	Ax1000 Sample 5
1	0	0	0			8
2	0	-1	0		4	13
3	0	0	2		13	28
4	0	2	3		--	291
5	0	0	0		11	70

6.3 PARTICLE SIZE DISTRIBUTION

The Mie theory presents a method by which the number of polymer particles and the particle size distribution can be determined from measurements of absorbance. The Mie theory predicts that for a monodispersed spherical suspension

$$\tau^* = K^* \pi r^2 N \quad (1)$$

where τ^* is the turbidity of a dispersion defined by

$$\tau^* = 1/\ell \ln(I_0/I) \quad (2)$$

r is the radius of the particle (cm)

K^* is the light scattering coefficient

N is the number of particles (#/cc)

ℓ is the path length of transmission cell (cm)

I_0, I are the incident and transmitted intensities.

Since the absorbance, A , is defined as

$$A = \log_{10}(I_0/I) \quad (3)$$

and the length of transmission cell in this study was 1.000 cm

$$\tau = 2.303 A. \quad (4)$$

For a polydispersed spherical suspension the turbidity, τ can be determined by the summation of the individual effects of each particle, that is

$$\tau = N \int_0^{\infty} K^* \pi r^2 f(r) dr \quad (5)$$

where $f(r)dr$ is the number frequency of particles in the size range r to $r + dr$.

If an analytical form for the particles size distribution is now assumed, then by measurement of turbidities at several wavelengths, the particle size distribution, the

number of particles and thus the concentration of particles can be calculated. This is explained in Appendix A.

The β and generalised exponential distributions were compared using a minimum sum of squares deviation as a criteria of fit. The particle size distributions measured by Keung(1) were used as the basis for comparison. The β distribution was found to give a closer approximation to the electron microscope data. Table 4 shows the calculated values of \bar{d}_n and \bar{d}_w compared with the electron microscope values. Note that the weight average particle diameter compares favourably with the electron microscope data in most cases and has the same order of error as the light scattering data, also from Keung(1).

TABLE 4: Comparison of Number and Weight Average Particle Diameters using the β -Distribution

Expt #	\bar{d}_n (E.M.) (Å)	\bar{d}_n (τ) (Å)	\bar{d}_w (E.M.) (Å)	\bar{d}_w (τ) (Å)	% Dev. \bar{d}_n	% Dev. \bar{d}_w	% Dev. (E.M./L.S.)
A1	1090	1280	1650	1604	+17	-3	-5
A2	685	1050	1230	1380	+53	+12	-9
A3	420	770	770				-9
A4	520	874	910	1320	+68	+35	+21
A5	840	1056	1360	1390	+25	+2	+5
A6	490	722	850	1084	+47	+27	+10
A7	650	920	1160	1262	+41	+9	+7

However, the number average particle diameters are higher than electron microscope data by approximately 50%. This greater error in the number average particle diameter is to be expected. When the particle size is very small compared with the wavelength of light, only the weight average particle diameter can be measured as explained below.

A problem arises in the ability to calculate the particle size distribution when the particles are very small, or when a large portion of the distribution are small particles. This can be demonstrated by considering the scattering coefficient, K^* . For very small particles this coefficient approaches that for Rayleigh scattering

$$K^* = k \frac{r^4}{\lambda^4} \quad (6)$$

where k is a constant dependent only on the dispersion media and independent of the wavelength or particle size.

Since

$$\tau = N \int_0^{\infty} K^* \pi r^2 f(r) dr \quad (5)$$

Then for Rayleigh particles

$$\frac{\tau \lambda^4}{N} = k \int_0^{\infty} r^6 f(r) dr \quad (7)$$

or in terms of concentration

$$\frac{\tau \lambda^4}{C} = \frac{k \int_0^{\infty} r^6 f(r) dr}{\rho \frac{4}{3} \pi \int_0^{\infty} r^3 f(r) dr} = \frac{3k}{4\pi\rho} \overline{rw} \quad (8)$$

The right hand sides of equations (7) and (8) are

constant, independent of the wavelength and distribution function ($f(r)$). Only one moment of the distribution can be calculated, commonly termed the turbidity average particle diameter. This value is the same as the weight average particle diameter used in this study.

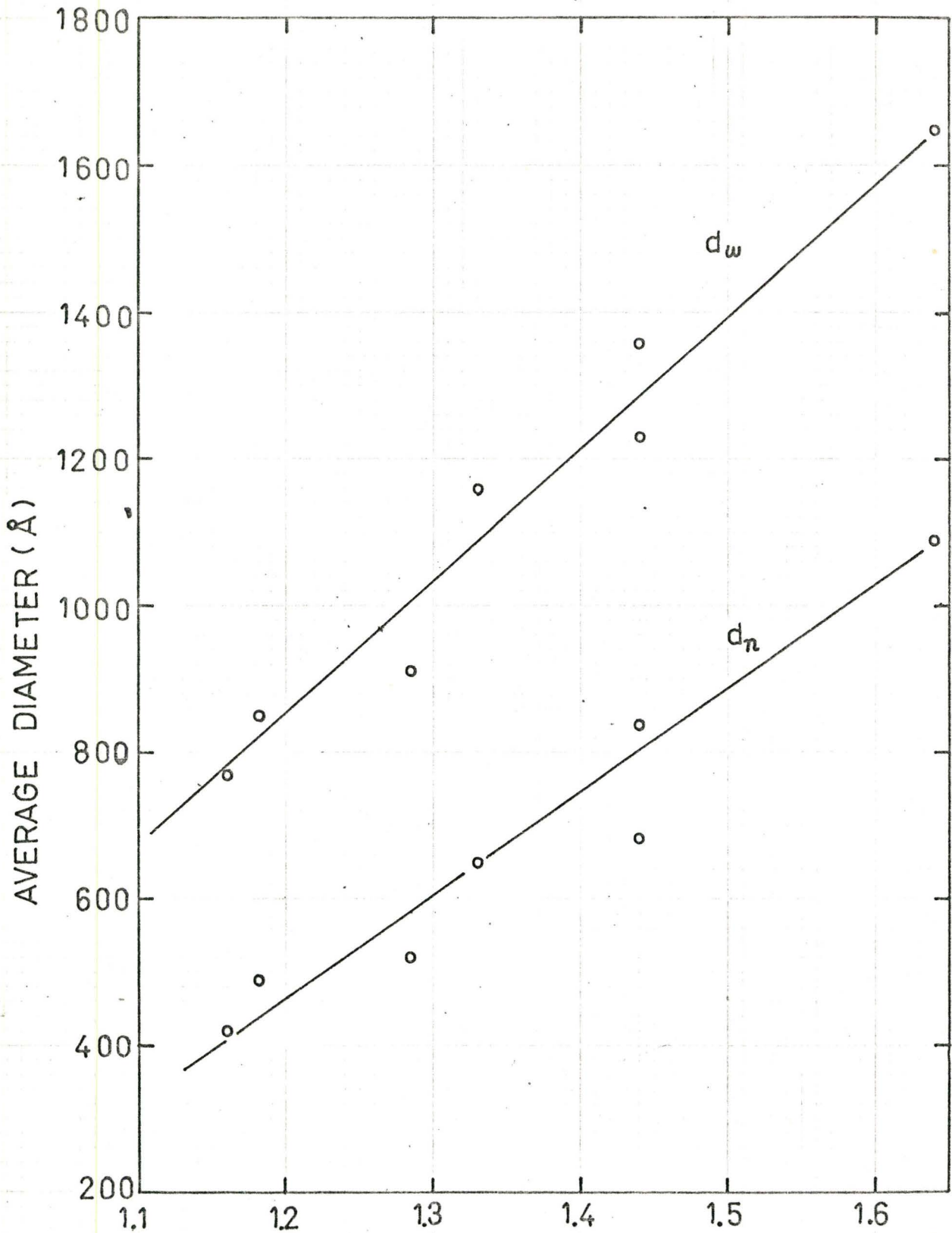
In order to further examine the results of the experiment, the B function was defined. B is the turbidity ratio

$$B = \frac{\tau_2 \lambda_2^4}{\tau_1 \lambda_1^4} \quad (9)$$

The turbidity ratio has several rather important qualities. Firstly it is independent of both the concentration of sample and the number of particles within the sample. It is a function only of the particle size distribution. Secondly, for a similar distribution, average particle diameters can be correlated with the turbidity ratio. This is demonstrated with the data from Keung(1) where the turbidity ratio with $\lambda_1 = 4000 \text{ \AA}$ and $\lambda_2 = 5890 \text{ \AA}$ is correlated with the average particle diameters measured by electron microscopy. Figure 3 defines this relationship for the various particle size distributions used in this study and by Keung. The third important quality of the B function is that several qualitative conclusions can be made about the numerical value of the turbidity ratio. The lower limit of B is 1.0, this is the value of B when there are only very small particles in the distribution. That is, when the particles are in the Rayleigh scattering region and the term $\tau \lambda^4$ does not vary with wavelength.

Fig. 3

AVERAGE PARTICLE SIZE versus B



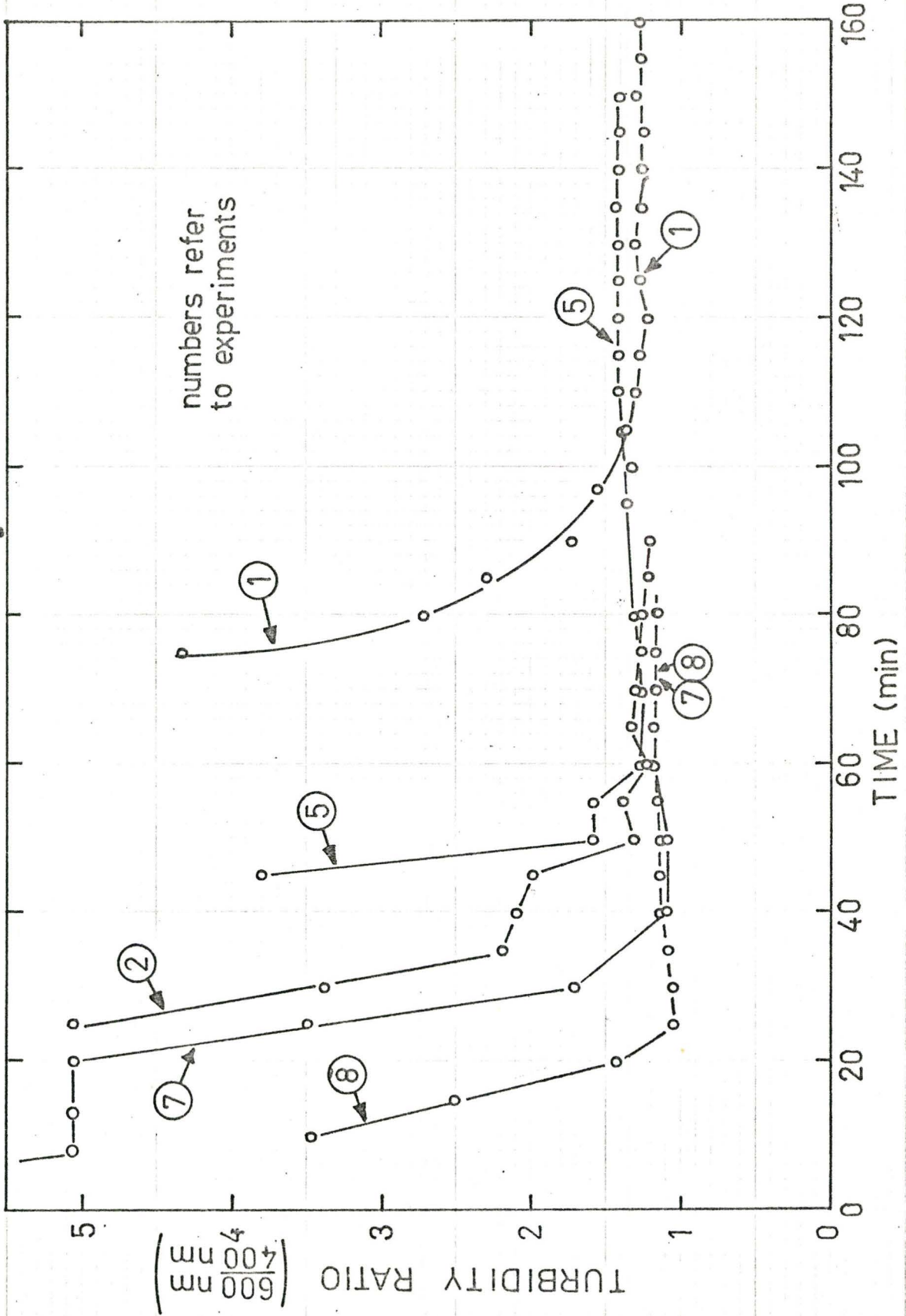
$$B = \frac{\tau(5890)}{\tau(400)} \times \left(\frac{5.89}{4}\right)^4$$

Narrow particle size distributions cause lower values for B. It can be shown that for the β distribution, developed in Appendix A, as the distribution becomes wider (p,q parameters are smaller) the function B becomes larger.

Figure 4 shows the B values obtained in this study for $\lambda_2 = 6000 \text{ \AA}$ and $\lambda_1 = 4000 \text{ \AA}$. Note that near the start of the reaction the turbidity ratio is high. The probable reason is that early in the reaction a wide distribution of particles is obtained. As soon as a polymer particle is formed, it grows very rapidly but new particles continue to form resulting in the wide distribution. At the end of stage 1, however, new particles are no longer formed. The distribution becomes narrower as the smaller particles grow more rapidly because of their large surface area. The B value decreases until the particle size distribution becomes established, near the end of stage 2 polymerization. The particles then continue to grow and B increases correspondingly. At this point particle diameters can be correlated with the turbidity ratio as indicated in figure 3.

Figures 5 and 6 show how the turbidity ratio using wavelengths of 3000 \AA and 4000 \AA varies throughout the reaction. The increase of B with the growth of the particles is clearly demonstrated. Note that using these higher frequency light waves, the turbidity ratio appears more dependent on the average particle diameter than the shape of the particle size distribution.

Fig. 4 TURBIDITY RATIOS



numbers refer to experiments

Fig. 5

TURBIDITY RATIOS, EXPTS 1-5

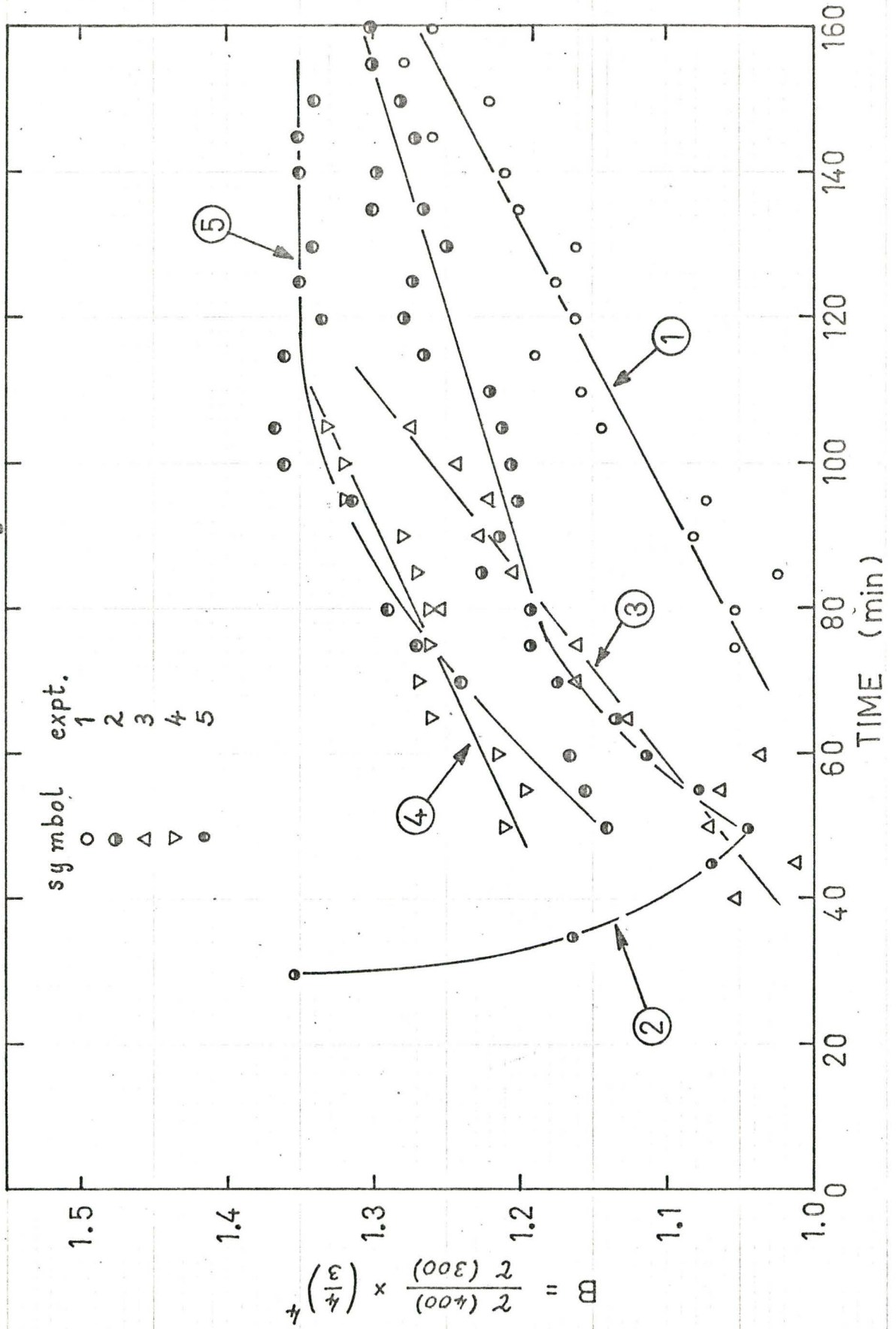
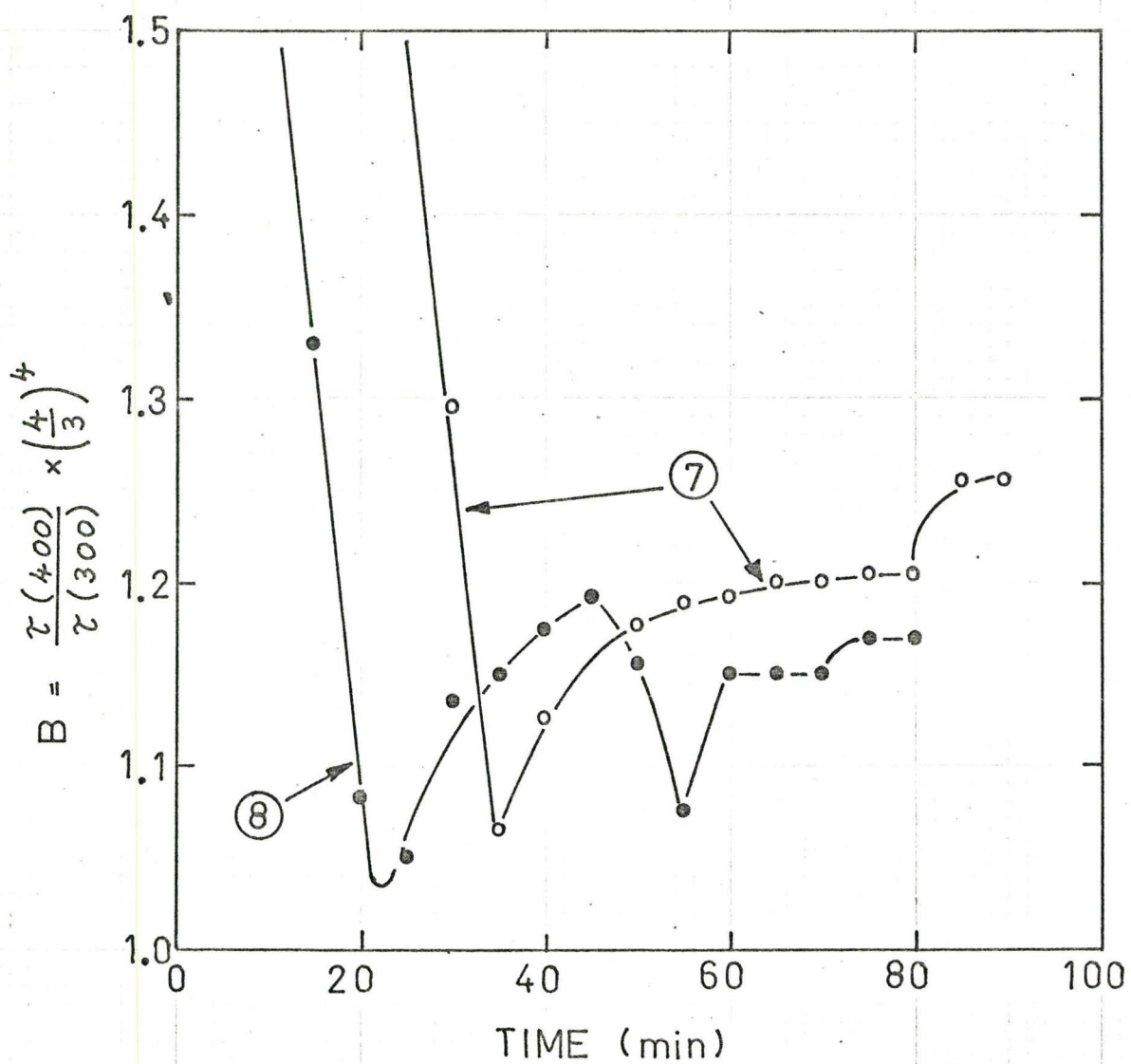


Fig. 6 TURBIDITY RATIOS, EXPTS 7, 8



7. CONCLUSIONS AND RECOMMENDATIONS

A hardware and software system was developed for on-line measurement of the turbidity of a latex in growth. The interaction between the user and the software was simplified so that an engineer with minimal experience can use the system. The software system is modular in that additional routines can be built into the system with a minimum of effort. The computer controlled sampling system allows fast and accurate preparation of samples for measurement by the U.V. spectrophotometer. It is recommended that the U.V. spectrophotometer now be interfaced with the minicomputer so that full use of this sampling system can be made. The computer can prepare a sample every two minutes but manual measurement of the sample takes over four minutes so that, for this study, samples were taken at five minute intervals. A computer controlled spectrophotometer would reduce overall sample analysis to less than two minutes and would eliminate lost samples due to operator error, which sometimes occurred during a run. This computer system can now be used to assist in the development of a control strategy for the latex reactor.

A preliminary study was made to develop techniques to convert turbidity spectra into particle size distributions. The results show that there is a definite correlation between the turbidity and the size distribution. It was found that

the β distribution gave a reasonably precise description of the particle size distribution. The parameters of the β distribution show sensitive variation with conversion. A B function was defined which is sensitive during the early stages of the polymerization and is probably related to the nucleation phenomena.

To control the latex reactor it is not necessary to follow the exact particle size distribution. A possible approach to the problem of control is to correlate the turbidity spectrum with the desired end product properties. In other words, the turbidity spectrum can give a measurement of the particle size distribution and the particle size distribution determines the properties of the latex. However, the calculation of the particle size distribution can be bypassed. If the effects of the various variables of the reaction on the turbidity spectrum are determined, then to control the reaction simply follow a predetermined turbidity curve, or properties of the turbidity curve such as the turbidity ratio at certain wavelengths.

8. NOMENCLATURE

A	Absorbance
A*	Equivalent absorbance
A/D	Analog to digital
B	turbidity ratio
CPU	Central processing unit
D/A	Digital to Analog
K*	Light scattering coefficient
N	Number of particles per unit volume
RTOS	Real time operating system
Å	Angstrom
dn	Number average particle diameter
dw	weight average particle diameter
l	path length transmission cell
p	parameter of β distribution
q	parameter of β distribution
r	particle radius
r _n	number average particle radius
r _w	weight average particle radius
λ	wavelength of light
ρ	density of polymer
τ^*	turbidity

9. REFERENCES

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APPENDIX A PARTICLE SIZE DISTRIBUTION FROM LIGHT TRANSMISSION MEASUREMENTS

As discussed in section 6.3 the turbidity can be calculated from the expression

$$\tau = N \int_0^{\infty} K^* \pi r^2 f(r) dr \quad (5)$$

K^* is a complicated function of the ratio r/λ but can be approximated with a high degree of accuracy (when $r/\lambda < 1.4$) by the expression

$$\pi r^2 K^* = 55.818 \frac{r^4}{\lambda^4} - 650.72 \frac{r^8}{\lambda^8} + 1860.8 \frac{r^{10}}{\lambda^{10}} \quad (10)$$

If a function is now chosen to represent the particle size distribution, then the distribution and number of particles can be determined by solving n simultaneous equations; where n is one greater than the number of parameters in the chosen distribution. This is demonstrated in the remainder of this section with the β distribution.

For the β distribution, the particle size distribution is represented by

$$f(r) = \frac{1}{\beta(p,q)} r^{p-1} (1+r)^{-(p+q)} \quad (11)$$

where p and q are the parameters of the distribution and r is the particle radius. Upon substitution of this distribution

into equation (5) the following expression is obtained

$$\tau = \frac{N}{\beta(p,q)} \int_0^{\infty} K^* \pi r^2 r^{p-1} (1+r)^{-(p+q)} dr \quad (12)$$

Substitution of $K^* \pi r^2$ with equation 10 and integrating the result is the following expression.

$$\tau = \frac{N}{\beta(p,q)} \left[\frac{55.818}{\lambda^4} \beta(p+6, q-6) - \frac{650.72}{\lambda^6} \beta(p+8, q-8) + \frac{1860.8}{\lambda^8} \beta(p+10, q-10) \right] \quad (13)$$

Using the relationship between the β and Γ functions

$$\beta(p,q) = \frac{\Gamma(p)\Gamma(q)}{\Gamma(p+q)} \quad (14)$$

and rearranging 13, the following is obtained.

$$\begin{aligned} \frac{\tau \lambda^4}{N} &= 55.818 \frac{\Gamma(p+6)\Gamma(q-6)}{\Gamma(p)\Gamma(q)} - \frac{650.72}{\lambda^2} \frac{\Gamma(p+8)\Gamma(q-8)}{\Gamma(p)\Gamma(q)} \\ &+ \frac{1860.8}{\lambda^4} \frac{\Gamma(p+10)\Gamma(q-10)}{\Gamma(p)\Gamma(q)} \end{aligned} \quad (15)$$

This equation can be further simplified by making use of the relationship

$$\Gamma(n) = (n-1)\Gamma(n-1) \quad (16)$$

equation 15 can be rewritten as

$$\frac{\tau \lambda^4}{N} = 55.818 \gamma \left[1. - \frac{11.658}{\lambda^2} \alpha \left(1. - \frac{2.8596}{\lambda^2} \delta \right) \right] \quad (17)$$

where $\gamma = \frac{(p+5)(p+4)(p+3)(p+2)(p+1)p}{(q-1)(q-2)(q-3)(q-4)(q-5)(q-6)}$ (18)

$$\delta = \frac{(p+8)(p+9)}{(q-9)(q-10)} \quad (19)$$

$$\alpha = \frac{(p+6)(p+7)}{(q-7)(q-8)} \quad (20)$$

If turbidities are now measured at three different wavelengths, then the above becomes a system of three equations and three unknowns. The parameters, p, q and N, can be calculated as explained below.

$$\text{Let } E = \frac{\tau_2 \lambda_2^4 - \tau_1 \lambda_1^4}{\tau_3 \lambda_3^4 - \tau_1 \lambda_1^4} \quad (21)$$

$$\text{Then } E = \frac{\lambda_1^2 \left(1 - \left(\frac{\lambda_1}{\lambda_2}\right)^2\right) + 2.8596 \delta \left(\left(\frac{\lambda_1}{\lambda_2}\right)^4 - 1\right)}{\lambda_1^2 \left(1 - \left(\frac{\lambda_1}{\lambda_3}\right)^2\right) + 2.8596 \delta \left(\left(\frac{\lambda_1}{\lambda_3}\right)^4 - 1\right)} \quad (22)$$

$$\begin{aligned} \text{Rearranging} \\ \delta = \frac{\lambda_1^2 \left[E \left(\left(\frac{\lambda_1}{\lambda_3} \right)^2 - 1 \right) - \left(\left(\frac{\lambda_1}{\lambda_2} \right)^2 - 1 \right) \right]}{2.8596 \left[E \left(\left(\frac{\lambda_1}{\lambda_3} \right)^4 - 1 \right) - \left(\left(\frac{\lambda_1}{\lambda_2} \right)^4 - 1 \right) \right]} \end{aligned} \quad (23)$$

$$\text{Let } \beta = \frac{\tau_3 \lambda_3^4}{\tau_1 \lambda_1^4} \quad (9)$$

$$\text{then from 17 } \alpha = \frac{(1-B) \lambda_1^2}{11.658 \left[\left(\frac{\lambda_1}{\lambda_3} \right)^2 \left(1 - \frac{2.8596 \delta}{\lambda_3^2} \right) - B \left(1 - \frac{2.8596 \delta}{\lambda_1^2} \right) \right]} \quad (24)$$

p and q can now be calculated from α and β using equations 19 and 20. Upon determination of these parameters, the number and weight average particle diameters can be calculated as follows

$$\bar{r}_n^3 = \frac{\int_0^{\infty} r^3 f(r) dr}{\int_0^{\infty} f(r) dr} \quad (25)$$

Upon substitution of the β distribution (11) for $f(r)$, noting that $\int_0^{\infty} f(r) dr = 1$, and integrating

$$\bar{r}_n = \left[\frac{p(p+1)(p+2)}{(q-1)(q-2)(q-3)} \right]^{1/3} \quad (26)$$

Similarly

$$\bar{r}_w^3 = \frac{\int_0^{\infty} r^6 f(r) dr}{\int_0^{\infty} r^3 f(r) dr} \quad (27)$$

$$\bar{r}_w = \left[\frac{(p+3)(p+4)(p+5)}{(q-4)(q-5)(q-6)} \right]^{1/3} \quad (28)$$

The number of particles per unit volume of solution, N , can be calculated from equation 17. The concentration can then be determined from

$$c = N\rho \int_0^{\infty} 4/3 \pi r^3 f(r) dr \quad (29)$$

That is
$$c = N\rho 4/3\pi \frac{p(p+1)(p+2)}{(q-1)(q-2)(q-3)} \quad (30)$$

APPENDIX B.

EXPERIMENTAL RESULTS

In this section, the results obtained from the 8 experiments carried out during the summer of 1974 are given. The measurement from the UV spectrophotometer is reported as equivalent absorbance rather than the actual reading. Equivalent absorbance is the absorbance that would be obtained from an undiluted sample of latex, if no secondary scattering occurred, that is

$$A^* = A \times \frac{V_d}{V_s}$$

where A^* equivalent absorbance

A absorbance measured on UV spectrophotometer

V_d total diluted volume

V_s volume of latex from reactor

A^* is given since the value is independent of the dilution system.

The experimental reaction conditions are given below:

	<u>Expts. 1-5</u>	<u>Expts. 6-8</u>
Temperature	50°C	50°C
Volume monomer	800 ml	400 ml
Volume water	1750 ml	1750 ml
Initiator	1.2 g	1.2 g
Emulsifier	15 g	12.5 g
Stirrer speed	150 rpm	150 rpm

Table B1: EQUIVALENT ABSORBANCE, REACTION 1

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
7	55	0	0	0	0	0
8	60	.4	.3	.2	.2	.4
9	75	.6	.6	.7	1.1	2.1
10	80	.7	.8	1.3	2.1	3.9
11	85	1.0	1.3	2.2	3.7	6.8
12	90	1.3	2.0	3.8	6.1	11.1
13	95	1.8	3.0	5.8	9.5	17.1
14	105	4.2	7.4	15.7	25.6	43.3
15	110	4.7	8.4	18.3	29.3	50.0
16	115	6.3	11.7	25.2	40.8	67.0
17	120	5.2	9.2	21.4	34.0	58.2
18	125	7.7	14.3	30.9	49.1	83.1
19	130	9.2	16.9	36.2	57.4	98.9
20	135	10.7	20.0	43.2	68.4	112.8
21	140	12.5	23.8	50.2	79.1	130.0
22	145	14.2	26.9	57.5	90.5	143.8

Table B1: (continued)

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
23	150	10.5	19.3	40.9	63.5	107.1
24	155	14.3	27.4	58.1	91.3	143.8
25	160	16.2	31.4	64.0	100.5	160.1
26	165	18.0	33.8	70.3	110.4	179.3
27	170	19.6	36.7	76.6	118.8	---*

*Sample is above the measurement limit of spectrophotometer

Fig. B1

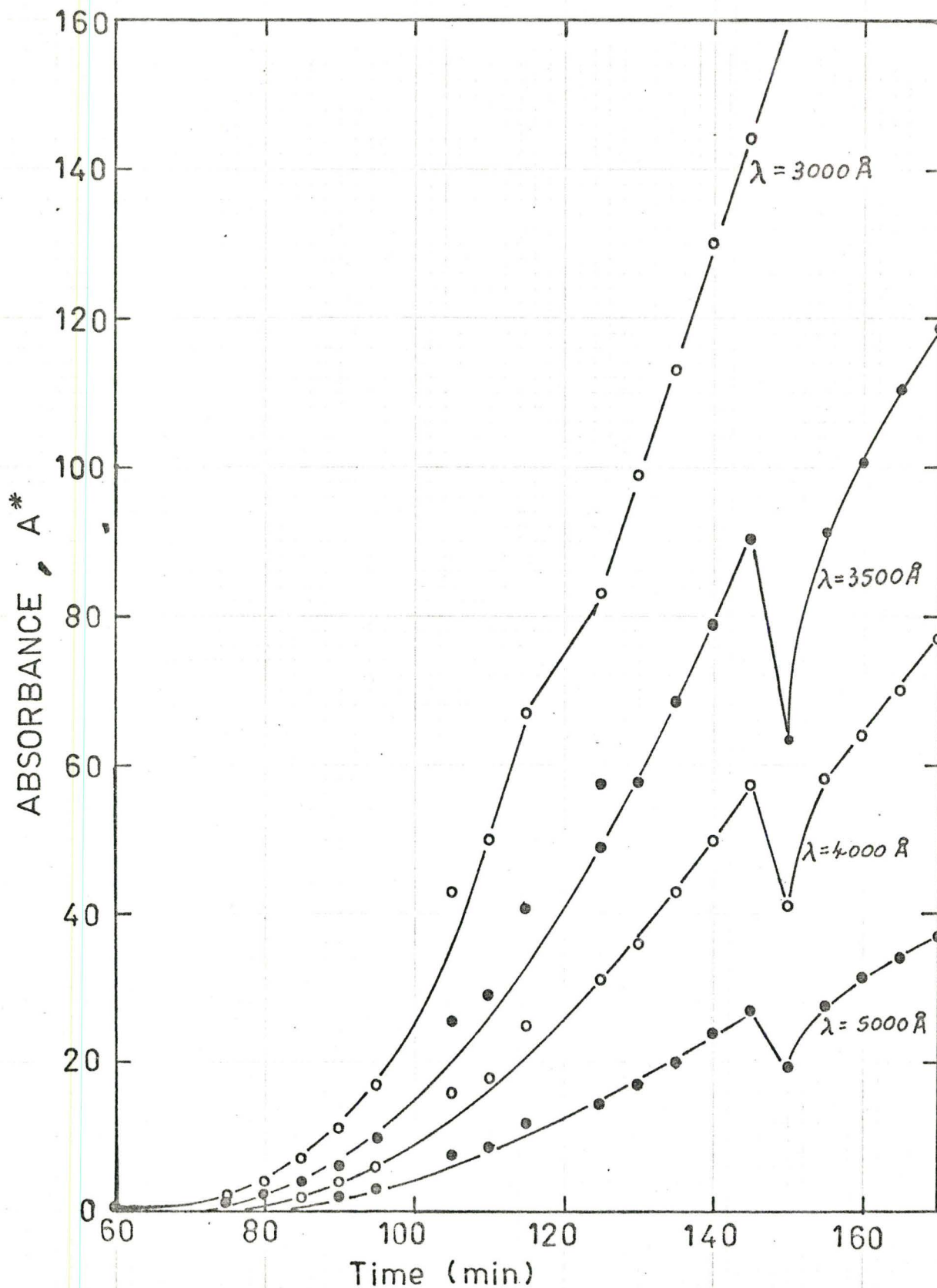
EQUIVALENT ABSORBANCE
REACTION 1

TABLE: B2 EQUIVALENT ABSORBANCE, REACTION 2

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
4	20	0	.1	.1	0	0
5	25	.2	.2	.2	.1	.2
6	30	.2	.3	.3	.4	.7
7	35	.3	.5	.7	1.0	1.9
8	40	.5	.7	1.2	1.9	4.0
9	45	.8	1.3	2.4	3.9	7.1
10	50	1.0	1.8	3.8	6.3	11.5
11	55	1.6	2.7	5.8	9.5	17.0
12	60	2.1	3.9	8.6	14.2	24.4
13	65	3.1	5.3	11.7	19.2	32.6
14	70	4.1	7.1	15.5	24.8	41.7
15	75	4.8	8.7	19.4	30.5	51.4
16	80	5.8	10.6	23.3	37.0	61.8
17	85	6.8	13.3	28.7	45.2	74.0
18	90	7.9	15.4	33.0	51.9	86.0
19	95	9.5	17.2	36.8	57.7	97.1

continued

TABLE: B2 (continued)

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
20	100	10.6	19.5	41.7	66.0	109.4
21	105	12.0	22.2	47.1	73.7	122.8
22	110	13.3	24.8	51.6	81.8	133.7
23	115	15.1	27.8	58.5	91.5	146.2
24	120	16.4	30.4	64.0	99.5	158.4
25	125	--	33.2	70.0	107.8	173.8
26	130	20.2	37.2	77.6	119.4	197.2
27	135	21.8	40.2	84.0	129.4	209.8
28	140	21.2	39.6	83.0	127.9	202.2
29	145	24.8	45.0	93.0	142.0	232.0
30	150	25.2	46.3	95.9	149.2	237.4
31	155	27.0	51.0	104.2	159.8	254.2
32	160	29.2	53.0	109.2	169.0	266.0
33	165	30.2	56.0	114.2	174.0	278.0
34	170	32.8	59.6	121.1	186.9	296.0

Fig. B2

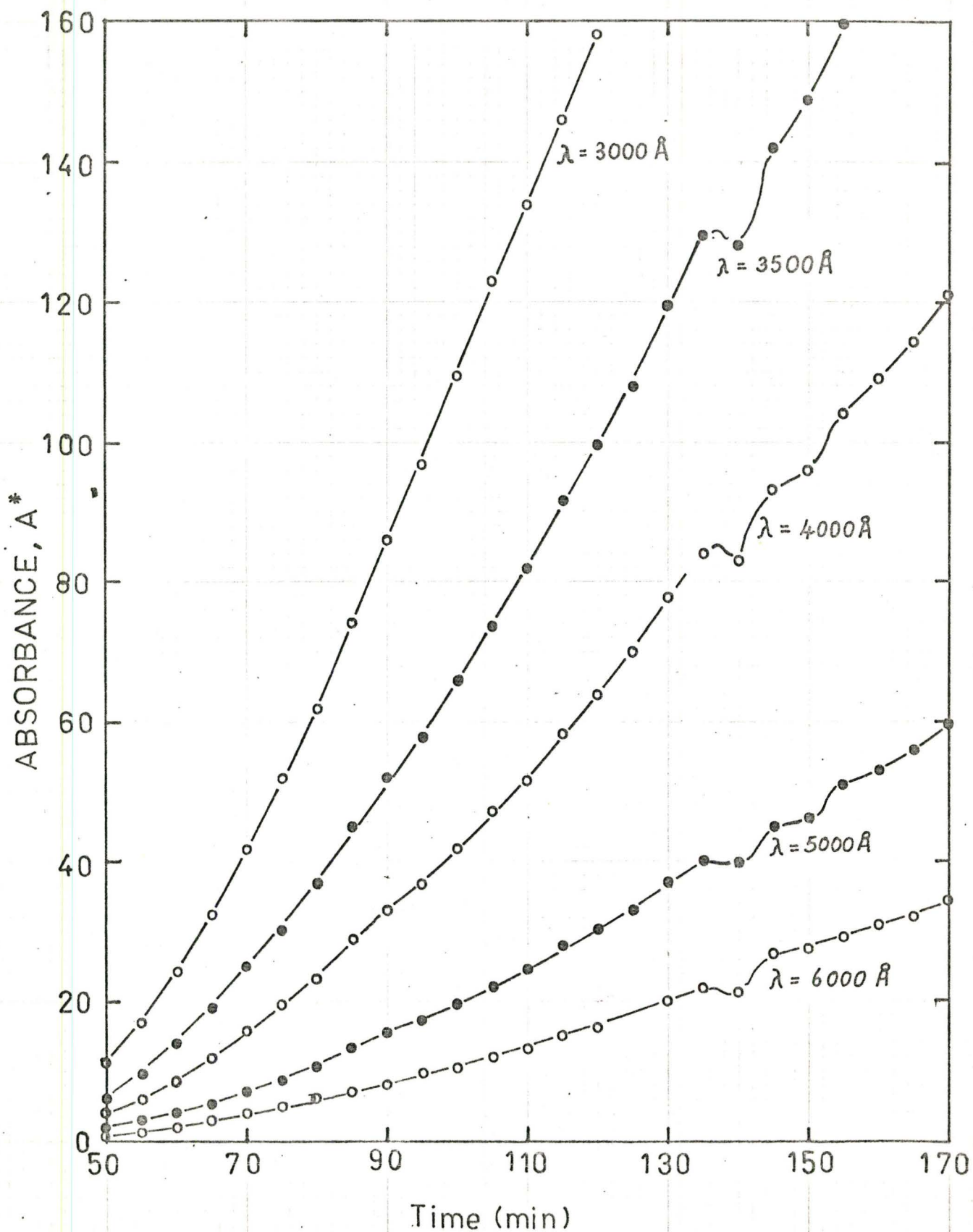
EQUIVALENT ABSORBANCE
REACTION 2

TABLE: B3 EQUIVALENT ABSORBANCE, REACTION 3

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
7	30	0	0	0	0	0
8	35	.1	.1	.1	.1	.2
9	40	.1	.2	.3	.5	.9
10	45	.2	.3	.8	1.4	2.5
11	50	.5	.9	2.0	3.1	5.9
12	55	1.0	1.6	3.6	6.0	10.7
13	60	1.5	2.6	5.5	9.2	16.8
14	65	2.4	4.2	9.1	14.5	25.3
15	70	3.0	5.5	12.3	19.9	33.4
16	75	4.3	7.7	16.8	26.9	45.8
17	80	5.3	9.8	21.9	34.7	55.2
18	85	6.6	12.3	25.7	41.5	67.4
19	90	8.0	14.9	31.8	49.6	81.9
20	95	9.5	17.5	36.9	57.4	95.5
21	100	12.0	21.4	45.3	70.0	115.1
22	105	12.9	24.2	50.8	78.3	125.8

Fig.B3

EQUIVALENT ABSORBANCE REACTION 3

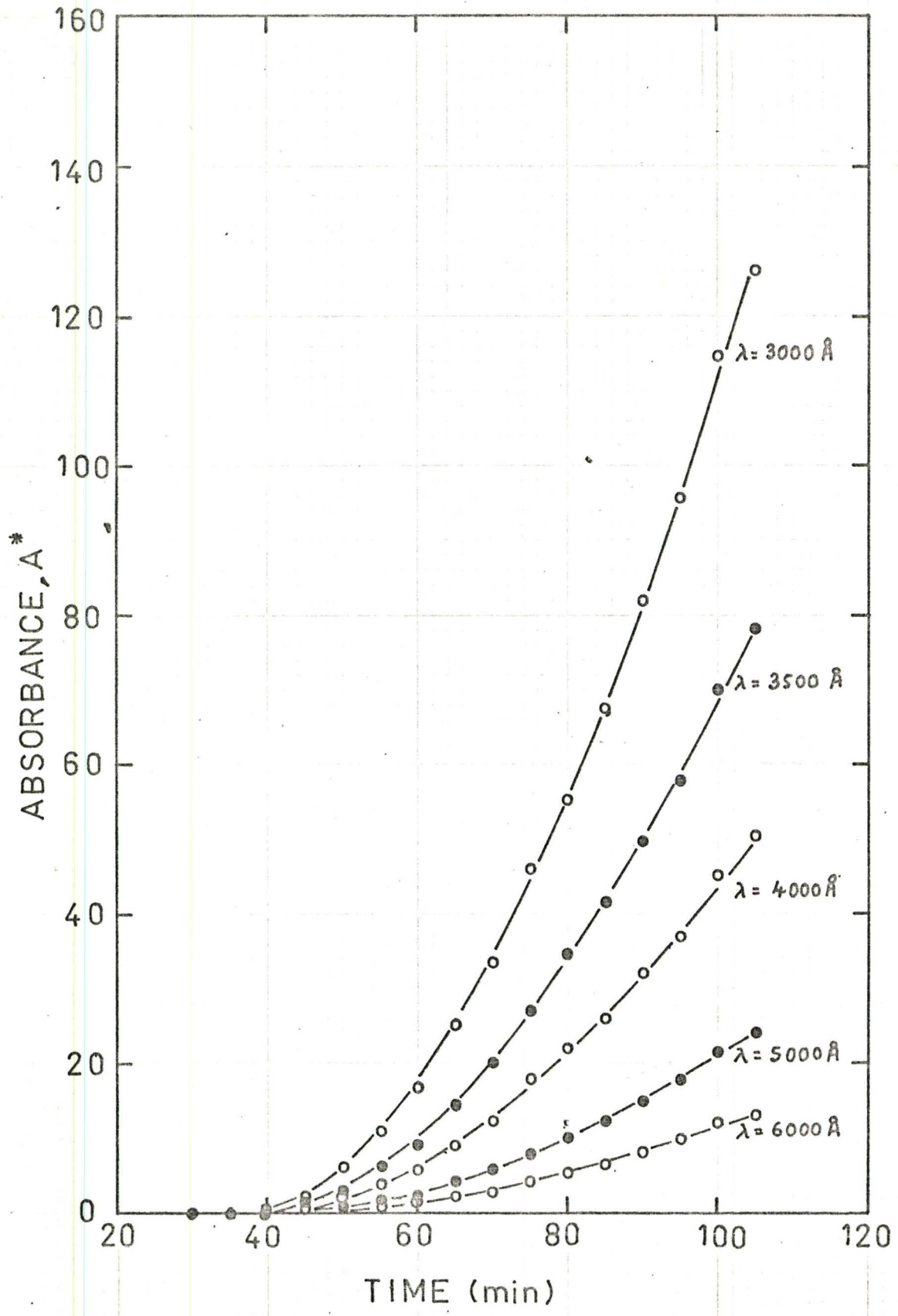


TABLE: B4 EQUIVALENT ABSORBANCE, REACTION 4

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
10	50	2.6	4.6	9.8	15.7	25.6
11	55	3.7	6.5	14.4	23.0	38.1
13	65	8.1	15.0	31.3	48.4	81.5
14	70	11.1	19.9	42.3	66.2	106.0
15	75	14.3	25.8	53.7	83.0	134.0
16	80	15.6	29.0	59.5	90.6	149.2
17	85	18.5	33.4	68.9	105.7	173.0
18	90	17.6	32.3	67.1	103.4	167.3
19	95	20.6	37.4	75.6	114.2	187.0
20	100	28.8	52.4	105.1	158.4	252.2
21	105	28.8	52.4	105.1	158.4	252.2
22	110	31.2	55.6	110.1	166.3	261.6
23	115	39.4	69.5	140.4	211.8	---*
24	120	36.6	64.9	131.2	197.5	---*
25	125	42.0	73.0	143.2	214.0	---*
26	130	44.8	78.7	153.9	229.0	---*
27	135	48.0	85.5	166.2	248.8	---*
28	140	60.6	105.0	208.0	---*	---*
29	145	55.6	96.6	191.0	---*	---*

TABLE: B4 (continued)

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
30	150	57.0	99.0	191.0	---*	---*
31	155	58.4	102.0	198.7	---*	---*
32	160	58.4	101.2	194.9	---*	---*

*Sample is above the measurement limit of spectrophotometer (a more diluted sample is required to measure absorbance)

Fig B4

EQUIVALENT ABSORBANCE
REACTION 4

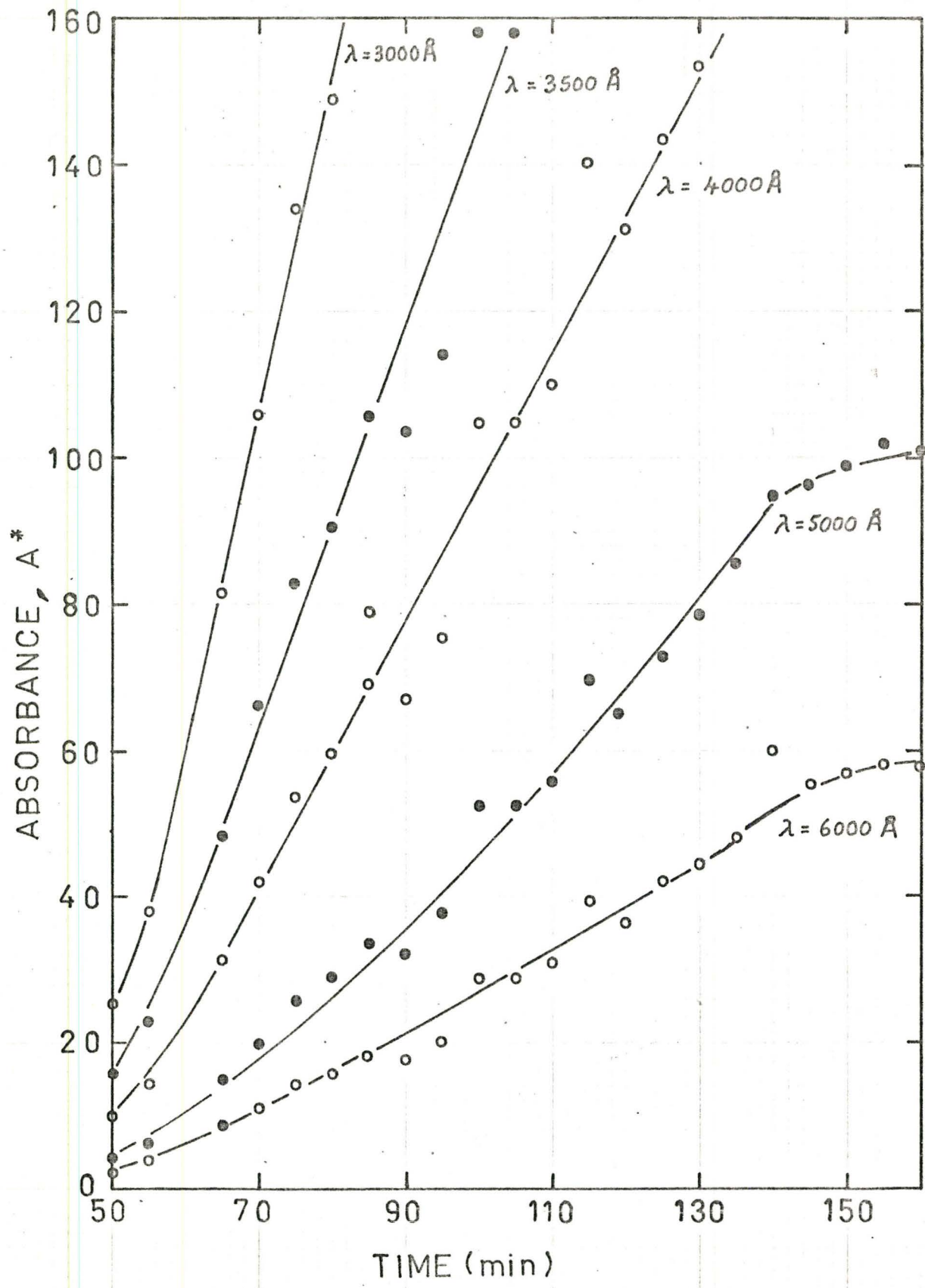


TABLE: B5 EQUIVALENT ABSORBANCE, REACTION 5

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
8	40	0	0	0	0	0
9	45	.6	.6	.8	1.2	1.7
10	50	1.2	2.0	3.9	6.4	10.8
11	55	3.0	4.6	9.6	15.8	26.3
12	60	3.9	7.3	15.6	25.6	42.3
14	70	8.5	15.6	34.2	53.8	87.0
15	75	12.4	24.9	49.6	77.1	123.4
16	80	15.6	29.0	59.9	91.9	146.9
19	95	25.2	46.8	93.5	142.8	224.2
20	100	28.9	56.2	111.7	168.1	259.6
21	105	35.2	64.0	127.1	191.8	294.0
22	110	41.0	73.4	145.2	217.6	---
23	115	38.2	68.9	136.1	205.0	316.0
24	120	39.0	70.1	140.2	212.0	332.0
25	125	44.7	82.0	162.4	246.0	380.0
26	130	41.9	74.6	149.0	225.0	351.8
27	135	44.7	80.4	156.2	233.8	380.0
28	140	46.7	86.6	170.9	257.0	401.0
29	145	45.9	85.8	169.0	253.0	395.5
30	150	44.7	81.6	158.4	238.4	374.4

Fig. B5

EQUIVALENT ABSORBANCE REACTION. 5

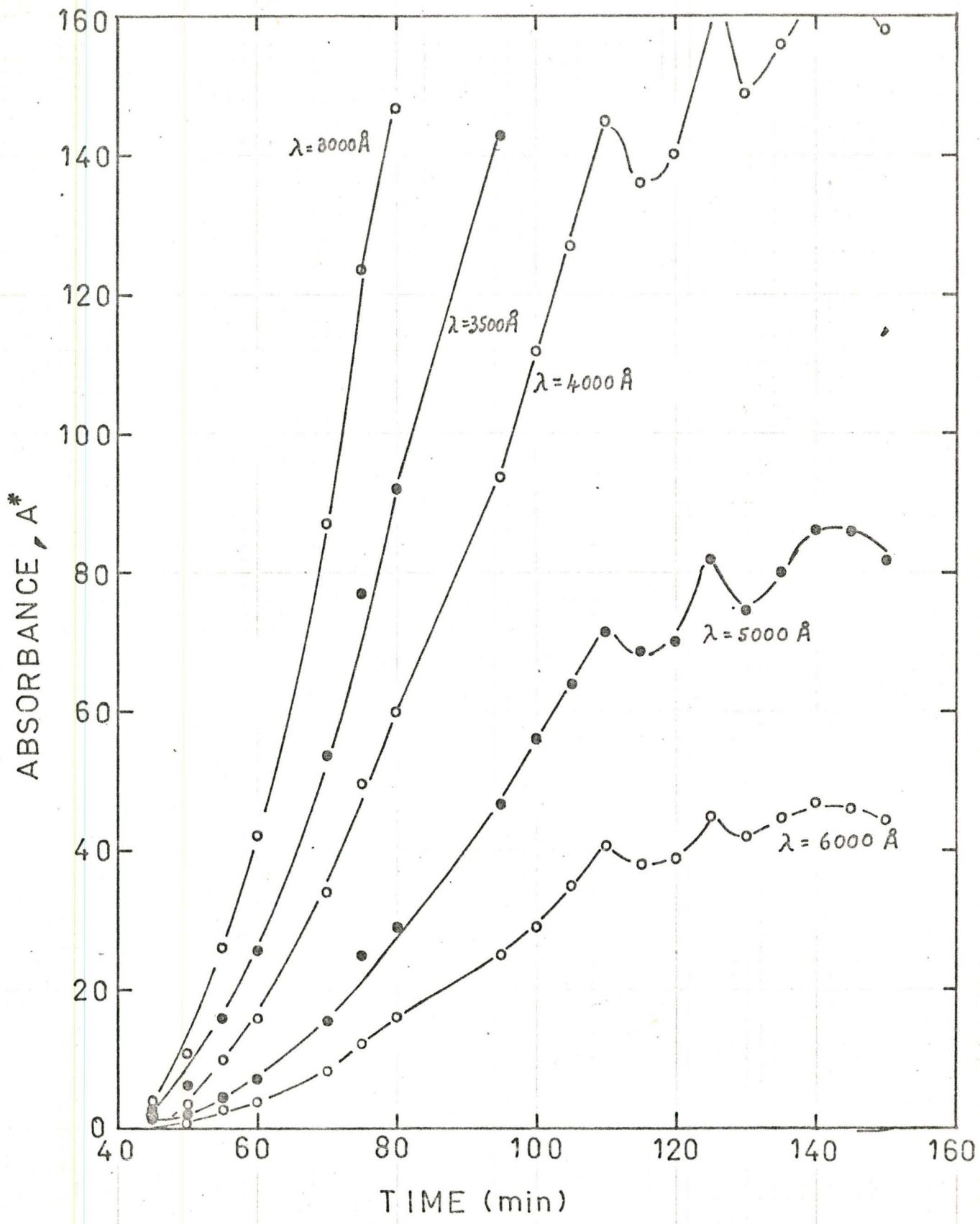


TABLE: B6 EQUIVALENT ABSORBANCE, REACTION 7

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
1	5	0	0	0	0	0
2	10	.9	.6	.9	.9	1.4
3	15	.9	.6	.9	.9	1.4
4	20	.6	.3	.6	.6	.9
5	25	2.2	2.5	3.2	4.1	6.0
6	30	3.5	5.7	10.4	15.8	25.4
7	35	4.1	8.9	20.6	34.2	61.1
8	40	8.9	18.0	41.2	66.5	115.7
10	50	14.2	29.2	65.2	103.0	175.1
11	55	15.8	31.0	68.1	107.2	181.3
12	60	16.8	32.6	71.5	113.0	189.5
13	65	16.5	32.0	70.0	110.2	184.5
14	70	16.5	32.3	70.9	111.0	186.9
15	75	16.5	32.3	70.9	110.8	186.0
16	80	16.5	32.3	70.9	111.0	186.0
17	85	17.4	33.5	72.4	111.8	182.2
18	90	17.5	33.6	72.4	112.0	182.2

Fig.B6

EQUIVALENT ABSORBANCE
REACTION 7

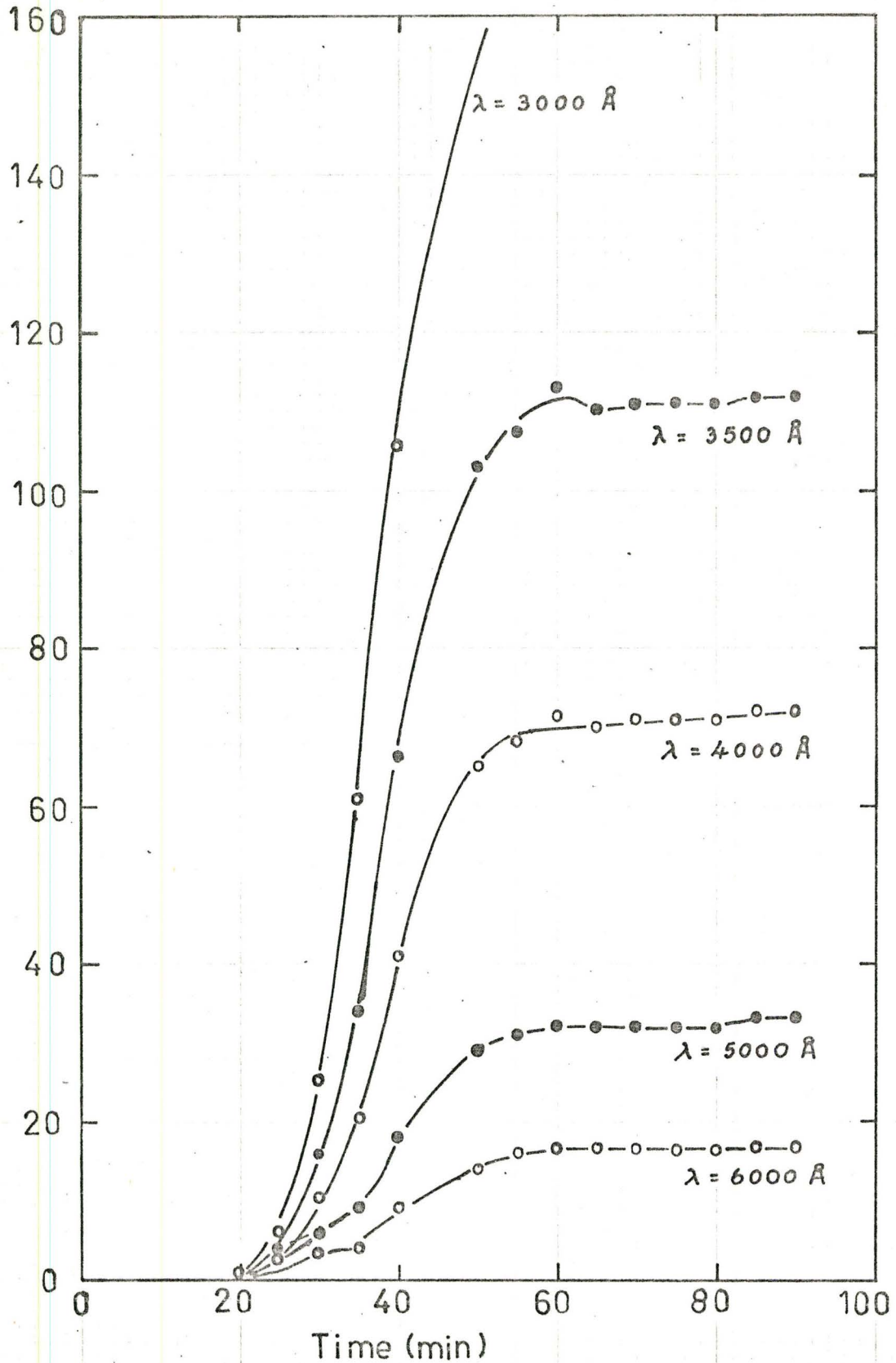
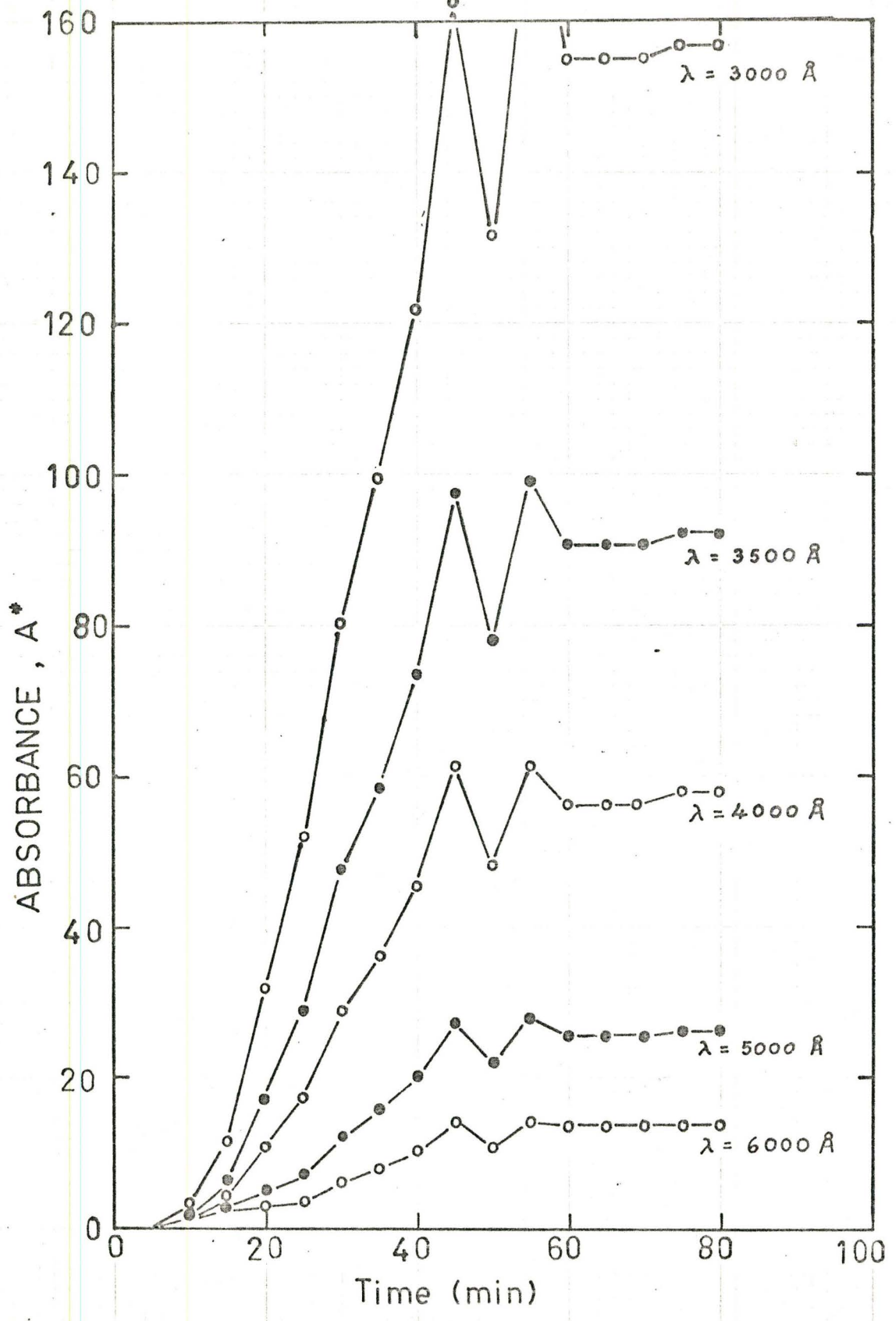


TABLE: B7 EQUIVALENT ABSORBANCE, REACTION 8

Sample No.	Time (Min)	Wavelength 600 nm	Wavelength 500 nm	Wavelength 400 nm	Wavelength 350 nm	Wavelength 300 nm
1	5	0	0	0	0	0
2	10	1.5	1.7	2.2	2.4	3.4
3	15	2.4	3.1	4.8	6.6	11.4
4	20	3.1	4.9	10.9	17.3	31.8
5	25	3.6	7.1	17.3	29.0	52.0
6	30	6.1	12.4	28.9	47.5	80.5
7	35	7.8	15.5	36.0	58.3	99.1
8	40	10.4	20.2	45.4	73.4	122.2
9	45	13.8	27.0	61.5	97.5	162.9
10	50	10.7	21.9	48.0	78.0	131.5
11	55	13.8	27.7	61.5	99.1	181.0
12	60	13.3	25.3	56.5	90.7	155.2
13	65	13.3	25.3	56.5	90.7	155.2
14	70	13.3	25.3	56.5	90.7	155.2
15	75	13.4	26.2	58.1	92.4	157.0
16	80	13.4	26.2	58.1	92.4	157.0

Fig. B7

EQUIVALENT ABSORBANCE REACTION 8



APPENDIX C SAMPLE PREPARATION

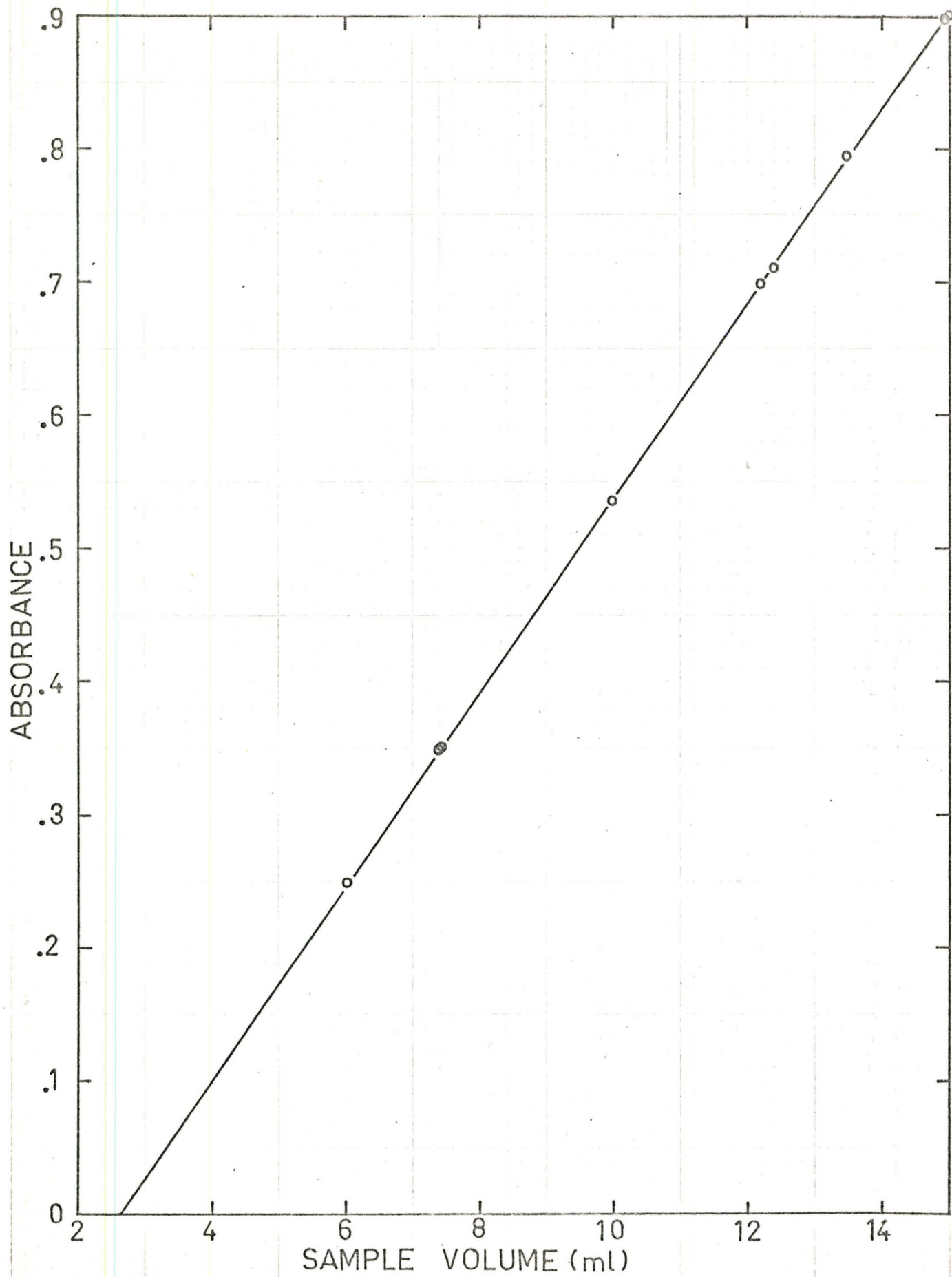
Upon final development of the sample system, an accurate controlled volume of latex solution could be diluted for measurement of absorbance using the computer. However, it was necessary to calibrate the system to obtain the correct volumes of latex and dilution vessel. To this end, samples were prepared using different withdrawal times of the syringe, using the same latex solution and measuring the absorbance of the diluted solution at a single wavelength (400 nm). The results of this experiment are tabulated in table C1 and displayed graphically in figure C1.

Table C1: ABSORBANCE vs LATEX CONCENTRATION

Syringe withdrawal time (secs)	volume withdrawn (ml)	measured absorbance
24.8	12.4	.710
24.4	12.2	.698
30.0	15.0	.900
14.9	7.45	.350
14.8	7.4	.348
29.85	14.92	.897
19.95	9.98	.534
27.0	13.5	.795
12.1	6.05	.248
20.0	10.0	.535

Fig C1

ABSORBANCE v LATEX CONC.



The important result from analysis of the data is that the absorbance has a linear relationship with latex concentration. This demonstrates that secondary scattering has no significant effect on the absorbance for the latex solutions used in this study. This is a requirement for determining particle size distributions by the Mie theory.

The linear relationship between absorbance and concentration also allows the use of the following equation to determine the effective volume of the dilution vessel and sample volume.

$$A = \frac{k}{VT} (V - V_d)$$

where A is the measured absorbance

k is a constant depending on the particle size distribution and number of particles in undiluted latex sample.

VT is the effective volume of the dilution vessel (total diluted volume)

V is volume withdrawn by syringe

V_d is volume of latex sample that remains in sample line and is not diluted (dead volume)

Using least squares linear regression, the dead volume was calculated to be 2.65 ml and the volume of the dilution vessel was 570 ml.

APPENDIX D COMPUTER PROGRAMS

In this section, the entire user part of the computer software system is presented. The programs are given in the following order,

1. INTER ... Intercommunication with operator (program executive)
2. INPUT ... Interpretation of names input by operator
3. SAMPL ... Operation of sampling system
4. RTDBØ ... Conversion of decimal input on teletype to binary
5. RTBDØ ... Conversion of binary to decimal output on teletype
6. MATHS ... Math routines
7. INFCE ... Routines to handle interface equipment
8. CLOCK ... System clock
9. PINIT ... Initializer of scheduled programs
10. UVANS ... Operation of UV analyzer
11. LOG ... Standard logging routine
12. FEEDS ... Controls feedrates to reactor
13. TCTRL ... Temperature control of reactor

```

0001 INTER
01 . TITL INTER
02 . ENT START ENTRY JOBS ERROR TMIN BEGIN
03 . ENT CHNGE FROM TO READ RDOCT STOP SCHED
04 . EXTN FLAGL SAMPL UVANS LOGST TTOO PINIT TRANS ITEM1
05 . EXTN CLOCK INPTT INPTP INPTD RTBDO RTDBO
06 . EXTN .BRK .PTY .FORK .QUIT
07 . EXTN INIT
08 . EXTN DEBUG
09 . NREL
10 ; THIS IS THE EXECUTIVE ROUTINE FOR RDOCS
11 ; ALL OPERATOR COMMUNICATION ENTERS THROUGH THIS PROGRAM
12 ; THIS FIRST SECTION DEALS WITH START UP OF SYSTEM
13
14 00000'002401 TMIN: JMP @ +1
15 00001'177777 INIT
16
17 00002'177777 START: .PTY ;SET HIGH PRIORITY FOR THIS PROGRAM
18 00003'000007 7
19 00004'177777 .FORK ;START UP SYSTEM CLOCK
20 00005'000015 15
21 00006'177777 CLOCK
22 00007'000004' .FORK ;INITIALIZE SCHEDULER
23 00010'000040 40
24 00011'177777 PINIT
25 00012'000007' .FORK ;START READING A/D CHANNELS
26 00013'000377 377
27 00014'177777 TRANS
28 00015'000012' .FORK ;INITIALIZE LOGGING ROUTINE
29 00016'000077 77
30 00017'177777 LOGST
31 00020'000015' .FORK ;PREPARE UV SPECTROPHOTOMETER
32 00021'000050 50
33 00022'177777 UVANS
34
35 00023'177777 PAUSE: .BRK ;OPERATOR INTERRUPT - THIS SECTION
36 00024'000201 201 ;PROCEEDS UPON ISSUE OF CTRL A
37 00025'102400 SUB 0 0 ;STOP LOGGING ROUTINE
38 00026'042430 STA 0 @POINT+5 ;FROM PRINTING
39 00027'000020' .FORK
40 00030'000010 10 ;FIND OUT WHAT OPERATOR WANTS
41 00031'000033' JOBS
42 00032'000771 JMP PAUSE
43
44 00033'006422 JOBS: JSR @POINT+4 ;PRINT CR AND LF
45 00034'000043' MESS
46 00035'006415 ENTRY: JSR @POINT+1 ;GET OPERATOR INSTRUCTION
47 00036'115000 MOV 0 3
48 00037'001400 JMP 0 3 ;GO TO REQUESTED JOB
49
50 00040'006415 ERROR: JSR @POINT+4 ;PRINT NO IF INPUT NOT ACCEPTABLE
51 00041'000044' MESS+1
52 00042'000771 JMP JOBS ;GO BACK FOR MORE INPUT
53
54 00043'000430"MESS: AA*2
55 00044'000450" CC*2
56 00045'000434" BB*2
57 00046'000454" DD*2
58 00047'000460" EE*2
59 00050'000464" FF*2

```

```

01
02
03           ; THE FOLLOWING SET OF ROUTINES CARRY OUT THE
04           ; OPERATOR INSTRUCTIONS
05
06 00051'177777 POINT:  INFTD
07 00052'177777       INFTP
08 00053'177777       RTBDO
09 00054'177777       RTDBO
10 00055'177777       TTOD
11 00056'177777       FLAGL
12 00057'177777       INFTT
13
14 00060'000000 ADRES:  0
15 00061'000006 C6:    6
16 00062'177772 N6:   -6
17
18           ; THIS SECTION STARTS CHANGE OF DATA
19
20
21 00063'006766 CHNGE:  JSR @POINT      ; GET DATA LOCATION
22 00064'040774       STA 0 ADRES      ; THIS ADDRESS - STORE IT
23 00065'000750       JMP ENTRY        ; GO FOR NEXT INSTRUCTION
24
25           ; THE FOLLOWING CAUSES CURRENT DATA REGISTER TO BE PRINTED
26
27 00066'022772 FROM:  LDA 0 @ADRES    ; LOAD VALUE IN ADDRESS
28 00067'024772       LDA 1 C6        ; #SPACES TO PRINT
29 00070'006763       JSR @POINT+2    ; PRINT VALUE IN DECIMAL
30 00071'000744       JMP ENTRY        ; GO FOR NEXT INSTRUCTION
31
32           ; THIS SECTION COMPLETE CHANGE OF DATA
33
34 00072'006762 TO:    JSR @POINT+3    ; READ VALUE
35 00073'046765       STA 1 @ADRES    ; STORE IT
36 00074'000737       JMP JOBS
37
38           ; THIS SECTION READS A DATA LOCATION AND PRINTS IT
39
40 00075'006754 READ:  JSR @POINT      ; GET LOCATION
41 00076'115000       MOV 0 3
42 00077'021400       LDA 0 0 3      ; LOAD VALUE
43 00100'024761       LDA 1 C6        ; #SPACES TO PRINT
44 00101'006752       JSR @POINT+2    ; PRINT VALUE IN DECIMAL
45 00102'000773       JMP READ        ; REPEAT ON SAME LINE
46
47           ; THIS SECTION READS A LOCATION IN OCTAL
48
49 00103'006746 RDOCT: JSR @POINT      ; GET DATA LOCATION
50 00104'115000       MOV 0 3
51 00105'021400       LDA 0 0 3      ; LOAD VALUE
52 00106'024754       LDA 1 N6        ; INDICATE OCTAL NUMBER
53 00107'006744       JSR @POINT+2    ; PRINT 6 SPACES OCTAL
54 00110'000773       JMP RDOCT      ; REPEAT
55
56           ; THIS SECTION STOPS A PROGRAM RUNNING
57
58 00111'006746 STOP:  JSR @POINT+6    ; GET PROGRAM
59 00112'040404       STA 0 +4

```

```

0003 INTER
01 00113'014403 DSZ .+3
02 00114'000027 . FORK ; INITIATE PROGRAM STOP
03 00115'000050 50
04 00116'177777 SAMPL
05 00117'000714 JMP JOBS
06
07 ; THIS SECTION STARTS A TASK PROGRAM
08
09 00120'006737 BEGIN: JSR @POINT+6 ; GET TASK TO BE STARTED
10 00121'040403 STA 0 .+3
11 00122'000114 . FORK ; CREATE JOB
12 00123'000050 50
13 00124'000116 SAMPL
14 00125'000706 JMP JOBS ; GO BACK FOR NEXT INSTRUCTION
15
16 ; THIS SECTION SCHEDULES A TASK TO BE RUN AT SOME FUTURE TIME
17
18 00126'006731 SCHED: JSR @POINT+6 ; INPUT PROGRAM TO BE SCHEDULED
19 00127'040425 STA 0 PROG ; SAVE PROGRAM ADDRESS
20 00130'006725 JSR @POINT+4 ; OUTPUT
21 00131'000045 MESS+2 ; "TO START AT"
22 00132'004424 JSR GTTME ; GET STARTING TIME
23 00133'000000 STRT: 0
24 00134'006721 JSR @POINT+4 ; OUTPUT
25 00135'000050 MESS+5 ; "AND STOP AT"
26 00136'004420 JSR GTTME ; GET STOPPING TIME
27 00137'000000 STP: 0
28 00140'034415 LDA 3 ITEMN ; LOAD ADDRESS OF NEXT ITEM
29 00141'020413 LDA 0 PROG ; LOAD SCHEDULED PROGRAM
30 00142'041400 STA 0 0 3 ; STORE IT FOR SCHEDULER
31 00143'175400 INC 3 3
32 00144'020767 LDA 0 STRT ; LOAD WHEN TO START PROGRAM
33 00145'041400 STA 0 0 3 ; STORE IT
34 00146'175400 INC 3 3
35 00147'020770 LDA 0 STP ; LOAD WHEN TO STOP PROGRAM
36 00150'041400 STA 0 0 3 ; STORE IT
37 00151'175400 INC 3 3 ; PREPARE ADDRESS INDICATOR FOR NEXT I
38 00152'054403 STA 3 ITEMN
39 00153'000660 JMP JOBS ; RETURN FOR NEXT INSTRUCTION
40
41 00154'000124 PROG: SAMPL
42 00155'177777 ITEMN: ITEM1
43
44 00156'054435 GTTME: STA 3 AC3
45 00157'006675 JSR @POINT+3 ; GET TIME IN MINUTES
46 00160'125113 MOVL# 1 1 SNC ; CHECK SIGN
47 00161'000403 JMP .+3 ; SIGN POSITIVE - SKIP
48 00162'124400 NEG 1 1 ; MAKE POSITIVE
49 00163'044426 STA 1 SIGN ; INDICATE SIGN ACTUALLY NEGATIVE
50 00164'127120 ADDZL 1 1 ; N*4
51 00165'121000 MOV 1 0 ; AC0=N*4
52 00166'127120 ADDZL 1 1 ; N*16
53 00167'127120 ADDZL 1 1 ; N*64
54 00170'106400 SUB 0 1 ; N*60
55 00171'044421 STA 1 TEMP ; STORE NUMBER IN SECONDS
56 00172'006663 JSR @POINT+4 ; OUTPUT
57 00173'000046 MESS+3 ; "MIN"
58 00174'006660 JSR @POINT+3 ; GET SECONDS PART OF TIME
59 00175'020415 LDA 0 TEMP ; FIND MINUTE PART

```

0004 INTER

```

01 00176'107000      ADD 0 1          ;GET CORRECT TIME
02 00177'020412      LDA 0 SIGN        ;CHECK SIGN
03 00200'101004      MOV 0 0 SZR
04 00201'124400      NEG 1 1
05 00202'046411      STA 1 @AC3
06 00203'102400      SUB 0 0          ;MAKE SURE POSITIVE FOR NEXT ENTRY
07 00204'040405      STA 0 SIGN
08 00205'006650      JSR @POINT+4    ;OUTPUT
09 00206'000047'     MESS+4          ;"SEC"
10 00207'010404      ISZ AC3
11 00210'002403      JMP @AC3        ;RETURN
12
13 00211'000000      SIGN: 0
14 00212'000000      TEMP: 0
15 00213'000000      AC3: 0
16
17                      AA: .TXT @<15><12><40>@
    00214'005015
    00215'000040
18                      BB: .TXT @TO START AT@
    00216'047524
    00217'051440
    00220'040524
    00221'052122
    00222'040440
    00223'000124
19                      CC: .TXT @ N@e
    00224'047040
    00225'000117
20                      DD: .TXT @MINE
    00226'044515
    00227'000116
21                      EE: .TXT @SECE@
    00230'042523
    00231'000103
22                      FF: .TXT @ AND STOP AT@
    00232'040440
    00233'042116
    00234'051440
    00235'047524
    00236'020120
    00237'052101
    00240'000000
23
24          000000'     .END TMIN

```

0001 INPUT

```

01 . TITL INPUT
02 . ENT INFTP INFTD INFTT
03 . EXTN . IOX . QUIT
04 . EXTN MONMR INITR EMJLS RDOCT ATOD ATOD1
05 . EXTN SAMPL LOG CHNGE TO FROM READ ERROR
06 . EXTN TCTRL TSP TCINT BEGIN TYPEC
07 . EXTN HOUR MINIT SECND SMINT LGINT SMVOL STOP
08 . EXTN SCHED RTIME ITEM1 I1SRT I1STP
09 . EXTN ITEM2 I2SRT I2STP ITEM3 I3SRT I3STP
10 . EXTN ITEM4 I4SRT I4STP ITEM5 I5SRT I5STP
11 . EXTN ITEM6 I6SRT I6STP ITEM7 I7SRT I7STP
12 . EXTN MAXMF MAXIF MAXEF MFLOW IFLOW EFLOW
13 . NREL
14
15 ; PROGRAM GETS A STRING OF LETTERS FROM TELETYPE
16 ; CHECKS CODE OF STRING FOR ACCEPTABLE ADDRESS
17 ; IF ACCEPTABLE - RETURNS WITH ACO CONTAINING ADDRESS
18 ; IF NOT - ERROR MESSAGE IS PRINTED
19
20 00000'020463 INFTT: LDA 0 LISTT ; ENTRY POINT FOR TASK INPUT
21 00001'040461 STA 0 LIST
22 00002'020555 LDA 0 TABLT
23 00003'040553 STA 0 TABLE
24 00004'000412 JMP INPUT
25
26 00005'020465 INFTP: LDA 0 LISTP ; ENTRY POINT FOR PROGRAM INPUT
27 00006'040454 STA 0 LIST
28 00007'020556 LDA 0 TABLP
29 00010'040546 STA 0 TABLE
30 00011'000405 JMP INPUT
31
32 00012'020473 INFTD: LDA 0 LISTD ; ENTRY POINT FOR DATA ADDRESS INPUT
33 00013'040447 STA 0 LIST
34 00014'020563 LDA 0 TABLD
35 00015'040541 STA 0 TABLE
36
37 00016'054437 INPUT: STA 3 AC3 ; SAVE RETURN ADDRESS
38 00017'152400 SUB 2 2 ; CLEAR AC2 FOR CODING INPUT
39 00020'177777 . IOX
40 00021'000000 0 ; TELETYPE
41 00022'020000 020000 ; INPUT AND ECHO
42 00023'000054' CHARR ; ADDRESS FOR INPUT
43 00024'000001 1 ; READ 1 CHARACTER
44 00025'177777 ERROR ; ERROR RETURN ADDRESS
45 00026'020426 LDA 0 CHARR ; LOAD INPUT CHARACTER
46 00027'024430 LDA 1 C101 ; LOAD ASCII "A"
47 00030'034430 LDA 3 C132 ; LOAD ASCII "Z"
48 00031'106033 ADCZ# 0 1 SNC ; CHECK IF INPUT
49 00032'116033 ADCZ# 0 3 SNC ; IS A CHARACTER
50 00033'000404 JMP CHECK ; NO - END OF INPUT
51 00034'151120 MOVZL 2 2 ; YES DO CODE
52 00035'113000 ADD 0 2 ; COMPLETE CODE
53 00036'000762 JMP INPUT+2 ; GO BACK FOR NEXT CHARACTER
54 00037'034423 CHECK: LDA 3 LIST ; GET ADDRESS OF LIST OF ACCEPTABLE ADI
55 00040'126400 SUB 1 1 ; CLEAR ADDRESS INDICATOR (AC1)
56 00041'175400 INC 3 3 ; GET ADDRESS
57 00042'021400 LDA 0 0 3 ; GET CODE
58 00043'101005 MOV 0 0 SNR ; END OF LIST ?
59 00044'002415 JMP @POINT ; YES AND CODE NOT ACCEPTABLE

```

0002 INPUT

01	00045	125400	INC 1 1	; NO - INCREMENT ADDRESS LOCATION INDIC
02	00046	112414	SUB# 0 2 SZR	; IS THIS THE CODE ?
03	00047	000772	JMP CHECK+2	; NO - GO BACK TO CHECK NEXT CODE
04	00050	034506	LDA 3 TABLE	; GET LOCATION OF TABLE OF ADDRESSES
05	00051	137000	ADD 1 3	; GET ADDRESS OF ADDRESS
06	00052	021400	LDA 0 0 3	; LOAD ADDRESS INDICATED BY CODE
07	00053	002402	JMP @AC3	; RETURN TO CALLING PROGRAM
08				
09	00054	000000	CHARR: 0	
10	00055	000000	AC3: 0	
11	00056	000177	MASK: 177	
12	00057	000101	C101: 101	
13	00060	000132	C132: 132	
14	00061	000025	POINT: ERROR	
15	00062	000062	LIST: LIST	
16				
17	00063	000063	LISTT: LISTT	
18	00064	011365	11365	; SAMPLE
19	00065	023210	23210	; MONOMER
20	00066	112630	112630	; INITIATOR
21	00067	023640	23640	; EMULSIFIER
22	00070	044370	44370	; CONTROLT
23	00071	000000	0	
24				
25	00072	000072	LISTP: LISTP	
26	00073	001025	1025	; LOG
27	00074	010363	10363	; CHANGE
28	00075	002143	2143	; FROM
29	00076	000367	367	; TO
30	00077	002152	2152	; READ
31	00100	002326	2326	; STOP
32	00101	045741	45741	; SCHEDULE
33	00102	022546	22546	; READOCT
34	00103	004714	4714	; START
35	00104	000000	0	
36				
37	00105	000105	LISTD: LISTD	
38	00106	114322	114322	; TYPECONTROL <
39	00107	002170	2170	; HOUR
40	00110	011341	11341	; MINUTE
41	00111	011344	11344	; SECOND
42	00112	023724	23724	; SMPLINT
43	00113	024002	24002	; SMPLVOL
44	00114	011274	11274	; LOGINT
45	00115	011556	11556	; TEMFSP
46	00116	047014	47014	; TEMFCINT
47	00117	045463	45463	; REACTINE
48	00120	002072	2072	; ATOD
49	00121	004266	4266	; ATODB
50	00122	045267	45267	; MAXFLOWN
51	00123	045263	45263	; MAXFLOWI
52	00124	045257	45257	; MAXFLOWE
53	00125	004367	4367	; FLOWN
54	00126	004363	4363	; FLOWI
55	00127	004357	4357	; FLOWE
56	00130	004437	4437	; ITEM A
57	00131	011731	11731	; START A
58	00132	004755	4755	; STOP A
59	00133	004440	4440	; ITEM B

0003 INPUT

01	00134'011732	11732	; STARTB
02	00135'004756	4756	; STOPB
03	00136'004441	4441	; ITEM C
04	00137'011733	11733	; STARTC
05	00140'004757	4757	; STOPC
06	00141'004442	4442	; ITEM D
07	00142'011734	11734	; STARTD
08	00143'004760	4760	; STOPD
09	00144'004443	4443	; ITEM E
10	00145'011735	11735	; STARTE
11	00146'004761	4761	; STOPE
12	00147'004444	4444	; ITEM F
13	00150'011736	11736	; STARTF
14	00151'004762	4762	; STOPF
15	00152'004445	4445	; ITEM G
16	00153'011737	11737	; STARTG
17	00154'004763	4763	; STOPG
18	00155'000000	0	
19			
20	00156'000156'TABLE:	TABLE	
21			
22	00157'000157'TABL:	TABL	
23	00160'177777	SAMPL	
24	00161'177777	MONMR	
25	00162'177777	INTR	
26	00163'177777	EMULS	
27	00164'177777	TCTRL	
28			
29	00165'000165'TABLP:	TABLP	
30	00166'177777	LOG	; ADDRESS OF LOG
31	00167'177777	CHNGE	; ADDRESS OF CHNGE
32	00170'177777	FROM	
33	00171'177777	TO	
34	00172'177777	READ	
35	00173'177777	STOP	
36	00174'177777	SCHED	
37	00175'177777	RDOCT	
38	00176'177777	BEGIN	
39			
40	00177'000177'TABLD:	TABLD	
41	00200'177777	TYPEC	
42	00201'177777	HOUR	
43	00202'177777	MINIT	
44	00203'177777	SECND	
45	00204'177777	SMINT	
46	00205'177777	SNVOL	
47	00206'177777	LGINT	
48	00207'177777	TSP	
49	00210'177777	TCINT	
50	00211'177777	RTIME	
51	00212'177777	ATOD	
52	00213'177777	ATODI	
53	00214'177777	MAXMF	
54	00215'177777	MAXIF	
55	00216'177777	MAXEF	
56	00217'177777	NFLOW	
57	00220'177777	IFLOW	
58	00221'177777	EFLOW	
59	00222'177777	ITEM1	

0004 INPUT
01 00223'177777
02 00224'177777
03 00225'177777
04 00226'177777
05 00227'177777
06 00230'177777
07 00231'177777
08 00232'177777
09 00233'177777
10 00234'177777
11 00235'177777
12 00236'177777
13 00237'177777
14 00240'177777
15 00241'177777
16 00242'177777
17 00243'177777
18 00244'177777
19 00245'177777
20 00246'177777
21
22

I1SRT
I1STP
ITEM2
I2SRT
I2STP
ITEM3
I3SRT
I3STP
ITEM4
I4SRT
I4STP
ITEM5
I5SRT
I5STP
ITEM6
I6SRT
I6STP
ITEM7
I7SRT
I7STP

. END

```

01 .TITL SAMPL
02 .ENT SAMPL SMINT SMVOL SMIN SSEC
03 .EXTN .PTY .FORK .WAIT RTIME .XMIT .QUIT TTOO
04 .EXTN RELYS
05 .NREL
06
07 ; THIS PROGRAM HANDLES ALL THE VALVES, INFUSION PUMP, AND
08 ; STIRRER FOR THE SAMPLING DILUTION SYSTEM.
09 ;
10 ; THIS IS A TASK PROGRAM
11 ; - USES .XMIT OVER CHANNEL 3 FOR UV ANALYSER ROUTINE
12
13 00000'000454 SMINT: 300. ;SAMPLING INTERVAL(SECS)
14 00001'000003 PURGE: 3. ;SAMPLE LINE PURGE TIME
15 00002'000005 STINT: 5. ;STIRRING INTERVAL
16 00003'000017 EMINT: 15. ;TIME REQUIRED TO EMPTY
17 00004'000024 SMVOL: 20. ;SAMPLE VOLUME
18 00005'000010 SLFSH: 10 ;SAMPLE LINE FLUSH TIME
19 00006'000012 FSHTM: 10. ;FLUSHING TIME FOR DILURION VESSEL
20 00007'000031 UVINT: 25. ;DELAY IN OPENING VALVE
21 00010'000043 FILLR: 35. ;MINIMUM TIME TO FILL VESSEL
22 00011'000170 MINTM: 120. ;TOTAL TIME TO COMPLETE A SAMPLE
23 00012'000055 MAXST: 45. ;MAXIMUM SYRINGE WITHDRAWAL TIME
24 ;
25 ; RELAY 1 = WATER VALVE IN
26 ; RELAY 2 = VALVE TO DRAIN
27 ; RELAY 3 = OVERFLOW VALVE
28 ; RELAY 4 = POWER TO SYRINGE MACHINE
29 ; RELAY 5 = 0 - WITHDRAW SYRINGE 1 - INFUSE SYRINGE
30 ; RELAY 6 = SAMPLE INLET VALVE TO DILUTER
31 ; RELAY 7 = VALVE TO UV ANALYSER
32 ; RELAY 8 = STIRRER CONTROL
33 ; RELAY 9 = PURGE VALVE
34 ; RELAY 10= REACTOR VALVE
35 ;
36 00013'012500 RELAY: 012500 ;TABLE OF RELAYS
37 00014'000400 000400 ;FOR SWITCHING VALVES
38 00015'021000 021000
39 00016'061000 061000
40 00017'060000 060000
41 00020'140000 140000
42 00021'134000 134000
43 00022'102200 102200
44 00023'000700 ,000700
45 00024'120000 120000
46
47 00025'177777 POINT: TTOO
48 00026'177777 RTIME
49 00027'000000 SMIN: 0
50 00030'000000 SSEC: 0
51 00031'000000 DRAW: 0
52 00032'000767 STATUS: JMP .-9.
53
54 00033'000535 STOPR: JMP END
55
56 ;
57 ; THE FOLLOWING SECTION PREPARES FOR SAMPLING
58 ;
59 00034'020776 SAMPL: LDA 0 STATUS ;THIS INSTRUCTION ALLOWS PROGRAM TO R

```

```

01 00035'040414      STA 0 PLACE
02 00036'177777      .PTY          ; SET PRIORITY
03 00037'000100      100
04
05          ; SAMPLE CONTROL
06
07 00040'177777 FORK: .FORK          ; TAKE SAMPLE
08 00041'000101      101
09 00042'000052'     DO
10 00043'020735      LDA 0 SMINT      ; WAIT FOR SPECIFIED TIME INTERVAL
11 00044'100400      NEG 0 0
12 00045'177777      .WAIT
13 00046'000144      100.
14 00047'101404      INC 0 0 SZR
15 00050'000775      JMP .-3
16 00051'000767 PLACE: JMP .-9.
17
18          ; THIS SECTION TAKES A SAMPLE
19
20 00052'020726 DO:  LDA 0 SMINT      ; CHECK SAMPLE INTERVAL
21 00053'024731      LDA 1 SMVOL
22 00054'125120      MOVZL 1 1          ; BOTH INFUSE AND WITHDRAW
23 00055'030734      LDA 2 MINTM      ; LOAD MINIMUM SAMPLE TIME
24 00056'147000      ADD 2 1          ; COMPUTE TOTAL TIME TO SAMPLE
25 00057'106513      SUBL# 0 1 SNC    ; ENOUGH TIME TO SAMPLE ?
26 00060'000506      JMP SEROR      ; NO - PRINT ERROR AND QUIT
27 00061'024723      LDA 1 SMVOL      ; LOAD SAMPLE VOLUME (*2.)
28 00062'044747      STA 1 DRAW      ; SAVE VALUE FOR LATER ON
29 00063'030727      LDA 2 MAXST      ; LOAD MAXIMUM SYRINGE TIME
30 00064'146513      SUBL# 2 1 SNC    ; VALUE TOO BIG ?
31 00065'000501      JMP SEROR      ; YES - PRINT ERROR AND QUIT
32 00066'024713      LDA 1 PURGE      ; LOAD SAMPLE PURGE TIME
33 00067'020734      LDA 0 RELAY+8.
34 00070'004450      JSR RESET
35 00071'022735      LDA 0 @POINT+1
36 00072'040736      STA 0 SSEC
37 00073'020720      LDA 0 RELAY      ; LOAD RELAYS TO TAKE SAMPLE
38 00074'024735      LDA 1 DRAW
39 00075'004443      JSR RESET
40 00076'020716      LDA 0 RELAY+1    ; STIR ONLY
41 00077'024703      LDA 1 STINT
42 00100'004440      JSR RESET
43 00101'020714      LDA 0 RELAY+2    ; SEND SAMPLE TO UVANS
44 00102'024705      LDA 1 UVINT
45 00103'177777      .XMIT
46 00104'000003      3          ; TELL ANALYSER ROUTINE SAMPLE COMING
47 00105'004433      JSR RESET
48 00106'020710      LDA 0 RELAY+3    ; CONTINUE EMPTYING VESSEL
49 00107'024700      LDA 1 UVINT
50 00110'004430      JSR RESET
51 00111'020706      LDA 0 RELAY+4    ; COMPLETE EMPTYING
52 00112'024671      LDA 1 EMINT
53 00113'004425      JSR RESET
54 00114'020704      LDA 0 RELAY+5    ; FLUSH VESSEL
55 00115'024671      LDA 1 FSHTM
56 00116'004422      JSR RESET
57 00117'020702      LDA 0 RELAY+6    ; FILL WITH WATER & EMPTY SYRINGE
58 00120'024711      LDA 1 DRAW
59 00121'004417      JSR RESET

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0003 SAMPL

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01 00122'020702      LDA 0 RELAY+9.      ; COMPLETE FILLING IF NOT YET FULL
02 00123'024706      LDA 1 DRAW
03 00124'030664      LDA 2 FILLR
04 00125'146422      SUBZ 2 1 SZC
05 00126'000403      JMP .+3
06 00127'124400      NEG 1 1
07 00130'004410      JSR RESET
08 00131'020671      LDA 0 RELAY+7      ; FLUSH SAMPLE LINE
09 00132'024653      LDA 1 SLFSH
10 00133'004405      JSR RESET
11 00134'102400      SUB 0 0              ; CLOSE ALL VALVES
12 00135'126520      SUBZL 1 1
13 00136'004402      JSR RESET
14 00137'177777      .QUIT
15
16                    ; SUBROUTINE INDICATES RELAYS FOR RELAY PROGRAM
17
18 00140'130405  RESET:  NEG 1 2 SNR      ; TEST IF NO WAITING
19 00141'001400      JMP 0 3              ; RETURN
20 00142'054412      STA 3 RETRN        ; MUST SAVE RETURN ADDRESS
21 00143'000040'    .FORK              ; SET RELAYS
22 00144'000001      1                  ; MUST USE HIGHEST PRIORITY
23 00145'177777      RELYS
24 00146'000045'    .WAIT              ; WAIT ONE SECOND
25 00147'000144      100.
26 00150'151404      INC 2 2 SZR
27 00151'000775      JMP .-3
28 00152'002402      JMP @RETRN        ; RETURN
29
30 00153'000077  SETRL:  77
31 00154'000000  RETRN:  0
32
33                    ; ERROR MESSAGE
34
35 00155'000334"AA:  A*2
36                    A:      .TXT @SAMPLING ERROR@
00156'040523
00157'050115
00160'044514
00161'043516
00162'042440
00163'051122
00164'051117
00165'000000
37 00166'006637  SERDR:  JSR @POINT
38 00167'000155'    AA
39
40                    ;
41                    ;
42 00170'020402  END:    LDA 0 .+2      ; THIS INSTRUCTION WILL STOP SAMPLE RO
43 00171'040660      STA 0 PLACE
44 00172'000137'    .QUIT
45
46                    .END

```

```

01 .TITL RTDBO
02 .ENT RTDBO
03 .EXTN IOX TT00
04 .NREL
05
06 ; PROGRAM RECIEVES UP TO 5 DECIMAL DIGITS PLUS SIGN FROM TELETYPE
07 ; RETURNS WITH INPUT CONVERTED TO BINARY IN AC1
08 ; "+" OR "-" ACCEPTED AS SIGN ("+" OPTIONAL)
09 ; SPACE INDICATES END OF INPUT
10 ; ANY OTHER CHARACTER CAUSES DELETION OF INPUT
11 ; AND REQUEST FOR NEW NUMBER
12
13 00000'054454 RTDBO: STA 3 AC3 ;SAVE RETURN ADDRESS
14 00001'006452 JSR @POINT ;PRINT WAITING FOR NUMBER MESSAGE. #
15 00002'000055' AA
16 00003'102400 SUB 0 0 ;CLEAR ACO
17 00004'040452 STA 0 SIGN ;ENSURE STARTING SIGN IS "+"
18 00005'040452 STA 0 RESULT ;CLEAR RESULT REGISTER
19 00006'177777 GETC: .IOX
20 00007'000000 0 ;TELETYPE
21 00010'020000 020000 ; ECHO ON INPUT - WORD FORMAT
22 00011'000060' INPUT ;ADDRESS OF STORAGE
23 00012'000001 1 ;ONE CHARACTER
24 00013'000001' RTDBO+1 ;ERROR RETURN ADDRESS
25 00014'020444 LDA 0 INPUT ;LOAD INPUT CHARACTER
26 00015'024444 LDA 1 C60 ;LOAD ASCII "0"
27 00016'034444 LDA 3 C71 ;LOAD ASCII "9"
28 00017'162033 ADCZ# 3 0 SNC ;TEST IF INPUT CHARACTER
29 00020'106032 ADCZ# 0 1 SZC ;IS A DIGIT
30 00021'000402 JMP .+2 ;NOT A DIGIT
31 00022'000414 JMP DIGIT
32 00023'024440 LDA 1 PSIGN ;LOAD ASCII "+"
33 00024'106415 SUB# 0 1 SNR ;TEST FOR "+"
34 00025'000761 JMP GETC ;YES - GO BACK FOR NEXT CHARACTER
35 00026'024436 LDA 1 SP ;LOAD ASCII SPACE
36 00027'106415 SUB# 0 1 SNR ;TEST FOR SPACE
37 00030'000416 JMP END
38 00031'024434 LDA 1 NSIGN ;LOAD ASCII "-"
39 00032'106414 SUB# 0 1 SZR ;TEST FOR "-"
40 00033'000746 JMP RTDBO+1 ;NO
41 00034'040422 STA 0 SIGN ;SET SIGN INDICATOR
42 00035'000751 JMP GETC ;GO FOR NEXT CHARACTER
43
44 00036'122400 DIGIT: SUB 1 0 ;CONVERT INPUT TO BINARY
45 00037'024420 LDA 1 RESULT ;LOAD PREVIOUS INPUT
46 00040'135000 MOV 1 3 ;MULTIPLY PREVIOUS INPUT BY 10.
47 00041'127120 ADDZL 1 1 ;N*4
48 00042'167120 ADDZL 3 1 ;N*10.
49 00043'123000 ADD 1 0 ;OBTAIN NEW NUMBER
50 00044'040413 STA 0 RESULT ;STORE NEW NUMBER
51 00045'000741 JMP GETC
52
53 00046'024411 END: LDA 1 RESULT ;LOAD ANSWER
54 00047'020407 LDA 0 SIGN ;LOAD SIGN INDICATOR
55 00050'101004 MOV 0 0 SZR ;TEST SIGN OF NUMBER
56 00051'124400 NEG 1 1 ;NEGATIVE NUMBER SO CHANGE SIGN
57 00052'002402 JMP @AC3 ;RETURN TO CALLING PROGRAM
58
59 00053'177777 POINT: TT00

```

0002 RTDB0

01 00054'000000 AC3: 0
02 00055'000154"AA: A*2
03 00056'000000 SIGN: 0
04 00057'000000 RESLT: 0
05 00060'000000 INFJT: 0
06 00061'000060 C60: 60
07 00062'000071 C71: 71
08 00063'000053 PSIGN: 53
09 00064'000040 SP: 40
10 00065'000055 NSIGN: 55
11
12 A: .TXT "# "
00066'020043
00067'000000

13

14

.END

```

01 . TITL RTBDO
02 . ENT RTBDO
03 . EXTN . IOX BIDEC
04 . NREL
05
06 ; PROGRAM TO OUTPUT A NUMBER ON TELETYPE
07 ; CALL WITH ACO - NUMBER TO BE PRINTED
08 ; AC1 - NUMBER OF CHARACTERS (OCTAL IF NEGATIVE) (MAX)
09 ; AC2 - NOT USED AND SAVED
10 ; SPACE PRINTED AT END OF NUMBER
11
12 00000'050511 RTBDO: STA 2 AC2 ;SAVE AC2
13 00001'054511 STA 3 AC3 ;SAVE RETURN ADDRESS
14 00002'125112 MOVL# 1 1 SZC ;TEST IF OCTAL NUMBER
15 00003'000516 JMP OCTAL ;YES GO TO THAT ROUTINE
16 00004'034507 LDA 3 MASK ;LOAD TO GET # OF CHARACTERS
17 00005'131300 MOVS 1 2 ;MOVE AND SWAP WORD
18 00006'167400 AND 3 1 ;MASK OUT UNWANTED BITS
19 00007'044501 STA 1 NUMBR ;STORE NUMBER OF CHARACTERS
20 00010'173400 AND 3 2 ;MASK OUT TO GET DECIMAL PLACE
21 00011'050503 STA 2 DECML
22 00012'006466 JSR @POINT+1 ;CONVERT TO DECIMAL
23 000006 RESULT: .BLK 6 ;SPACES FOR RESULT
24 00021'000040 C40: 40 ;ASCII SPACE
25 00022'034455 LDA 3 POINT ;GET ADDRESS OF RESULT
26 00023'102400 SUB 0 0 ;CLEAR ACO
27 00024'040463 STA 0 NVAL ;CLEAR NVAL
28 00025'030774 LDA 2 C40 ;LOAD ASCII SPACE
29 00026'024456 LDA 1 C60 ;LOAD ASCII ZERO
30 00027'021401 LDA 0 1 3 ;LOAD DIGIT
31 00030'106414 SUB# 0 1 SZR ;TEST IF ASCII ZERO
32 00031'000405 JMP .+5 ;NO - HAVE FIRST NON ZERO DIGIT
33 00032'010455 ISZ NVAL ;INCREMENT ZERO COUNTER
34 00033'051401 STA 2 1 3 ;STORE SPACE IN DIGIT
35 00034'175400 INC 3 3 ;INCREMENT ADDRESS INDICATOR
36 00035'000772 JMP .-6 ;GO BACK TO TEST NEXT DIGIT
37 00036'024451 LDA 1 NVAL ;LOAD NUMBER OF LEADING ZEROS
38 00037'020754 LDA 0 RESULT ;GET SIGN OF NUMBER
39 00040'050753 STA 2 RESULT ;STORE SPACE IN HERE
40 00041'034442 LDA 3 NSIGN ;GET ASCII "-"
41 00042'116414 SUB# 0 3 SZR ;TEST IF NEGATIVE NUMBER
42 00043'000406 JMP .+6 ;NO SKIP TO NEXT TEST
43 00044'034433 LDA 3 POINT ;GET ADDRESS OF RESULT
44 00045'137000 ADD 1 3 ;GET ADDRESS WHERE SIGN SHOULD BE
45 00046'041400 STA 0 0 3 ;STORE SIGN
46 00047'014440 DSZ NVAL ;DECREMENT NUMBER OF LEADING ZEROS
47 00050'000401 JMP .+1
48 00051'020435 LDA 0 C6 ;LOAD 6
49 00052'024435 LDA 1 NVAL ;LOAD # OF UNNECESSARY PRINTS
50 00053'125400 INC 1 1 ;GET ACTUAL REDUNDANT PRINTS
51 00054'122404 SUB 1 0 SZR ;OBTAIN NUMBER OF SPACES REQU'D FOR PRINT
52 00055'000404 JMP .+4 ;THESE NEXT THREE INSTRUCTIONS
53 00056'030426 LDA 2 C60 ;STORE 0 FOR ALL ZERO NUMBER
54 00057'050741 STA 2 RESULT+5
55 00060'101400 INC 0 0
56 00061'024427 LDA 1 NUMBR ;GET NUMBER OF SPACE SPECIFIED
57 00062'040425 STA 0 NVAL ;SAVE NUMBER OF ACTUAL DIGITS
58 00063'125005 MOV 1 1 SNR
59 00064'000433 JMP MIN ;WANT MINIMUM # OF SPACES PRINTED

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0002 RTBDO
01 00065'122033      ADCZ# 1 0 SNC      ;SKIP IF NUMBR<NVAL
02 00066'000452      JMP  OUTPT
03
04 00067'020413      LDA  0  I          ;LOAD ASCII "*"
05 00070'024415      LDA  1  N6         ;LOAD # OF DIGITS
06 00071'034406      LDA  3  POINT     ;LOAD ADDRESS OF RESULT
07 00072'041400      STA  0  0  3     ;STORE *'S TO INDICATE OVERFLOW
08 00073'175400      INC  3  3         ;INCREMENT ADDRESS INDICATOR
09 00074'125404      INC  1  1  SZR    ;TEST COMPLETION
10 00075'000775      JMP  -3          ;GO BACK FOR NEXT STORE
11 00076'000442      JMP  OUTPT
12
13          ; DATA FOR RTBDO
14
15 00077'000013'POINT:  RESULT
16 00100'177777      BIDEC
17 00101'000021'      RESULT+6
18 00102'000052  I:    052
19 00103'000055  NSIGN: 55
20 00104'000060  C60:   60
21 00105'177772  N6:    -6
22 00106'000006  C6:    6
23 00107'000000  NVAL:  0
24 00110'000006  NUMBR:  6
25 00111'000000  AC2:   0
26 00112'000000  AC3:   0
27 00113'000007  MASK:  7
28 00114'000000  DECML:  0
29 00115'000116'DOTAD: DOTAD+1
30 00116'000056      056
31
32 00117'040771  MIN:   STA  0  NUMBR
33 00120'000420      JMP  OUTPT
34
35 00121'024765  OCTAL:  LDA  1  C6          ;ALTER TO POSITIVE NUMBER
36 00122'044766      STA  1  NUMBR
37 00123'030762      LDA  2  N6         ;LOAD COUNTER
38 00124'024767      LDA  1  MASK     ;LOAD OCTAL MASK
39 00125'107400      AND  0  1         ;GET OCTAL DIGIT
40 00126'034756      LDA  3  C60       ;GET ASCII CONVERSION NUMBER
41 00127'167000      ADD  3  1         ;CONVERT OCTAL DIGIT TO ASCII
42 00130'034747      LDA  3  POINT     ;GET RESULT ADDRESS
43 00131'156400      SUB  2  3         ;GET CORRECT POSITION
44 00132'045777      STA  1  -1  3     ;STORE IN CORRECT DIGIT REGISTER
45 00133'101220      MOVZR 0  0        ;MOVE INPUT TO CORRECT POSITION
46 00134'101220      MOVZR 0  0        ;FOR GETTING NEXT DIGIT
47 00135'101220      MOVZR 0  0
48 00136'151404      INC  2  2  SZR    ;TEST IF FINISHED
49 00137'000765      JMP  OCTAL+3
50
51 00140'020754  OUTPT:  LDA  0  DECML     ;LOAD # OF DIGITS AFTER DECIMAL
52 00141'024746      LDA  1  NVAL     ;LOAD # DIGITS IN RESULT
53 00142'106433      SUBZ# 0  1  SNC   ;TEST IF ANY BLANKS AFTER ". "
54 00143'000425      JMP  ADZRO      ;A BLANK - REPLACE BY "0"
55 00144'020735      LDA  0  POINT+2 ;GET ADDRESS OF LAST DIGIT
56 00145'024743      LDA  1  NUMBR   ;LOAD # OF DIGITS TO PRINT
57 00146'122400      SUB  1  0        ;GET POSITION OF FIRST DIGIT
58 00147'030745      LDA  2  DECML   ;LOAD # OF DIGITS AFTER DECIMAL
59 00150'146405      SUB  2  1  SNR   ;GET # DIGITS BEFORE DECIMAL

```


0003 RTBDO

```

01 00151'000402      JMP  +2      ;NO DIGITS - SO DON'T PRINT ANY
02 00152'004427      JSR PRINT    ;PRINT LEADING DIGITS
03 00153'030741      LDA 2 DECML   ;LOAD # DIGITS AFTER DECIMAL
04 00154'151005      MOV 2 2 SNR   ;TEST IF DECIMAL WANTED
05 00155'000404      JMP FINIS    ;NO - SO DON'T PRINT ANY
06 00156'020737      LDA 0 DOTAD   ;LOAD ADDRESS OF "."
07 00157'126520      SUBZL 1 1     ;PRINT ONE CHARACTER
08 00160'004421      JSR PRINT    ;PRINT "."
09 00161'024733 FINIS: LDA 1 DECML   ;GET REMAINING DIGITS
10 00162'020717      LDA 0 POINT+2 ;GET ADDRESS OF FINAL DIGIT
11 00163'122400      SUB 1 0      ;GET ADDRESS FOR PRINT
12 00164'125400      INC 1 1      ;INCREMENT TO INCLUDE FINAL SPACE
13 00165'004414      JSR PRINT    ;PRINT REMAINING CHARACTERS
14 00166'030723      LDA 2 AC2    ;RESTORE AC2
15 00167'002723      JMP @AC3    ;RETURN
16
17 00170'034711 ADZRO: LDA 3 POINT+2 ;GET ADDRESS OF LAST DIGIT
18 00171'125400      INC 1 1      ;INCREMENT DIGIT COUNTER
19 00172'136400      SUB 1 3      ;GET CORRECT POSITION FOR "0"
20 00173'030711      LDA 2 C60    ;LOAD "0"
21 00174'051400      STA 2 0 3    ;REPLACE BLANK WITH "0"
22 00175'030713      LDA 2 NUMBR   ;
23 00176'132433      SUBZ# 1 2 SNC ;SKIP IF NUMBR >OR= NVAL
24 00177'010711      ISZ NUMBR   ;INCREMENT # PRINTS
25 00200'000742      JMP OUTPT+2 ;
26
27 00201'054412 PRINT: STA 3 RET
28 00202'040405      STA 0 PFP
29 00203'044405      STA 1 NNN
30 00204'177777      . IOX
31 00205'000000      0
32 00206'120000      120000
33 00207'000013'PFP: RESULT
34 00210'000006 NNN: 6
35 00211'000212'    . +1
36 00212'002401      JMP @RET
37 00213'000000 RET: 0
38
39                      . END

```

```

01          .TITL MATHS
02          .ENT BIDEC MULTY DIVID
03          .NREL
04
05          ; THESE PROGRAMS ARE ALL RE-ENTRANT
06          ; EACH WILL BE DESCRIBED SEPARATELY BELOW
07
08          ; PROGRAM 1 - BINARY TO DECIMAL CONVERSION
09          ; CALL SEQUENCE
10          ;     JSR BIDEC
11          ;     .BLK 7
12          ;     <RETURN>
13          ;
14          ;     CALL WITH ACO CONTAINING BINARY
15          ;     DECIMAL NUMBER RETURNED IN FIRST SIX
16          ;     LOCATIONS FOLLOWING CALL STATEMENT
17          ;     SIGN GIVEN IN FIRST LOCATION IN ASCII
18 00000'024437 BIDEC: LDA 1 C60          ; LOAD ASCII "0"
19 00001'045400 STA 1 0 3          ; STORE IN SIGN INDICATOR
20 00002'101113  MOV# 0 0 SNC          ; TEST SIGN OF NUMBER
21 00003'000404 JMP +4          ; POSITIVE NUMBER - JUMP
22 00004'100400 NEG 0 0
23 00005'024431 LDA 1 NSIGN          ; LOAD ASCII "-"
24 00006'045400 STA 1 0 3          ; STORE IN SIGN ADDRESS
25 00007'030421 LDA 2 TEST          ; LOAD ADDRESS OF POWERS OF TEN TABLE
26 00010'151400 NEXT: INC 2 2          ; INCREMENT DIVISOR ADDRESS
27 00011'175400 INC 3 3          ; INCREMENT DIGIT ADDRESS
28 00012'024425 LDA 1 C60          ; LOAD ASCII "0"
29 00013'045400 STA 1 0 3          ; STORE AS START FOR DIGIT
30 00014'025000 LDA 1 0 2          ; GET DIVISOR
31 00015'125212 MOVR# 1 1 SZC          ; TEST IF LAST DIVISOR
32 00016'000406 JMP END          ; YES
33 00017'122512 SUBL# 1 0 SZC          ; TEST IF DIVISOR GOES IN
34 00020'000770 JMP NEXT          ; NO - GET NEXT DIVISOR
35 00021'122400 SUB 1 0          ; SUBTRACT DIVISOR
36 00022'011400 ISZ 0 3          ; INCREMENT DIGIT
37 00023'000774 JMP -4          ; TRY AGAIN
38 00024'025400 END: LDA 1 0 3          ; LOAD LAST "0"
39 00025'107000 ADD 0 1          ; GET LAST NUMBER
40 00026'045400 STA 1 0 3          ; STORE IT
41 00027'001402 JMP 2 3          ; RETURN TO CALLING PROGRAM
42
43 00030'000030 TEST: TEST
44 00031'023420 10000.
45 00032'001750 1000.
46 00033'000144 100.
47 00034'000012 10.
48 00035'000001 1.
49 00036'000055 NSIGN: 55
50 00037'000060 C60: 60
51
52          ; PROGRAM 2 - SINGLE PRECISION MULTIPLY
53          ; CALL SEQUENCE
54          ;     JSR (MULTY)
55          ;     16:
56          ;     <RETURN>
57          ;
58          ;     CALL WITH NUMBERS IN ACO AND AC1
59          ;     HIGHER ORDER RESULT IN ACO
          ;     LOWER ORDER RESULT IN AC1 RETURNED

```

```

01
02 00040'020422 MULTY:  LDA 0 C16      ;LOAD COUNTER
03 00041'041400      STA 0 0 3      ;STORE COUNTER
04 00042'102400      SUB 0 0          ;CLEAR ACO
05 00043'125203      MOVR 1 1 SNC      ;CHECK NEXT MULTIPLIER BIT
06 00044'101201      MOVR 0 0 SKP      ;BIT=0, SHIFT ONLY
07 00045'143220      ADDZR 2 0      ;BIT=1, ADD MULTIPLIER AND SHIFT
08 00046'015400      DSZ 0 3        ;COUNT STEP
09 00047'001401      JMP 1 3        ;RETURN
10
11          ; PROGRAM 3 - SINGLE PRECISION DIVIDE
12          ; CALL SEQUENCE
13          ; JSR (DIVID)
14          ; 16.
15          ; <RETURN>
16          ; ACO AND AC1 CONTAIN HIGHER AND LOWER
17          ; ORDER NUMERATOR RESPECTIVELY
18          ; AC2 CONTAINS DENOMINATOR
19          ; RETURNS WITH RESULT IN AC1
20
21 00050'125120 DIVID:  MOVZL 1 1      ;SHIFT DIVIDEND LOW PART
22 00051'101100      MOVL 0 0        ;SHIFT DIVIDEND HIGH PART
23 00052'142412      SUB# 2 0 SZC      ;DOES DIVISOR GO IN
24 00053'142400      SUB 2 0
25 00054'125100      MOVL 1 1
26 00055'015400      DSZ 0 3        ;COUNT STEP
27 00056'000773      JMP DIVID+1
28 00057'030403      LDA 2 C16      ;RELOAD COUNTER
29 00060'051400      STA 2 0 3      ;STORE COUNTER
30 00061'001401      JMP 1 3        ;RETURN
31
32 00062'000020 C16:  16.
33
34          .END

```

```

01          .TITL INFCE
02          .ENT RELYS TTOD ATOD TRANS ATOD1 SRLYS TTR TTC
03          .EXTN .IOX .WAIT
04          .EXTN DIVID .QUIT
05          .NREL
06
07          ; THIS ROUTINE SETS THE RELAY PATTERN
08          ; MUST BE HIGHEST PRIORITY IN SYSTEM
09          ; CALL SEQUENCE
10          ;          .FORK
11          ;          1
12          ;          RELYS
13          ;
14          ;          ACO SHOULD CONTAIN DESIRED RELAYS
15          ;          AC1 SHOULD CONTAIN RELAYS THAT SHOULD
16          ;          NOTBE CHANGED
17 00000'000000 SRLYS: 0          ;CURRENT STATUS OF RELAYS
18
19 00001'030777 RELYS: LDA 2 SRLYS  ;LOAD CURRENT RELAY STATUS
20 00002'133400      AND 1 2      ;KEEP RELAYS NOT TO BE CHANGED
21 00003'113000      ADD 0 2      ;ADD NEW RELAY CONFIGERATION
22 00004'071025      DCA 2 25     ;OUTPUT RELAY CONFIGERATION
23 00005'050773      STA 2 SRLYS  ;UPDATE RELAY STATUS
24 00006'177777      .QUIT
25
26          ; THIS ROUTINE OUTPUTS A STRING OF CHARACTERS TO TELETYPE
27          ;          CALLING SEQUENCE
28          ;          JSR TTOD
29          ;          ADDRESS OF BYTE POINTER
30          ;          RETURN
31          ; AC1, AC2 AND CARRY REMAIN UNCHANGED
32
33 00007'023400 TTOD: LDA 0 @0 3   ;LOAD ADDRESS OF BYTE POINTER
34 00010'040406      STA 0 A      ;STORE IN CORRECT POSITION
35 00011'175400      INC 3 3      ;GET RETURN ADDRESS
36 00012'054410      STA 3 AA     ;SAVE RETURN ADDRESS
37 00013'177777      .IOX
38 00014'000000      0           ;TELETYPE
39 00015'102000      102000      ;OUTPUT
40 00016'000000 A: 0           ;ADDRESS OF BYTE POINTER
41 00017'000454      300.        ;# OF CHARACTERS (RTDS STOPS AT FIRST
42 00020'000021'    .+1         ;ERROR RETURN ADDRESS
43 00021'002401      JMP @AA     ;RETURN TO CALLING PROGRAM
44 00022'000000 AA: 0
45
46          ; THIS ROUTINE CONTINUALLY READS THE A/D CHANNELS
47
48 00023'000013'TRANS: .IOX
49 00024'000007      7           ;A/D
50 00025'000000      0
51 00026'000075'    ATOD        ;ADDRESS OF DATA STORAGE
52 00027'000020      16.        ;READ ALL 16 CHANNELS
53 00030'000031'    .+1         ;ERROR RETURN ADDRESS
54
55          ;THE FOLLOWING IS A DIGITAL FILTER
56
57 00031'024444      LDA 1 ATOD   ;LOAD REACTOR TEMPERATURE
58 00032'020437      LDA 0 TR    ;LOAD RUNNING SUM
59 00033'123000      ADD 1 0

```

0002 INFCE

```

01 00034'040435 STA 0 TR
02 00035'034441 LDA 3 ATOD1
03 00036'030432 LDA 2 TC
04 00037'173000 ADD 3 2
05 00040'050430 STA 2 TC
06 00041'014433 DSZ CONTR
07 00042'000761 JMP TRANS
08 00043'050423 STA 2 SAVE
09 00044'105000 MOV 0 1
10 00045'102400 SUB 0 0
11 00046'030421 LDA 2 NUMBR
12 00047'006416 JSR @POINT
13 00050'000020 16.
14 00051'044421 STA 1 TTR
15 00052'024414 LDA 1 SAVE
16 00053'102400 SUB 0 0
17 00054'006411 JSR @POINT
18 00055'000020 16.
19 00056'044415 STA 1 TTC
20 00057'102400 SUB 0 0 ; CLEAR ACO
21 00060'040411 STA 0 TR ; RESET SUMMING REGISTERS
22 00061'040407 STA 0 TC
23 00062'020405 LDA 0 NUMBR ; RESET COUNTER
24 00063'040411 STA 0 CONTR
25 00064'000737 JMP TRANS ; REPEAT ROUTINE
26
27 00065'177777 POINT: DIVID
28 00066'000000 SAVE: 0
29 00067'000037 NUMBR: 37
30 00070'000000 TC: 0
31 00071'000000 TR: 0
32 00072'000000 TTR: 0
33 00073'000000 TTC: 0
34 00074'000010 CONTR: 8.
35 00075'000000 ATOD: 0
36 000017 ATOD1: . BLK 15.
37
38 .END

```

```

01 .TITL CLOCK
02 .ENT CLOCK HOUR MINIT SECND RTIME
03 .EXTN RTDBO .WAIT .FORK .XMIT .RCV .QUIT
04 .NREL
05
06 ; THIS PROGRAM KEEPS TRACK OF TIME
07
08 00000'130740 RTIME: -20000.
09 00001'000000 HOUR: 0
10 00002'000000 MINIT: 0
11 00003'000000 SECND: 0
12 00004'000074 C60: 60.
13 00005'000015 C13: 13.
14
15 00006'177777 CLOCK: .FORK
16 00007'000005 5
17 00010'000045' TIME
18 00011'020773 LDA 0 C60
19 00012'030773 LDA 2 C13
20 00013'177777 RCVE: .RCV ;WAIT FOR INDICATION THAT A SECOND HAS
21 00014'000004 4
22 00015'010763 ISZ RTIME
23 00016'000401 JMP .+1
24 00017'177777 .XMIT
25 00020'000001 1
26 00021'024762 LDA 1 SECND
27 00022'125400 INC 1 1 ;INCREMENT SECOND COUNTER
28 00023'106415 SUB# 0 1 SNR ;TEST IF MINUTE HAS PASSED
29 00024'126400 SUB 1 1 ;YES - SET SECOND COUNTER TO ZERO
30 00025'044756 STA 1 SECND
31 00026'125004 MOV 1 1 SZR ;TEST SECOND COUNTER
32 00027'000764 JMP RCVE
33 00030'024752 LDA 1 MINIT ;MINUTE HAS PASSED
34 00031'125400 INC 1 1 ;INCREMENT MINUTE COUNTER
35 00032'106415 SUB# 0 1 SNR ;TEST IF HOUR HAS PASSED
36 00033'126400 SUB 1 1 ;YES - ZERO HOUR COUNTER
37 00034'044746 STA 1 MINIT
38 00035'125004 MOV 1 1 SZR ;TEST MINUTE COUNTER
39 00036'000755 JMP RCVE
40 00037'024742 LDA 1 HOUR ;HOUR HAS PASSED
41 00040'125400 INC 1 1 ;INCREMENT HOUR COUNTER
42 00041'146415 SUB# 2 1 SNR ;TEST IF 12 HOURS HAVE PASSED
43 00042'126520 SUBZL 1 1 ;YES - SET HOUR COUNTER = 1
44 00043'044736 STA 1 HOUR
45 00044'000747 JMP RCVE
46
47 00045'177777 TIME: .WAIT ;WAIT FOR ONE SECOND
48 00046'000144 100.
49 00047'000017' .XMIT ;TELL CLOCK A SECOND HAS PASSED
50 00050'000004 4
51 00051'000774 JMP TIME ;GO WAIT ANOTHER SECOND
52
53 .END

```

```

01 . TITL PINIT
02 . ENT PINIT ITEM1 I1SRT I1STP ITEM2 I2SRT I2STP
03 . ENT ITEM3 I3SRT I3STP ITEM4 I4SRT I4STP
04 . ENT ITEM5 ITEM6 I5SRT I6SRT I5STP I6STP
05 . ENT ITEM7 I7SRT I7STP
06 . EXTN . RCV . FORK ERROR RTIME
07 . NREL
08
09 ;
10 ; PROGRAM INITIATES AND TERMINATES PROGRAMS AT DESIRED TIME
11 ; AS SCHEDULED
12 ;
13
14 00000'177777 PINIT: . RCV ; WAIT FOR SECOND COUNTER FROM CLOCK
15 00001'000001 1
16 00002'022424 LDA 0 @FOINT ; FIND CURRENT TIME
17 00003'034424 LDA 3 ITEMS ; LOAD ITEM ADDRESS
18 00004'054020 STA 3 Z0 ; STORE IN AUTOINCREMENT REGISTER
19 00005'026020 CHECK: LDA 1 @Z0 ; LOAD PROGRAM
20 00006'125005 MOV 1 1 SNR ; CHECK IF THERE IS A PROGRAM THERE
21 00007'000771 JMP PINIT ; NO - END OF TABLE
22 00010'044414 STA 1 PROG+3 ; STORE LOCATION OF PROGRAM
23 00011'026020 LDA 1 @Z0 ; LOAD STARTING TIME FOR THIS PROGRAM
24 00012'106415 SUB# 0 1 SNR ; READY TO BE STARTED ?
25 00013'004406 JSR PROG ; YES - GO START IT
26 00014'014410 DSZ PROG+3 ; GET ADDRESS TO STOP PROGRAM
27 00015'026020 LDA 1 @Z0 ; LOAD STOPPING TIME
28 00016'106415 SUB# 0 1 SNR ; READY TO BE STOPPED ?
29 00017'004402 JSR PROG ; YES - GO START IT
30 00020'000765 JMP CHECK
31 00021'171000 PROG: MOV 3 Z
32 00022'177777 . FORK
33 00023'000050 50
34 00024'177777 ERROR
35 00025'001000 JMP 0 Z
36
37 00026'177777 FOINT: RTIME
38
39 00027'000027 ITEMS: ITEMS
40 00030'000000 ITEM1: 0
41 00031'000000 I1SRT: 0
42 00032'000000 I1STP: 0
43 00033'000000 ITEM2: 0
44 00034'000000 I2SRT: 0
45 00035'000000 I2STP: 0
46 00036'000000 ITEM3: 0
47 00037'000000 I3SRT: 0
48 00040'000000 I3STP: 0
49 00041'000000 ITEM4: 0
50 00042'000000 I4SRT: 0
51 00043'000000 I4STP: 0
52 00044'000000 ITEM5: 0
53 00045'000000 I5SRT: 0
54 00046'000000 I5STP: 0
55 00047'000000 ITEM6: 0
56 00050'000000 I6SRT: 0
57 00051'000000 I6STP: 0
58 00052'000000 ITEM7: 0
59 00053'000000 I7SRT: 0

```

0002 FINIT

01 00054'000000 I7STP: 0
02 00055'000000 0

03

04 . END


```

01          .TITL UVANS
02          .ENT UVANS
03          .EXTN .RCV .WAIT FLAGL TT00 RTBDO LOG
04          .EXTN SMIN SSEC .FORK .QUIT
05          .NREL
06
07          ; THIS PROGRAM SUPERVISES THE OPERATION OF THE UV
08          ; SPECTROPHOTOMETER, ANALYSIS AND PRINTING OF
09          ; RESULTS
10
11 00000'177777 UVANS:  .RCV          ;WAIT FOR SAMPLE INDICATION FROM
12 00001'000003          3          ;SAMPLE PROGRAM
13 00002'022413          LDA 0 @POINT+3 ;GET TIME WHEN SAMPLE WAS TAKEN
14 00003'040415          STA 0 STIME   ;SAVE TIME IN MINUTES
15 00004'022412          LDA 0 @POINT+4
16 00005'040414          STA 0 STIME+1 ;SAVE TIME IN SECONDS
17 00006'177777          .FORK
18 00007'000100          100
19 00010'000042'        PRINT
20 00011'000767        JMP UVANS
21
22          ; DATA SECTION FOR UVANS
23
24 00012'177777 POINT:  TT00
25 00013'177777          RTBDO
26 00014'177777          FLAGL
27 00015'177777          SMIN
28 00016'177777          SSEC
29 00017'177777          LOG
30
31 00020'000000 STIME:  0
32 00021'000000          0
33 00022'000000 POSTN:  0
34 00023'000023'WAVE:  WAVE
35 00024'001130 WAVE1:  600.
36 00025'000000 TURB1:  0
37 00026'000764 WAVE2:  500.
38 00027'000000 TURB2:  0
39 00030'000620 WAVE3:  400.
40 00031'000000 TURB3:  0
41 00032'000536 WAVE4:  350.
42 00033'000000 TURB4:  0
43 00034'000454 WAVE5:  300.
44 00035'000000 TURB5:  0
45 00036'000000          0
46
47 00037'000000 SNO:    0
48 00040'000006 C6:    6
49 00041'001406 F6:    1406
50
51          ; THIS SECTION PRINTS RESULTS OF UV ANALYSIS
52
53 00042'022752 PRINT:  LDA 0 @POINT+2 ;LOAD LOGGING FLAG
54 00043'101004          MOV 0 0 SZR   ;TEST IF LOG ROUTINE RUNNING
55 00044'000404          JMP CONT    ;YES - SO CAN PRINT
56 00045'177777          .WAIT
57 00046'000144          100.
58 00047'000773          JMP PRINT
59 00050'102400 CONT:   SUB 0 0          ;CLEAR ACO

```

```

0002 UVANS
01 00051'042743 STA 0 @POINT+2 ;STOP LOGGING ROUTINE
02 00052'000045' .WAIT ;MAKE SURE LOGGING HAS STOPPED
03 00053'000120 80.
04 00054'006736 JSR @POINT ;PRINT SAMPLE #
05 00055'000112' MESSA
06 00056'010761 ISZ SNO ;INCREMENT SAMPLE #
07 00057'020760 LDA 0 SNO
08 00060'126400 SUB 1 1 ;INDICATE MINIMUM PRINTING
09 00061'006732 JSR @POINT+1 ;PRINT NUMBER
10 00062'006730 JSR @POINT ;PRINT "TAKEN AT (SEC)"
11 00063'000113' MESSB
12 00064'020735 LDA 0 STIME+1
13 00065'126400 SUB 1 1 ;MINIMUM PRINTING
14 00066'006725 JSR @POINT+1 ;PRIT TIME IN SECONDS
15 00067'006723 JSR @POINT ;PRINT WAVELENGTH AND TURBIDITY
16 00070'000114' MESSC
17 00071'030732 LDA 2 WAVE ;LOAD ADDRESS OF WAVELENGTH
18 00072'050730 STA 2 POSTN ;STORE IN POSITION INDICATOR
19 00073'006717 REPET: JSR @POINT ;PRINT CR AND LF
20 00074'000115' MESSD
21 00075'010725 ISZ POSTN ;INCREMENT POSITION INDICATOR
22 00076'022724 LDA 0 @POSTN ;LOAD VALUE OF WAVELENGTH
23 00077'024741 LDA 1 C6
24 00100'101005 MOV 0 0 SNR ;TEST IF AT END OF TABLE
25 00101'000407 JMP ENDF
26 00102'006711 JSR @POINT+1 ;PRINT WAVELENGTH VALUE
27 00103'010717 ISZ POSTN ;INCREMENT POSITION INDICATOR
28 00104'022716 LDA 0 @POSTN ;LOAD TURBIDITY
29 00105'024734 LDA 1 F6
30 00106'006705 JSR @POINT+1
31 00107'000764 JMP REPET
32
33 00110'126520 ENDF: SUBZL 1 1
34 00111'002706 JMP @POINT+5 ;RESTART LOGGING ROUTINE
35
36 00112'000234"MESSA: A*2
37 00113'000252"MESSB: B*2
38 00114'000274"MESSC: C*2
39 00115'000322"MESSD: D*2
40
41 A: .TXT @<15><12><12>SAMPLE # @
00116'005015
00117'051412
00120'046501
00121'046120
00122'020105
00123'020043
00124'000000
42 B: .TXT @ TAKEN AT (SEC) @
00125'020040
00126'040524
00127'042513
00130'020116
00131'052101
00132'024040
00133'042523
00134'024503
00135'000040
43 C: .TXT @<15><12><12>W. L. (NM) TURBIDITY@

```

0003 UVANS

99

00136'005015
00137'053412
00140'046056
00141'024056
00142'046516
00143'020051
00144'052524
00145'041122
00146'042111
00147'052111
00150'000131

01 D: .TXT @<15><12> @
00151'005015
00152'000040

02
03 .END

```

01 . TITL LOG
02 . ENT LOG LOGST FLAGL LGINT
03 . EXTN SRLYS RTBDO HOUR MINIT SECND TTOD RTIME
04 . EXTN TEMPC TEMPR
05 . EXTN . QUIT . FORK . WAIT
06 . NREL
07
08 ; THIS ROUTINE LOGS VALUES ON TTOD
09 ; PROGRAM CONTINUES TO RUN BUT DOES NOT LOG WHEN FLAGL=0
10 ; PROGRAM OUTPUTS TO TTD AGAIN WHEN FLAGL=0
11
12 00000'177777 POINT: RTBDO
13 00001'177777 TTOD
14
15 00002'000002 LIST: LIST
16 00003'177777 HOUR
17 00004'000002 2
18 00005'177777 MINIT
19 00006'000002 2
20 00007'177777 SECND
21 00010'000002 2
22 00011'177777 RTIME
23 00012'000006 6
24 00013'177777 SRLYS
25 00014'177772 -6
26 00015'177777 TEMPC
27 00016'000405 405
28 00017'177777 TEMPR
29 00020'000405 405
30 00021'000000 0 ; END OF TABLE INDICATION
31
32 00022'000000 FLAGL: 0
33 00023'000154"AA: A*2
34 00024'000224"BB: B*2
35
36 00025'006754 LOG: JSR @POINT+1 ; TYPE LOGGER HEADING
37 00026'000023 AA
38 00027'102520 SUBZL 0 0 ; SET FLAG=1 FOR LOGGER
39 00030'040772 STA 0 FLAGL
40 00031'177777 . QUIT
41
42 00032'000012 LGINT: 10.
43
44 00033'024777 LOGST: LDA 1 LGINT ; LOAD LOGGING INTERVAL
45 00034'124400 NEG 1 1
46 00035'177777 . WAIT ; WAIT ONE SECOND
47 00036'000144 100.
48 00037'125404 INC 1 1 SZR ; TEST IF INTERVAL IS UP
49 00040'000775 JMP .-3 ; NO - WAIT ANOTHER SECOND
50 00041'020761 LDA 0 FLAGL ; LOAD FLAG
51 00042'101005 MOV 0 0 SNR ; TEST FLAG
52 00043'000770 JMP LOGST ; FLAG=0 SO DON'T PRINT
53 00044'177777 . FORK ; START LOGGING ROUTINE
54 00045'000100 100
55 00046'000050 LOGER
56 00047'000764 JMP LOGST ; GO WAIT FOR NEXT LOG
57
58 00050'006731 LOGER: JSR @POINT+1 ; TYPE CR AND LF
59 00051'000024 BB

```

0002 L06
 01 00052'030730
 02 00053'151400
 03 00054'035000
 04 00055'175005
 05 00056'000031'
 06 00057'021400
 07 00060'151400
 08 00061'025000
 09 00062'034740
 10 00063'175004
 11 00064'006714
 12 00065'000766
 13
 14

```

LDA 2 LIST      ;LOAD ADDRESS OF LIST
INC 2 2         ;INCREMENT ADDRESS
LDA 3 0 2       ;LOAD ADDRESS OF VALUE TO BE PRINTED
MOV 3 3 SNR     ;TEST IF END OF TABLE
.QUIT          ;YES
LDA 0 0 3       ;NO - LOAD VALUE TO BE PRINTED
INC 2 2         ;GET ADDRESS OF TYPE OF PRINTING
LDA 1 0 2       ;LOAD VALUE
LDA 3 FLAGL     ;LOAD FLAG
MOV 3 3 SZR     ;TEST IF FLAG=1
JSR @POINT     ;YES GO PRINT VALUE
JMP LOGER+3    ;GO GET NEXT NUMBER

```

A: .TXT @<15><12> TIME RTIME RELAYS TEMPC TEMPR@

00066'005015
 00067'020040
 00070'052040
 00071'046511
 00072'020105
 00073'051040
 00074'044524
 00075'042515
 00076'020040
 00077'042522
 00100'040514
 00101'051531
 00102'020040
 00103'042524
 00104'050115
 00105'020103
 00106'052040
 00107'046505
 00110'051120
 00111'000000

B: .TXT @<15><12>@

00112'005015
 00113'000000

16
 17

. END

```

01 . TITL FEEDS
02 . ENT MONMR INITR ENULS
03 . ENT MAXMF MAXIF MAXEF MFLOW IFLOW EFLOW
04 . EXTN . PTY . FORK . WAIT . QUIT RELYS
05 . NREL
06
07 ; THIS IS A TASK PROGRAM TO CAUSE PSEUDO-VARIABLE
08 ; FEED RATES TO REACTOR
09
10 ; SECTION A - MONOMER FEED
11
12 00000'000436 JMP ENDM ; ENTER HERE TO STOP TASK
13 00001'177777 MONMR: . PTY ; SET HIGH PRIORITY FOR ACCURACY
14 00002'000006 6
15 00003'020410 LDA 0 GO ; SET PROGRAM TO RUN
16 00004'040406 STA 0 NOGDM
17 00005'177777 . FORK ; OPEN AND CLOSE VALVE
18 00006'000050 50
19 00007'000014' DOMON
20 00010'177777 . WAIT
21 00011'000764 MAXMF: 500.
22 00012'000773 NOGDM: JMP .-5
23 00013'000773 GO: JMP .-5
24
25 00014'020413 DOMON: LDA 0 MFLOW ; LOAD FLOWRATE
26 00015'101005 MOV 0 0 SNR ; TEST IF 0 FLOW
27 00016'177777 . QUIT
28 00017'101112 MOV# 0 0 SZC ; TEST IF NEGATIVE FLOW
29 00020'000016' . QUIT
30 00021'024414 LDA 1 MRELY ; OPEN MONOMER VALVE
31 00022'120000 COM 1 0 ; SET RELAY ON
32 00023'000005' . FORK
33 00024'000001 1
34 00025'177777 RELYS
35 00026'000010' . WAIT
36 00027'000310 MFLOW: 200.
37 00030'102400 SUB 0 0 ; CLOSE MONOMER VALVE
38 00031'000023' . FORK
39 00032'000001 1
40 00033'000025' RELYS
41 00034'000020' . QUIT
42
43 00035'177737 MRELY: 177737
44
45 00036'020402 ENDM: LDA 0 STOP
46 00037'040753 STA 0 NOGDM
47 00040'000034' STOP: . QUIT
48
49 ; SECTION B - INITIATOR FEED
50
51 00041'000435 JMP ENDI ; ENTER HERE TO STOP TASK
52 00042'000001' INITR: . PTY ; SET HIGH PRIORITY FOR ACCURACY
53 00043'000006 6
54 00044'020747 LDA 0 GO ; SET PROGRAM TO RUN
55 00045'040406 STA 0 NOGDI
56 00046'000031' . FORK
57 00047'000007 7
58 00050'000054' DOIN
59 00051'000026' . WAIT ; WAIT REQUIRED PERIOD

```

0002 FEEDS

```

01 00052'000454 MAXIF: 300. ; MAXIMUM INITIATOR FLOW
02 00053'000773 NOGOI: JMP .-5
03
04 00054'020413 DOIN: LDA 0 IFLOW ; LOAD DESIRED INITIATOR FLOW
05 00055'101005 MOV 0 0 SNR ; TEST IF FLOW IS 0
06 00056'000040' .QUIT
07 00057'101112 MOVL# 0 0 SZC ; TEST IF NEGATIVE FLOW
08 00060'000056' .QUIT
09 00061'024414 LDA 1 IRELY ; OPEN INITIATOR VALVE
10 00062'120000 COM 1 0
11 00063'000046' .FORK
12 00064'000001 1
13 00065'000033' RELYS
14 00066'000051' .WAIT ; WAIT REQUIRED INTERVAL
15 00067'000310 IFLOW: 200. ; INITIATOR FLOW
16 00070'102400 SUB 0 0 ; CLOSE INITIATOR VALVE
17 00071'000063' .FORK
18 00072'000001 1
19 00073'000065' RELYS
20 00074'000060' .QUIT
21 00075'177757 IRELY: 177757 ; INDICATION FOR RELAY PROGRAM
22
23 00076'020742 ENDI: LDA 0 STOP
24 00077'040754 STA 0 NOGOI
25 00100'000074' .QUIT
26
27 ; SECTION C - EMULSIFIER FEED
28
29 00101'000435 JMP ENDE
30 00102'000042'EMULS: .PTY ; SET HIGH PRIORITY FOR ACCURACY
31 00103'000006 6
32 00104'020707 LDA 0 GO
33 00105'040406 STA 0 NOGOE
34 00106'000071' .FORK
35 00107'000007 7
36 00110'000114' DOEM
37 00111'000066' .WAIT
38 00112'000310 MAXEF: 200.
39 00113'000773 NOGOE: JMP .-5
40
41 00114'020413 DOEM: LDA 0 EFLOW
42 00115'101005 MOV 0 0 SNR ; TEST IF FLOW 0
43 00116'000100' .QUIT
44 00117'101112 MOVL# 0 0 SZC ; TEST FOR NEGATIVE FLOW
45 00120'000116' .QUIT
46 00121'024414 LDA 1 ERELY
47 00122'120000 COM 1 0
48 00123'000106' .FORK
49 00124'000001 1
50 00125'000073' RELYS
51 00126'000111' .WAIT
52 00127'000226 EFLOW: 150.
53 00130'102400 SUB 0 0
54 00131'000123' .FORK
55 00132'000001 1
56 00133'000125' RELYS
57 00134'000120' .QUIT
58
59 00135'177767 ERELY: 177767

```

01
02 00136'020702 ENDE: LDA 0 STOP
03 00137'040754 STA 0 NOGGE
04 00140'000134' . QUIT
05
06 . END

0001 TCTRL

```

01 . TITL TCTRL
02 . ENT TCTRL TSP TEMPC TEMPR TCINT TYPEC
03 . EXTN . QUIT . WAIT . FORK . TTR . TTC . RELYS
04 . NREL
05
06 ; THIS PROGRAM CONTROLS REACTOR TEMPERATURE
07 ; IT IS A TASK PROGRAM
08
09 00000'000472 JMP END
10 00001'020414 TCTRL: LDA 0 GO
11 00002'040412 STA 0 PLACE
12 00003'177777 . FORK
13 00004'000051 51
14 00005'000027 FFORM
15 00006'024412 LDA 1 TCINT ; FIND CONTROL INTERVAL
16 00007'124400 NEG 1 1
17 00010'177777 . WAIT
18 00011'000144 100. ; WAIT ONE SECOND
19 00012'125404 INC 1 1 SZR
20 00013'000775 JMP .-3
21 00014'000767 PLACE: JMP .-9.
22 00015'000767 GO: JMP .-9.
23 00016'000764 STOP: JMP .-12.
24
25 00017'000000 TYPEC: 0
26 00020'000001 TCINT: 1
27 00021'000764 TSP: 500.
28 00022'000620 TEMPC: 400.
29 00023'000763 TEMPR: 499.
30 00024'000144 LOWER: 100.
31 00025'177777 POINT: TTR
32 00026'177777 TTC
33
34 00027'024775 FFORM: LDA 1 LOWER ; LOAD ABSOLUTE 0 DEG CENT.
35 00030'022775 LDA 0 @POINT ; LOAD RECTOR TEMP. (A/D UNITS)
36 00031'122400 SUB 1 0
37 00032'101120 MOVZL 0 0 ; MULT. * 2.
38 00033'040770 STA 0 TEMPR
39 00034'022772 LDA 0 @POINT+1 ; LOAD COOLANT TEMPERATURE
40 00035'122400 SUB 1 0
41 00036'101120 MOVZL 0 0
42 00037'040763 STA 0 TEMPC ; STORE TEMP. CONVERTED TO CENTIGRADE
43 00040'020757 LDA 0 TYPEC ; CHECK CONTROL DESIRED
44 00041'101004 MOV 0 0 SZR ; CHECK FOR ANY CONTROL
45 00042'000403 JMP ONOFF ; ON - OFF CONTROL
46 00043'177777 . QUIT ; NO CONTROL DESIRED
47
48 00044'000001 RANGE: 1
49
50 00045'020756 ONOFF: LDA 0 TEMPR ; GET TEMPERATURE OF REACTOR
51 00046'024753 LDA 1 TSP ; GET DESIRED SET POINT
52 00047'030775 LDA 2 RANGE ; GET RANGE OF NO ACTION
53 00050'122400 SUB 1 0
54 00051'142512 SUBL# 2 0 SZC ; IS TEMPERATURE TOO HIGH
55 00052'100401 NEG 0 0 SKP ; NO - TEST FOR TOO COLD
56 00053'000406 JMP COOL ; YES - COOL REACTOR
57 00054'142512 SUBL# 2 0 SZC ; IS TEMPERATURE TOO LOW
58 00055'000043 . QUIT ; IN BETWEEN LEAVE AS IS
59 00056'000401 JMP HEAT ; YES - HEAT REACTOR

```

0002 TCTRL

```
01
02 00057'020410 HEAT:   LDA 0 RHEAT       ; LOAD HOT WATER VALVE RELAY
03 00060'000402       JMP  +2
04
05 00061'020407 COOL:   LDA 0 RCOOL      ; LOAD COLD WATER RELAY
06 00062'024407       LDA 1 TRELY
07 00063'000003       . FORK
08 00064'000001       1
09 00065'177777       RELYS
10 00066'000055       . QUIT
11
12 00067'000004 RHEAT:   4
13 00070'000006 RCOOL:   6
14
15 00071'177771 TRELY:   177771
16
17 00072'020724 END:     LDA 0 STOP       ; THIS INSTRUCTION STOPS CONTROLLER
18 00073'040721       STA 0 PLACE
19 00074'102400       SUB 0 0       ; D/A 0
20 00075'000765       JMP COOL+1
21
22       . END
```